

FINAL DRAINAGE REPORT
FOR
WOODY MOUNTAIN CAMPGROUND
Phase 1 Construction

July 12, 2019

COF No. PZ-18-00210

Project Location:

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Flagstaff, AZ 86001

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EXPIRES 06-30-2020

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WE Project No. 118044

Final Drainage Report for Woody Mountain Campground Phase 1 Construction



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Final Drainage Report

for

Woody Mountain Campground Phase 1 Construction

1. INTRODUCTION

This is the final drainage report for the proposed Woody Mountain Campground (Campground) development on parcels 112-01-007, 102-01-008 and 102-01-701, with an area of 20.53 acres. The current zoning is Rural Residential (RR). The site is located in Section 19, Township 21 N, and Range 07E, located south of Route 66 and east of Woody Mountain Road in the City of Flagstaff. Please note that the northwest corner of the site (the portion of the site in County's jurisdiction) has no proposed improvements. However, since it naturally flows east along with other contributing areas to the subject site, it is included (Sub-3C) in the drainage analysis to account for the flow generated by it.

The site is currently used as a campground with RV sites in the western half of the site. The proposed layout calls for 80 RV sites, 41 park model houses and 42 tent sites with other amenities which include ramadas, bath houses and numerous trails. Figure 1 shows the parcel map for the subject site. The site will be accessed via a driveway on Route 66 and an emergency access driveway from Woody Mountain Road.

Wildwood Hills (WWH) Mobile Home Park (MHP) located east of the subject site is a senior living community and has a history of frequent flooding. The original design and construction of the MHP made little or no allowance for the conveyance of off-site stormwater entering the property from the west. The historic flow pattern of the stormwater enters the MHP around the location of Unit 9 and travels in an east-southeast direction towards Unit 47 and discharging into the Kit Carson RV Park. The flow discharged into the WWH flows through the development with no positive drainage consideration except for some make-shift rock channels built later as an effort to mitigate flooding. Flood walls and flood proofing measures have been attempted by the WWH residents with little success. There are no underground piping facilities to take even a portion of the flow. Establishing a flood conduit for the 100-year flow in Wildwood Hills would be projected to cost more than \$1.1 million.

Large rainfall events, typically during the Flagstaff monsoon season, are clearly subjecting the WWH residents to flooding conditions. Flows ripping through and between homes and streets in this nature create massive, forceful momentum that can pick up objects, knock down people and cause significant property damages. It also poses hazardous conditions for not only vehicles but also for pedestrian accessibility.

The Woody Mountain Campground project, thru a joint project with the City of Flagstaff, includes a detention basin that mitigates the increased flow due to proposed Campground improvements and provides significant peak flow attenuation for flood mitigation purposes for Wildwood Hills. The project would like to accommodate some of the offsite flow in the proposed detention basin

2. DEVELOPMENT PHASES

Due to the onset of the monsoons and the risk of continued flooding at WWH's, the Woody Mountain Campground improvements will be performed in two Phases to prioritize the detention basin construction to help mitigate WWH MHP flooding risk. This report will serve as a Master Drainage Report for the WMC improvements with the following phases:

i) Phase I

Phase 1 will consist of the construction and installation of most of the proposed improvements on the easterly 8-acre parcel plus a portion of access drive in the middle 8-acre parcel. The work will include the detention basin including the liner and permanent pond portion, outlet pipes and overflow structures, LID basins, culverts, improved channels, access drive, utilities, trails, gazebo, tent sites and other site amenities. This work is anticipated to occur this fall.

ii) Phase 2

Phase 2 will consist of all of the remaining improvements on the middle and westerly parcels. There are RV sites, Park model units, access drives, utilities, bath houses. This work is anticipated to occur this fall into the spring of 2020. All of the main stormwater management facilities will be installed with Phase 1. Only conveyances, etc. will be part of Phase 2 construction. We intend to provide an Addendum to this Final Drainage Report at that time to cover the improvements proposed in Phase 2.

Also, it should be noted that there are no proposed improvements in the northwest portion of the site (County's jurisdiction). However, as it naturally flows to the proposed detention pond, the pond is sized to provide stormwater mitigation for the future improvements on this portion of the site. A separate drainage report will be prepared as and when needed to the concerned jurisdiction to address the future improvements on this portion of the site.

3. OBJECTIVES AND PROCEDURES

The purpose of this Final Drainage Report is to support the Phase 1 Construction Plan submittal and to provide calculations and results of the proposed stormwater management facilities and outlets.

i) Objectives

- To provide Low Impact Development ("LID") Integrated Management Practices ("IMP's") based on the City of Flagstaff (COF or City) Ordinance No. 2009-07. The Runoff Control Volume ("ROCV") is incorporated within the LID basins.
- To provide stormwater detention facilities to mitigate the increase in flowrate from existing to proposed conditions.
- In addition, stormwater mitigation is provided for the increase in flowrate from the future half street improvements of the adjacent Right-of-Way (ROW) off Rte 66 and Woody Mountain Road.
- In addition, the proposed detention basin **mitigates about 72% of the offsite flow rate to help alleviate the flooding problems of the WWH MHP.** The pond serves as a multi-

purpose facility by providing detention for onsite and offsite flows and also functions as an amenity to the Campground.

ii) Methodology

- The proposed improvements include three (3) Bio-Retention Basins (BRB) to provide the ROCV from the proposed onsite improvements.
- Bio-Retention basins consists of a low-lying vegetated area underlain by a sand/soil bed and gravel/underdrain system. A shallow surcharge zone exists above the bio-retention for temporary storage of the ROCV. During a storm, accumulated runoff ponds in the vegetated zone and infiltrates into the underlying sand/soil bed, filling the void spaces of the sand. The underdrain gradually dewateres the sand/soil bed and discharges the runoff to a nearby channel, swale or storm sewer. If the site has a percolation rate greater than 1 inch per hour, underdrain and the supporting gravel layers may be eliminated.
- The flow is then directed to the stormwater detention basin to address the flow rate control requirements and provide a regional detention benefit.

iii) Procedures

- Hydrologic calculations are performed per the of Flagstaff Stormwater Design Manual (SWDM) Chapter 3. United States Army Corps Engineer's (USACE) Hydrologic Engineering Center software (HEC-1), Version 4.1 is used for the runoff computation as this analysis references hydrology from previous drainage studies for the Presidio in the Pines development which used HEC-1 analysis for runoff computation. We are matching procedures for the major contributing watershed.
- Time of Concentration (T_c) calculations are performed per SWDM section 3.1.6.
- Rainfall depths are referenced from the COF SWDM Table 3-2 for a 6-hour storm duration since the watershed area is less than 1 square mile.
- Per SWDM Section 3.2, Curve Numbers for undeveloped forest are referenced from Arizona Department of Water Resources' (ADWR) "Oak Creek Flood Warning System Hydrology Report, TR 90-4, September 1990" (will be referred to as Oak Creek Hydrology Report hereafter). Curve Numbers for other land cover types are referenced from Natural Resources Conservation Services' (NRCS) National Engineering Handbook (NEH) Part 630 Hydrology, Chapter 9 Hydrologic Soil Cover Complexes Tables 9-2 (runoff curve numbers for arid and semiarid rangelands) and Table 9-5 (runoff curve numbers for urban areas). Please note the runoff curve number tables from NEH are the same as the runoff curve number tables from the NRCS Technical Release-55 (TR-55).
- The project site lies within Zone X per FEMA FIRM 04005C6804G, 04005C6808G, 04005C6816G and 04005C6812G dated September 3, 2010.
- Federal Emergency Management Agency (FEMA) defines Zone X as areas of moderate flood hazard which are areas outside the Special flood Hazard Area (SFHA) and higher

than the elevation of the 0.2% annual-chance flood. The following Figure shows the FEMA's flood zones.



Figure 2: Floodzone Map

4. RUNOFF CONTROL VOLUME (ROCV)

This project proposes three (3) Bio-Retention basins and one (1) detention basin to address the LID and detention needs.

i) Impervious Area Summary

There is an existing building with some paved areas in the northwest corner of the site. The existing impervious area on the site is 2150 SF (excluding the parcel in the County's jurisdiction).

The total impervious area in the proposed condition is 130,101 SF. Thus, the total increase in the impervious area of the site is 127,952 SF. Please see Appendix B for the breakdown of the impervious areas in the proposed condition.

ii) ROCV Calculations

$$\begin{aligned} \text{ROCV required} &= ((1" \text{ Rain})/12) \times \text{Area} \\ &= ((1" \text{ Rain})/12) \times 127952 \text{ sq. ft} = 10,663 \text{ cu. ft} = 0.24 \text{ ac-ft} \end{aligned}$$

Where: Area = increase in the impervious area (Roofs, streets, and paved parking areas)

ROCV provided = 0.27 ac. ft (Sum of ROCV in LID ponds 1 thru 3)
 ROCV provided (0.27 ac.ft) > ROCV required (0.24ac.ft).

iii) LID Basins Summary

The following table summarizes the volume of the proposed Bio-Retention basin volumes. Please see Appendix B for elevation volume calculations of the LID basins.

Table 1-Summary of Bio-Retention Basin Volumes

ID	Vol. (CF)
LID-1	5952
LID-2	2297
LID-3	3704
Total	11953

Geotechnical exploration was performed for the detention pond and it was found that the soils on the site generally have good infiltration rates (more than 1 inch/hr). Therefore, no under drain system is proposed to drain the ROCV. Please see Appendix D for the geotechnical report.

5. REFERENCE DRAINAGE STUDIES

The subject site and the contributing offsite watershed areas were included in previous drainage studies for Presidio in the Pines (Presidio). The hydrologic analysis from the Presidio drainage study has been referenced into the HEC-1 analysis of the current study. Excerpts from the Presidio drainage study are included in Appendix D for reference.

6. HYDROLOGY

The City’s Stormwater Design Manual (SWDM) guidelines are followed to analyze the runoff generated by the site. Pre-developed and Post developed runoff is computed to design the detention facilities to mitigate the increase in flow rate from pre to post developed condition.

i) Rainfall

Rainfall depths are referenced from COF SWDM Table 3-2 for 6-hour storm duration since the watershed area is less than 1 square mile.

Table 2-Rainfall Depths

Storm Event	Intensity (inches/hour)	Depth (inches)
10	0.36	2.16
25	0.43	2.58
100	0.53	3.18

ii) Time of Concentration (Tc)

Tc calculations were performed per SWDM's section 3.1.6 and are included in Appendix B. Some of the calculated Tc values were too low. Thus, a minimum Tc of 15 mins and 10 mins are used for the pre and post developed conditions.

As a guidance to the minimum Tc, ADOT Hydrologic Drainage Design Manual, HDDM Section 2.2.4 has been referenced, the minimum Tc per HDDM is 10 minutes which is more realistic for Improved/Impervious areas. With the ADOT improvements which mostly include paved/impervious areas, the minimum Tc of 10 minutes is used for post developed condition. With this approach, the minimum Tc for pre-developed condition uses a slightly higher Tc of 15 minutes. While the minimum Tc for pre-developed condition could use 10 minutes, it would underestimate the increase in flow rate from pre to post developed condition. Please note that the standard TR-55 Tc calculations do not include a component to account for the time the rain drop takes to traverse from roof top, pass thru roof gutters and then join the surface/overland flow. Thus, it is believed that the Tc of 15 minutes and 10 minutes is apt for the pre and the post developed condition.

iii) Hydrologic Soil Group (HSG)

The soils information is referenced from Natural Resources Conservation Services' (NRCS) Web Soil Survey (WSS). WSS references soil map for Oak Creek-San Francisco Peaks Area which shows the soils on site to be composed of cobbly clay loam and stony clay loam with Hydrologic Soil Group "C" and "D" (HSG C and HSG D). Curve numbers are referenced from Oak Creek Hydrology Report and NRCS curve numbers tables. Composite curve number calculations are performed to account for the landcover/land use and different hydrologic soil groups. (Please see Appendix B for Soils Information and Curve Number tables).

iv) Existing Condition

The offsite watershed area includes both developed and undeveloped areas. The contributing offsite watershed area is comprised of the Vintage 37-acre parcel located southwest of Route 66 and Woody Mountain Road, northwest portion of Presidio in Pines and southern tip of Hidden Hollow Manufactured Homes and a portion of Rail Road Springs located north of Rte 66.

The Vintage 37-acre parcel was a part of the 2006 Woody Fire burn area. To reflect this existing condition, the current analysis uses curve numbers for the post burn condition.

The Campground site receives offsite flows from the following three locations:

- South perimeter: Offsite flow is released as a point source on southern boundary from the Presidio subdivision via a 30-inch cmp. The majority of the Vintage 37-acre parcel (drainage area SUB-1A), most of the Woody Mountain Road (SUB-1B) and a portion of the Presidio subdivision discharge flow to the 30-inch cmp. The flow from the Vintage parcel and the flow generated by the Woody Mountain Road discharge into a 4'x3' RCBC under Woody Mountain Road that connects into a storm drain system in Presidio. The storm drain system conveys onsite flows from Presidio and offsite flows and eventually discharges into a 30-inch cmp that drains into the Campground site. Please note that there is some portion of Timber Sky development Blocks 1 and 2 that historically drains east towards the WWH MHP. Per City's request to Timber Sky development, this area is diverted to flow west to provide relief to the flooding issues on WWH-MHP.
- North perimeter: An existing 24-inch cmp under Rte 66 discharges flow from Hidden Hollow north of Rte 66 (SUB-2) and a portion of Rte 66 (SUB-2A) discharges into the 24-inch cmp via an existing catch basin in Rte 66. Also flow from Rte 66 flows along the roadside ditch on the south side of the road which eventually terminates and discharges into the Campground site.
- West perimeter: An existing 24"x36" arch cmp under Woody Mountain Road discharges flow from a minor portion of the Vintage 37-acre parcel (SUB-1) and Rte 66 (SUB-2A) which flows in the roadside ditch which eventually terminates and discharges into the Campground site.

The onsite watershed area is divided into three (3) drainage areas: Sub-3A, Sub-3B and Sub-3C. Drainage area Sub-3A which includes the southwest quadrant of the site, flows in a southeasterly direction, along the south perimeter wall. This flow eventually combines with the offsite flow released from the Presidio subdivision, the combined flow then continues northeasterly towards the existing pond in the campground site.

The drainage area SUB-3B comprises the majority of the site. Runoff generated by Sub-3B and 3C traverses through the existing swales and eventually continues as ditches at the steeper easterly portion of the site.

All the onsite and offsite flow ultimately discharges into a makeshift pond that was roughly excavated to pond flows before the flow continues east into the WWH MHP. Based on the existing pond size, it appears that the pond may detain flows generated by smaller storms only. Once the pond fills up, the flow enters the MHP at the west perimeter of the MHP via two (2) rock/grouted channels located on north and south sides of WWH MHP unit 9. This is the single outlet for the stormwater discharged from the Campground site into the WWH MHP. The following table summarizes the 10-year and the 100-year storm event flows discharged at the Outlet in existing condition. Please see Exhibit 1 and Exhibit-2 for the offsite drainage map and the existing condition onsite drainage map included in Appendix A.

Table 3-Existing Condition-Outlet Flow Summary

Storm Event	Flow Rate (cfs)
10-year	97
100-year	199

v) Proposed Condition-Unattenuated

The offsite flow patterns remain the same as in the existing condition. However, per COF, the runoff generated by the additional impervious area for future half street improvements of the adjacent ROWs has been included in the post developed hydrologic calculations and in the detention facility design. Curve numbers are revised for the drainage areas SUB-1B and SUB-2A to account for the future street improvements.

The campground intends to maintain the existing grades to the maximum possible extent except for the pond grading and grading for RV pads and roads. For the onsite drainage areas SUB-3A and SUB-3B, the curve numbers area was revised to account for the newly added impervious areas. Sub-3C is assumed to have commercial improvements in the future and thus appropriate curve numbers for future improvements are used to estimate runoff in the proposed condition. Again, the improvements in SUB-3C are not a part of this project. The proposed runoff is computed just to accommodate mitigation of the increased flow from this portion of the site. A separate drainage study or addendum will be prepared as and when needed to address improvements on this portion of the site in future. Please refer to the composite curve number calculations included in Appendix B. Post developed runoff calculations are performed to account for the newly added impervious areas and the future half street improvements of adjacent ROWs. The following table summarizes the 10-year and the 100-year storm events flows discharged at the Outlet in post developed unattenuated condition.

Table 4-Proposed Condition Unattenuated-Outlet Flow Summary

Storm Event	Flow Rate (cfs)
10-year	118
100-year	234

vi) Post-Developed Condition-Attenuated

The detention basin is proposed at the downstream end of the campground, along the east perimeter of the site. The proposed detention basin serves as a campground amenity by maintaining a body of water year-round. The pond provides mitigation to the increased flows due to the proposed Campground improvements, and also mitigates the offsite flows discharged into the WWH MHP by almost 72%. Please see Section 7 of the report for the detention basin design description. The following table summarizes the 10-year and the 100-year storm event flows discharged at the Outlet in post developed attenuated condition.

Table 5-Proposed Condition Attenuated-Outlet Flow Summary

Storm Event	Flow Rate (cfs)
10-year	37
100-year	55

7. DETENTION BASIN

The pond will have 4’ of dead storage at the bottom, with 8’ live storage above the permanent pool. It should be noted that the dead storage volume is not included in the pond routing calculations. The pond will have rock lined sides with Malapai boulders to mimic a natural stream/waterbody. Please see Appendix B for the detention volume calculations.

The flow from the proposed improvements will be routed to the LID basins first and then directed to the detention basin. Rock swales/channels are proposed to bring the flow to the detention basin along the existing drainage paths. The rock swales are also analyzed to ensure that the 100-year storm event is contained within the channel. Please see Appendix C for channel calculations. The following table summarizes the pond elevations and volume.

Table 6- Detention Basin Elevation and Volume Summary

Permanent Pool		Detention				Emergency Spillway	Freeboard min. (1 ft)
Bottom	Top	Bottom	Top	Vol. (ac-ft)	100-yr WSE	Elev.	Elev.
6988	6992	6992	7000	8.31	6998.5	6998.5	1.5

The Arizona Department of Water Resources (ADWR) defines “jurisdictional dam” as an artificial barrier for the impounding or diversion of water either 25 feet or more in height or having a storage capacity of more than 50 ac-ft. From the above table, the total height is 12’ and the embankment height is 8’ and the storage capacity is 8.31 ac-ft. Thus, the proposed detention basin is not categorized as a “jurisdictional dam”. The following chart from ADWR’s “Jurisdictional dam” criteria shows the height and the volume limits.

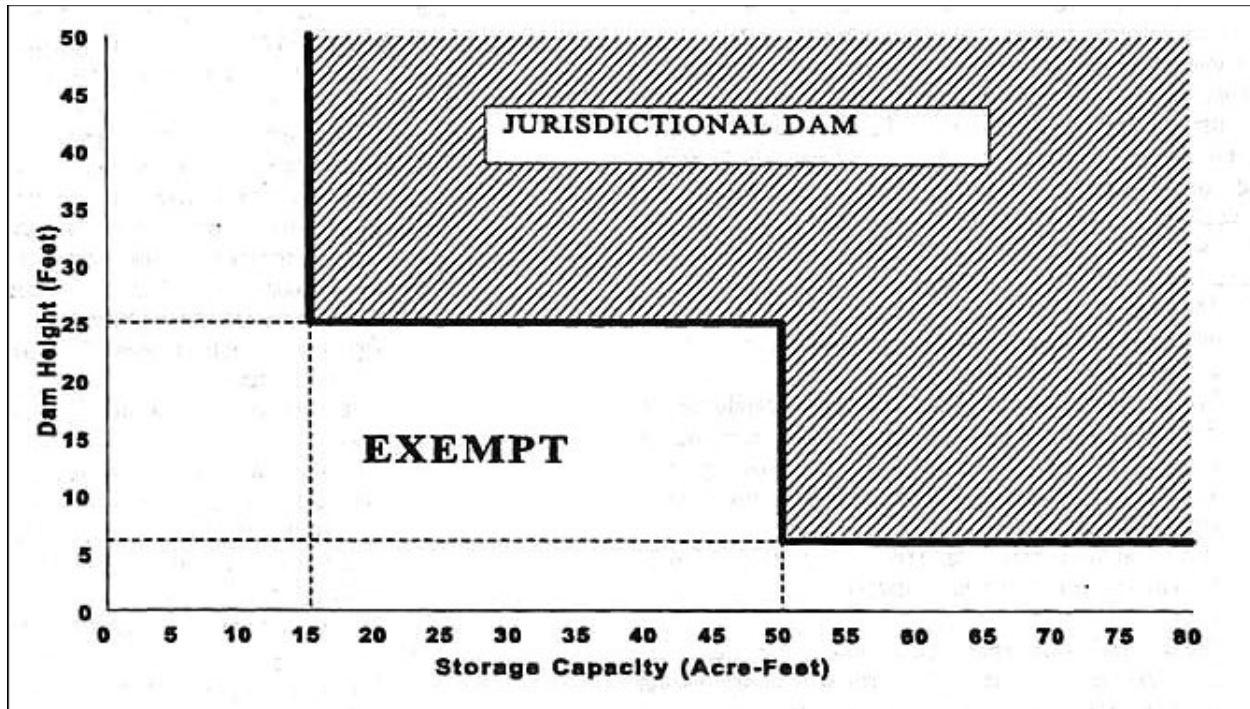


Figure 3: ADWR Dam Criteria Chart

i) Detention Embankment

The detention embankment is twelve (12) feet. As per the COF SWM manual section 8.4.6, a geotechnical engineering study and slope stability analysis is required for the embankments exceeding ten (10) feet. Thus, the embankment will be analyzed by a geotechnical engineer.

The top width of the embankment is eight (8) feet and is more than ½ of the height of the embankment per the COF SWM manual section 8.4.6.

ii) Outlet Facilities

Two (2) outlet pipes are proposed to discharge the detained volume. Both the outlet pipes are 21-inch cmpps and will have an invert elevation of 6,988', above the permanent pond elevation.

Outlet pipe-1 discharges flow into the existing south channel east of the basin. Outlet pipe-2 discharges flow into the existing north channel east of the basin. Safety gates will be proposed at the inlet and the outlet ends of the pipes to capture debris and to limit access through the pipes. Please see Appendix C for the outlet flow calculations.

The combined 100-year discharge from the outlet pipes is about 62 cfs which is slightly higher than the 100-year outflow from the detention basin (55 cfs). Thus, the pipes are sized adequately to convey the 100-year outflow released from the detention basin.

iii) Emergency Spillway

Per COF SWDM Section 8.4.6.1, emergency overflow facilities/spillways are required for instances where the primary outlet structure fails or storm events greater than the design capacity

occur. The emergency overflow shall be designed to pass the 100-year peak discharge at a minimum.

Since the flow from the subject site discharges into two (2) existing channels in Wildwood Hills Mobile Home Park, two (2) emergency overflow weirs are proposed to convey the 100-year flow. The emergency overflow weirs are sized to discharge the 100-year inflow released into the detention basin (234 cfs). The total flow is distributed between both the spillways. Thus, each spillway is designed to discharge about 118 cfs. Shallow rectangular concrete flumes are proposed on the slope of the embankment to carry the flow from the emergency overflow weirs and convey it to the existing channels. Please see Appendix C for weir sizing and concrete flume sizing calculations.

iv) Maintenance Road

A 10' access drive is proposed to provide access into the pond for maintenance. The pond will be maintained privately by the property owner. However, easement is provided to the City to access the pond.

8. HYDRAULICS

i) Culvert Crossings

Culvert crossings are proposed under access roads and trails. Per COF SWDM manual section 5.2.1, culverts under local streets are designed for a 25-year storm event. While the access roads are private roads, the culvert crossings are designed for 100-year storm event (with no overtopping of roads/trails) with exception to culverts 4 and 5 which are designed for 25-year storm event. Safety gates are proposed at the culvert ends to restrict entry into the culverts.

Culvert analysis is performed for both 25-year and 100-year storm events to ensure the Hw/D (Headwater depth/diameter to be less than 1.50) criteria is met per COF SWDM section 5.2.3. Please refer to Appendix C for culvert analysis calculations.

The culverts daylight into either riprap-lined or gabion-lined channels which provide erosion protection. Riprap protection is proposed at the culvert inlets where needed.

The following table summarizes the culvert flows, sizes and Hw/D for 25-yr and 100-yr storm events.

Table 7 : Culvert Summary Table

Culvert ID	Contributing Catchment	Pipe Size	Q25 (cfs)	Hw/D 25 yr	Q100 (cfs)	Hw/D 100 yr
BC1	35% of 3B	1-24" cmp	11	0.96	15	1.21
BC2	3B+2A+1	2-36" cmp	66	1.02	90	1.29
BC3	Sub-2	1-24" cmp	8	0.75	12	1.01
BC4	CP-30	1-9'x3' RCBC	99	0.92	137	1.19
1	Sub-2A+Sub-1	2-30" cmp	36	0.88	48	1.1
2	Sub-2	1-24" cmp	8	0.76	12	1.01
4	65% of 3B	2-24" cmp	20	0.85	27	1.07
5	35% of 3B	2-18" cmp	11	0.98	15	1.24
6	35% of 3B	2-18" cmp	11	0.91	15	1.17

ii) Channels

Channels are proposed to convey offsite flows released into the site to the detention basin and from LID basins to the detention basins. Per COF SWDM Section 4.3, the channels are designed for 25-year storm event and checked for 100-year storm event. The site's natural terrain is steep which leads to steep channels with high velocities. Due to the high velocity, the channels are proposed to be gabion lined with D50=6" rock. Stepped weir structures are adopted to break the natural steep grades and to slow down the flows.

Following is the summary of the channel flow rates.

Table 8: Channel Flow Rate Summary

Channel ID	Contributing Catchment	Q25 (cfs)	Q100 (cfs)
A	Sub-2	8	12
B	Sub-2A+Sub-1	36	48
C	Sub-3B	30	42
D	35% of 3B	11	15
E	CP-30	99	137
F	Sub-3A	9	14

9. SUMMARY AND CONCLUSIONS

- The proposed stormwater management facilities satisfy the rate control and the LID/ROCV requirement. Rate control is provided for the increased flows due to proposed improvements. In addition, mitigation is provided for offsite flows to alleviate flooding on WWH MHP.
- While this serves as a Master Drainage Report for the entire site including the northwest parcel, the Phase I improvements are for the easterly 8-acre parcel. Any future improvements on the rest of the Campground site will be covered by a future addendum. The future improvements on the northwest parcel will have a separate addendum as and when improvements will be proposed in future on that parcel. Since all of the site discharges into the natural low point where the proposed detention is planned, the pond is designed to address mitigation for increased flows due to proposed and future improvements along with additional mitigation to alleviate WWH MHP historic flooding.
- Though the proposed flow attenuation facilities do not completely reduce the flows to the capacity of existing drainage/conveyance facilities in WWH MHP, the flows are significantly lower than the existing condition flows (72% reduction).
- All the impervious areas are directed to the proposed LID basins to address the ROCV requirements to the maximum possible extent.
- The outlet location and the flow pattern in post developed condition is the same as pre-developed condition.
- Post developed flow rate released at the outlets is less than or equal to pre-developed flow rate.
- The drainage areas from the 2006 burn area use an existing burn condition for the curve numbers for the hydrologic analysis. This a conservative approach as the vegetation will eventually be re-established and the curve number will drop significantly.
- To reduce flows from the west of Woody Mountain Road to Wildwood Hills MHP, some areas of Timber Sky that naturally drain east will be routed west as recommended by the City with the Timber Sky improvements.
- The proposed detention basin is at the same location as the existing makeshift pond which is a natural concentration point with more than one inflow points. The proposed detention basin maintains the same flow pattern as in the existing condition. The permanent pond provides an additional site amenity.

10.REFERENCES

City of Flagstaff Stormwater Management Design Manual, City of Flagstaff Engineering Division, 2000

City of Flagstaff Low Impact Development Manual (January 2009)

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United States Army Corps Engineer's (USACE) Hydrologic Engineering Center software (HEC-1), Version 4.1

Hydraflow Express Extension for Autodesk AutoCAD Civil 3D by Autodesk, Inc.

Gabion structures, Maccaferri, Inc.

Presidio in Pines Drainage Report excerpts (December 2004)

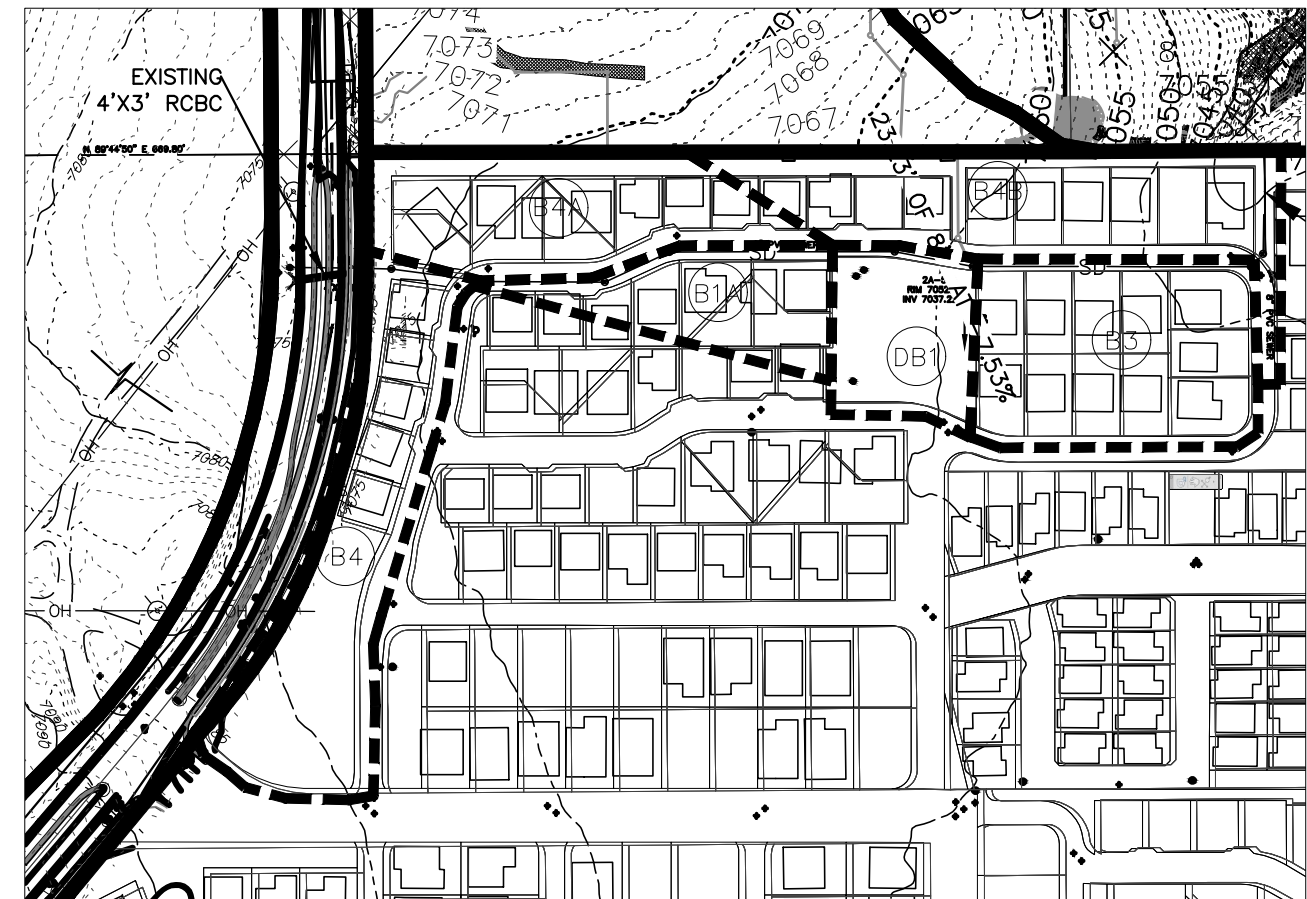
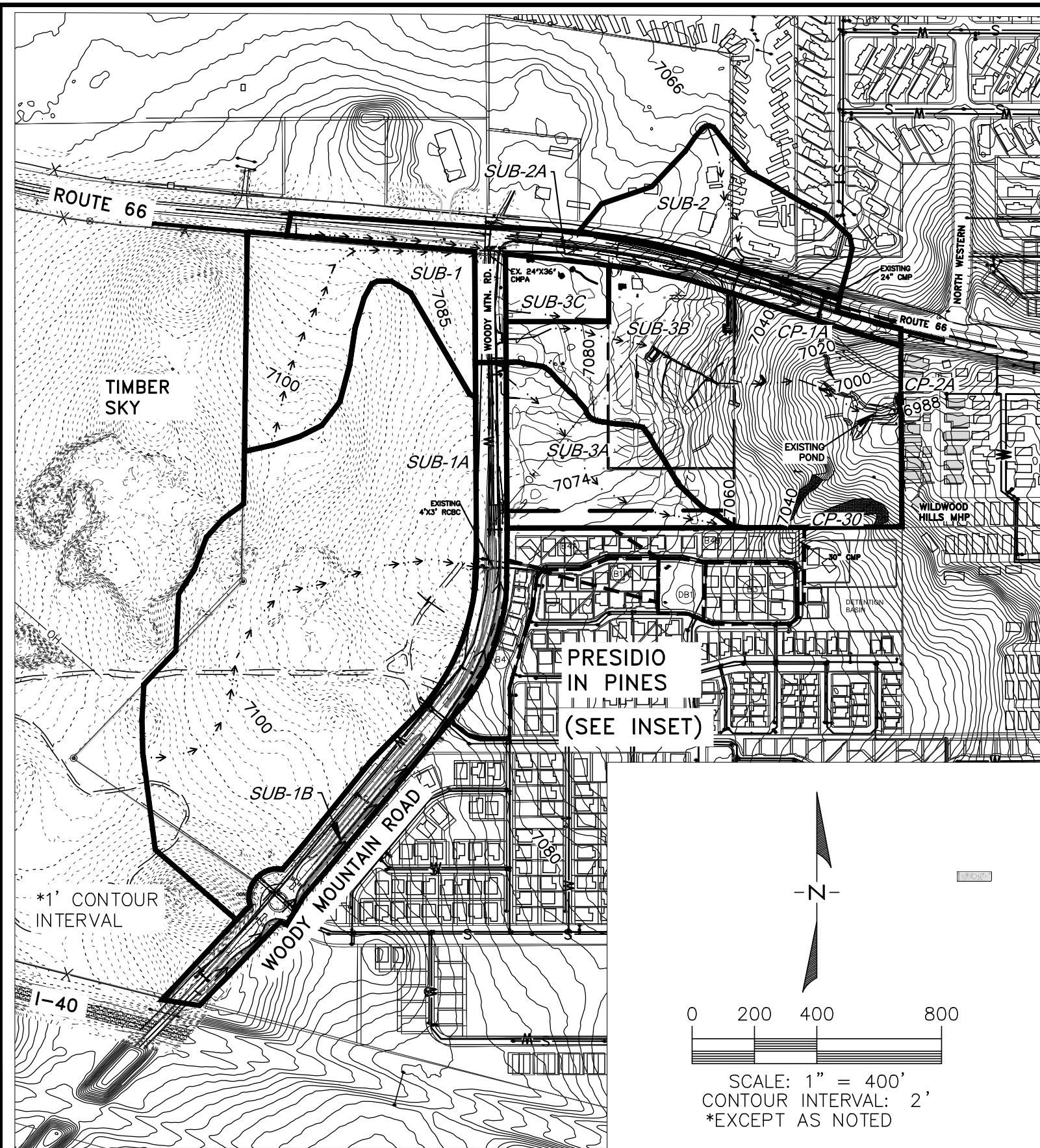
APPENDIX A

Exhibit 1- Drainage Area Map-Offsite Drainage Areas

Exhibit 2 - Drainage Area Map -Existing Conditions

Exhibit 3 - Drainage Area Map -Proposed Conditions

Exhibit 4 - Overall Plan



PRESIDIO IN THE PINES DRAINAGE AREAS

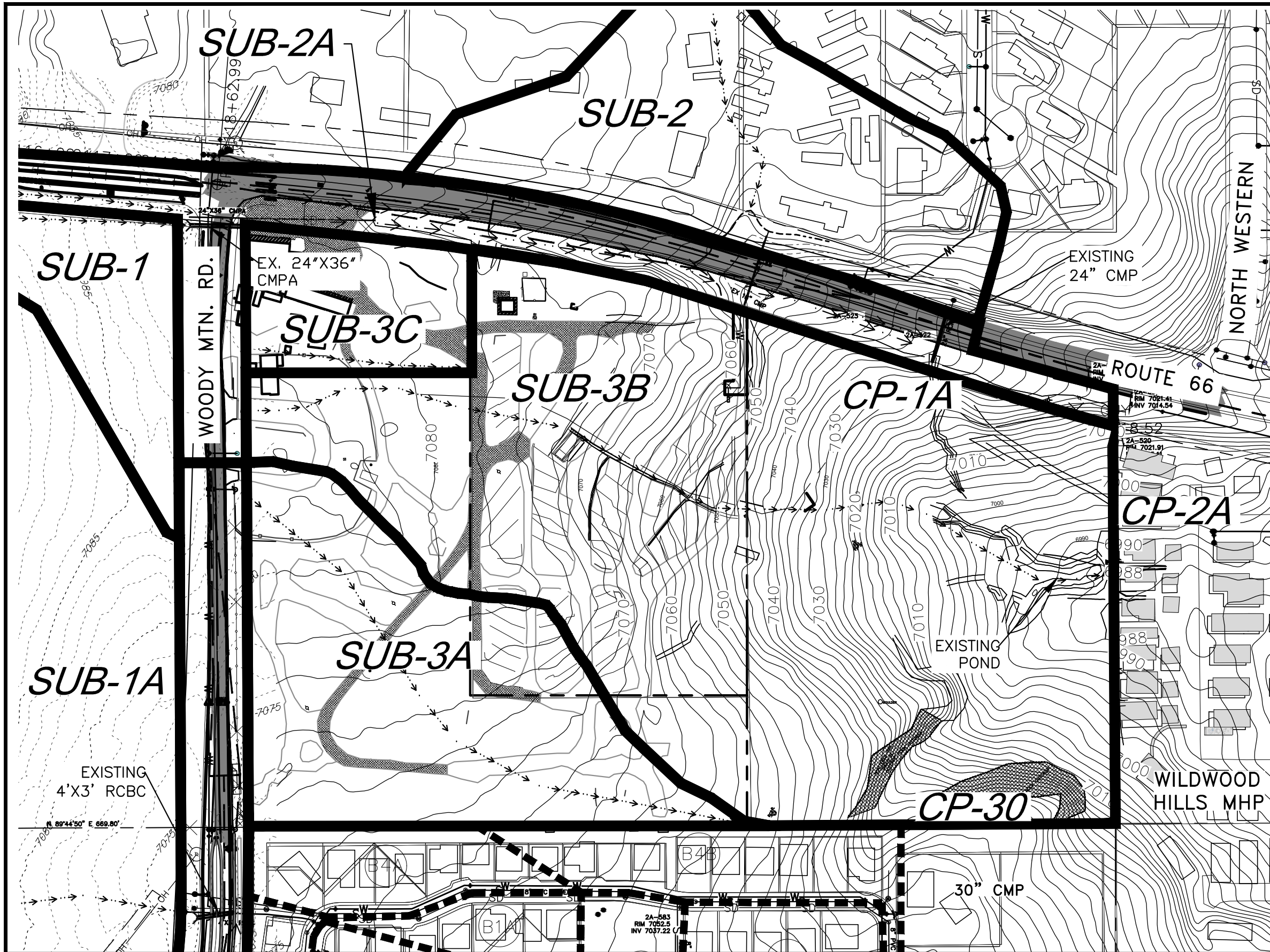
LEGEND

- SUB-1 DRAINAGE AREA ID
- DRAINAGE AREA LIMITS
- → → TRAVEL TIME PATH

DRAFTED BY: SK
 DATE: 06/24/19
 PROJ. NO.: 118044
 FN: 118044-Drainage

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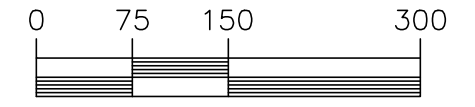
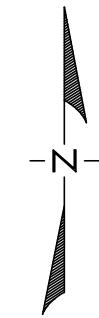
WOODY MOUNTAIN CAMPGROUND
 EXHIBIT 1-OFFSITE DRAINAGE AREA MAP



LEGEND

- SUB1 DRAINAGE AREA ID
- DRAINAGE AREA LIMITS
- TRAVEL TIME PATH

PLEASE SEE OFFSITE DRAINAGE AREA MAP FOR THE COMPLETE EXTENTS OF THE OFFSITE DRAINAGE AREAS.

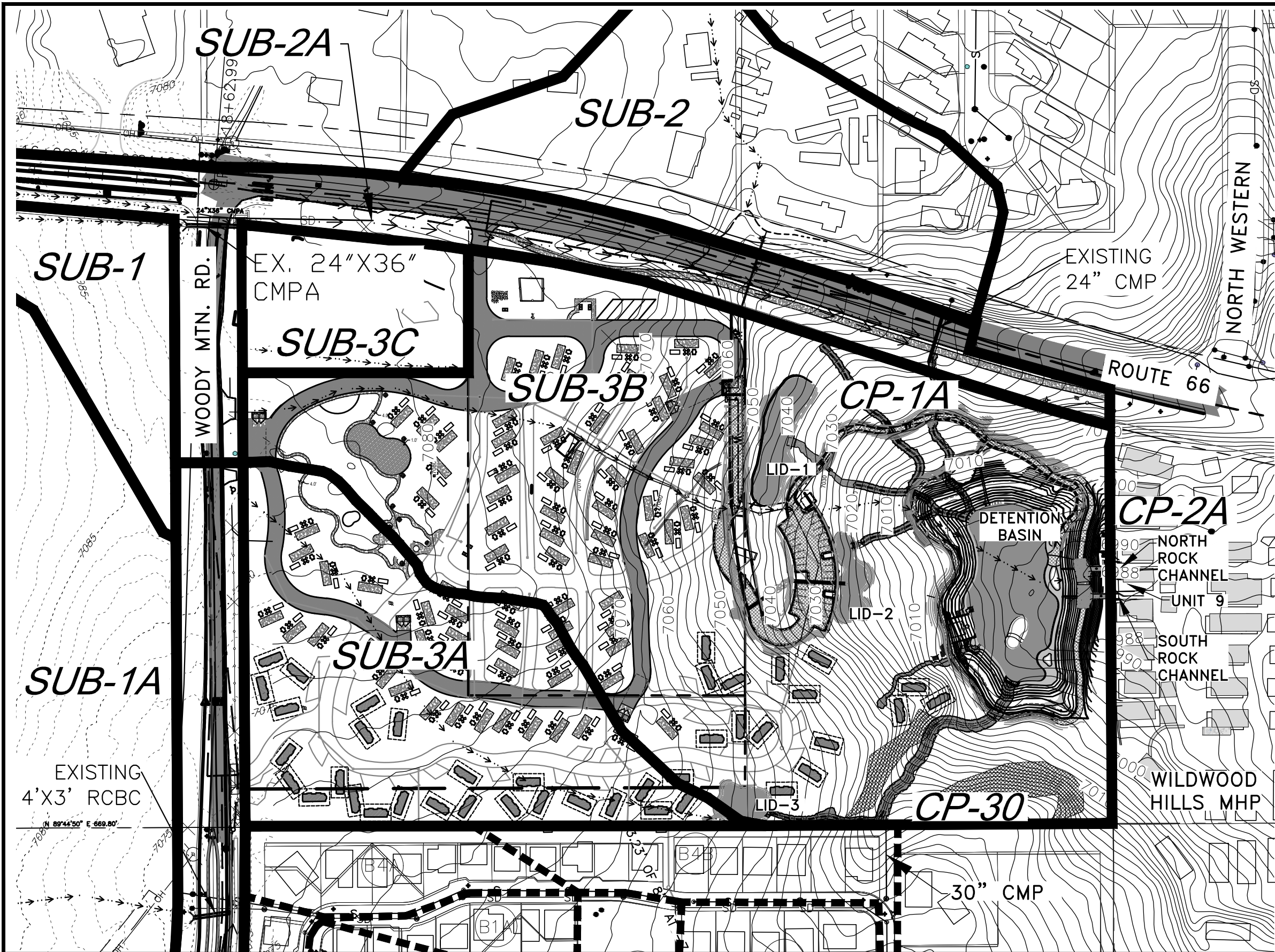


SCALE: 1" = 150'
CONTOUR INTERVAL: 1'

DRAFTED BY: SK
DATE: 07/15/2019
PROJ. NO.: 118044
FN: 118044 Drainage.dwg

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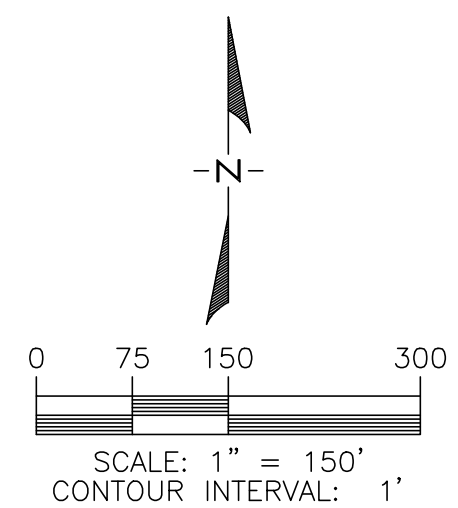
WOODY MOUNTAIN CAMPGROUND
EXHIBIT 2-DRAINAGE AREA MAP EXISTING CONDITION



- LEGEND**
- SUB 1 DRAINAGE AREA ID
 - DRAINAGE AREA LIMITS
 - TRAVEL TIME PATH

PLEASE SEE OFFSITE DRAINAGE AREA MAP FOR THE COMPLETE EXTENTS OF THE OFFSITE DRAINAGE AREAS.

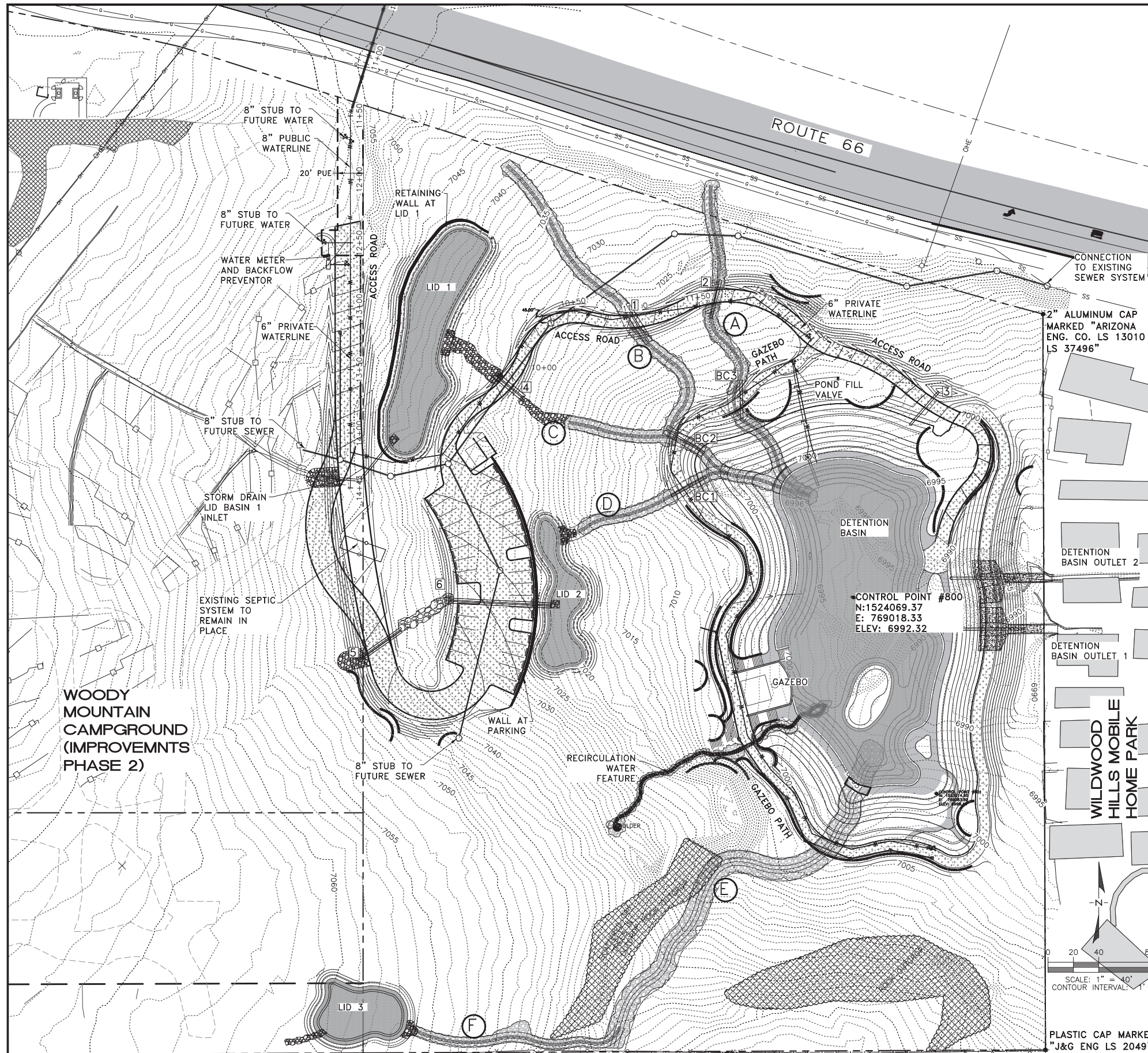
THE PHASE II IMPROVEMENTS ON THE CAMPGROUND ARE SHOWN FOR REFERENCE ONLY. PLEASE SEE EXHIBIT 4 FOR THE OVERALL PLAN THAT SHOWS THE PROPOSED IMPROVEMENTS IN PHASE I.



DRAFTED BY: SK
 DATE: 07/15/19
 PROJ. NO.: 118044
 FN: 118044-Drainage.dwg

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WOODY MOUNTAIN CAMPGROUND
 EXHIBIT 3-DRAINAGE AREA MAP PROPOSED CONDITION



CIVIL INDEX

- C1 OVERALL
- C2 NOTES AND QUANTITIES
- C3 DETAILS
- C4 DETAILS
- C5 GRADING PLAN - ACCESS ROAD
- C6 GRADING PLAN - ACCESS ROAD
- C7 GRADING PLAN - GAZEBO PATH
- C8 UTILITY PLAN
- C9 UTILITY PLAN
- C10 UTILITY PLAN
- C11 FILL STATION
- C12 LID BASINS
- C13 STORM DRAIN - ACCESS ROAD
- C14 DETENTION BASIN CONTROL
- C15 DETENTION BASIN OUTLETS
- C16 RETAINING WALL PARKING
- C17 RETAINING WALL AT LID 1
- C18 SWPPP
- C19 SWPPP DETAILS

LEGEND

- (D) CHANNEL NAME
- (6) CULVERT NAME

EARTHWORK QUANTITIES (CY)

	DETENTION BASIN	LID1	LID2	LID3	ACCESS ROAD	GAZEBO ROAD	TOTAL
EXCAVATION	9,787	1,166	294	360	1,176	516	13,300
EMBANKMENT	3,394	35	90	12	3,084	62	6,677

BY SIGNING THESE PLANS, THE DESIGNER OF THE LANDSCAPING PLANS CONFIRMS THAT THESE GRADING PLANS HAVE BEEN REVIEWED, IS AWARE OF THE SCOPE OF THE PROJECT, AND HAS IDENTIFIED AND ADDRESSED ANY POTENTIAL CONFLICTS BETWEEN THE GRADING AND LANDSCAPING PLANS.

LANDSCAPE DESIGNER _____ DATE _____

WOODY MOUNTAIN CAMPGROUND (IMPROVEMENTS PHASE 2)

WILDWOOD HILLS MOBILE HOME PARK

ROUTE 66



REVISIONS:

NO.	DATE	DESCRIPTION



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WOODY MTN. CAMPGROUND
 PHASE 1

OVERALL PLAN

HOR SCALE: 1"=30'
VERT SCALE: NA
DATE: 7/10/19
PROJECT NO.: 118044
AGENCY NO.: PZ18-00210
SHEET NO.: C1 OF 19

DESIGNED BY: AAS
 DRAFTED BY: AAS
 CHECKED BY: RLS

118044

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WOODY MTN. CAMPGROUND
 PHASE 1
 CONSTRUCTION PLANS

APPENDIX B

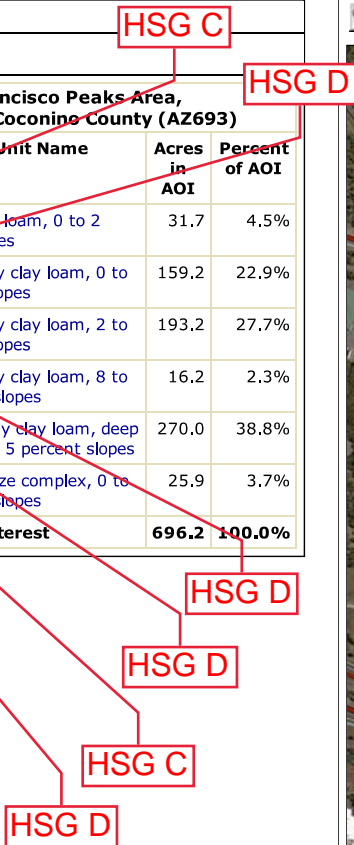
- Soils Information
- Composite Curve Number Calculations
- Time of Concentration Calculations
- Drainage Areas Summary Table
- HEC-1 Output-Existing Condition 10-year Storm Event
- HEC-1 Output-Existing Condition 100-year Storm Event
- HEC-1 Output-Proposed Condition Unattenuated 10-year Storm Event
- HEC-1 Output-Proposed Condition Unattenuated 100-year Storm Event
- HEC-1 Output-Proposed Condition Attenuated 10-year Storm Event
- HEC-1 Output-Proposed Condition Attenuated 100-year Storm Event
- Summary of Impervious Area and ROCV Calculations

Search

Map Unit Legend

**Oak Creek-San Francisco Peaks Area,
Arizona, Part of Coconino County (AZ693)**

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
1	Jacques clay loam, 0 to 2 percent slopes	31.7	4.5%
2	Brolliar stony clay loam, 0 to 2 percent slopes	159.2	22.9%
2A	Brolliar stony clay loam, 2 to 8 percent slopes	193.2	27.7%
2B	Brolliar stony clay loam, 8 to 30 percent slopes	16.2	2.3%
12	Brolliar cobbly clay loam, deep variant, 0 to 5 percent slopes	270.0	38.8%
15A	Tortugas-Daze complex, 0 to 15 percent slopes	25.9	3.7%
Totals for Area of Interest		696.2	100.0%



Soil Map

Scale (not to scale)



Warning: Soil Map may not be valid at this scale.

You have zoomed in beyond the scale at which the soil map for this area is intended to be used. Mapping of soils is done at a particular scale. The soil your AOI were mapped at 1:24,000. The design of map units and the level of detail shown in the resulting soil map are dependent on that map scale. Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps areas of contrasting soils that could have been shown at a more detailed scale.

Soil Data Available			
Name	Area Symbol	Data Availability	Version
Oak Creek-San Francisco Peaks Area, Arizona, Part of Coconino County	AZ693	Tabular and Spatial, incomplete	Survey Area: Version 5, Sep 14, 2014 Tabular: Version 4, Sep 14, 2014 Spatial: Version 2, Dec 17, 2013

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Oak Creek-San Francisco Peaks Area, Arizona, Part of Coconino County

1—Jacques clay loam, 0 to 2 percent slopes

Map Unit Setting

National map unit symbol: 1vhjq
Elevation: 6,580 to 7,080 feet
Mean annual precipitation: 18 to 24 inches
Mean annual air temperature: 43 to 49 degrees F
Frost-free period: 90 to 115 days
Farmland classification: Not prime farmland

Map Unit Composition

Jacques and similar soils: 100 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Jacques

Setting

Landform: Drainageways, valleys
Landform position (two-dimensional): Summit
Landform position (three-dimensional): Dip
Down-slope shape: Linear
Across-slope shape: Linear
Parent material: Mixed alluvium

Typical profile

H1 - 0 to 16 inches: clay loam
H2 - 16 to 60 inches: clay

Properties and qualities

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Well drained
Runoff class: Medium
Capacity of the most limiting layer to transmit water (Ksat):
Moderately low to moderately high (0.06 to 0.20 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: Frequent
Frequency of ponding: None
Available water storage in profile: High (about 9.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 6c
Hydrologic Soil Group: C

Hydric soil rating: No

Data Source Information

Soil Survey Area: Oak Creek-San Francisco Peaks Area, Arizona, Part of
Coconino County

Survey Area Data: Version 5, Sep 14, 2014

Oak Creek-San Francisco Peaks Area, Arizona, Part of Coconino County

2—Brolliar stony clay loam, 0 to 2 percent slopes

Map Unit Setting

National map unit symbol: 1vhjr
Elevation: 6,790 to 7,420 feet
Mean annual precipitation: 18 to 24 inches
Mean annual air temperature: 43 to 49 degrees F
Frost-free period: 90 to 115 days
Farmland classification: Not prime farmland

Map Unit Composition

Brolliar and similar soils: 100 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Brolliar

Setting

Landform: Plains
Landform position (two-dimensional): Summit
Landform position (three-dimensional): Interfluve
Down-slope shape: Convex
Across-slope shape: Convex
Parent material: Residuum weathered from basalt

Typical profile

H1 - 0 to 3 inches: stony clay loam
H2 - 3 to 30 inches: clay
R - 30 to 40 inches: bedrock

Properties and qualities

Slope: 0 to 2 percent
Percent of area covered with surface fragments: 15.0 percent
Depth to restrictive feature: 20 to 40 inches to lithic bedrock
Natural drainage class: Well drained
Runoff class: Medium
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.06 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum in profile: 1 percent
Available water storage in profile: Low (about 4.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 5c
Hydrologic Soil Group: D

Hydric soil rating: No

Data Source Information

Soil Survey Area: Oak Creek-San Francisco Peaks Area, Arizona, Part of Coconino County

Survey Area Data: Version 5, Sep 14, 2014

Oak Creek-San Francisco Peaks Area, Arizona, Part of Coconino County

2A—Brolliar stony clay loam, 2 to 8 percent slopes

Map Unit Setting

National map unit symbol: 1vhjs
Elevation: 6,620 to 7,540 feet
Mean annual precipitation: 18 to 24 inches
Mean annual air temperature: 43 to 49 degrees F
Frost-free period: 90 to 115 days
Farmland classification: Not prime farmland

Map Unit Composition

Brolliar and similar soils: 100 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Brolliar

Setting

Landform: Plains
Landform position (two-dimensional): Shoulder, summit
Landform position (three-dimensional): Interfluve
Down-slope shape: Convex
Across-slope shape: Convex
Parent material: Residuum weathered from basalt

Typical profile

H1 - 0 to 3 inches: stony clay loam
H2 - 3 to 30 inches: clay
R - 30 to 40 inches: bedrock

Properties and qualities

Slope: 2 to 8 percent
Percent of area covered with surface fragments: 15.0 percent
Depth to restrictive feature: 20 to 40 inches to lithic bedrock
Natural drainage class: Well drained
Runoff class: High
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.06 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum in profile: 1 percent
Available water storage in profile: Low (about 4.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 5c
Hydrologic Soil Group: D

Hydric soil rating: No

Data Source Information

Soil Survey Area: Oak Creek-San Francisco Peaks Area, Arizona, Part of Coconino County

Survey Area Data: Version 5, Sep 14, 2014

Oak Creek-San Francisco Peaks Area, Arizona, Part of Coconino County

2B—Brolliar stony clay loam, 8 to 30 percent slopes

Map Unit Setting

National map unit symbol: 1vhjt
Elevation: 6,760 to 7,550 feet
Mean annual precipitation: 18 to 24 inches
Mean annual air temperature: 43 to 49 degrees F
Frost-free period: 90 to 115 days
Farmland classification: Not prime farmland

Map Unit Composition

Brolliar and similar soils: 100 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Brolliar

Setting

Landform: Hills
Landform position (two-dimensional): Backslope
Landform position (three-dimensional): Side slope
Down-slope shape: Convex
Across-slope shape: Convex
Parent material: Residuum weathered from basalt

Typical profile

H1 - 0 to 3 inches: stony clay loam
H2 - 3 to 30 inches: clay
R - 30 to 40 inches: bedrock

Properties and qualities

Slope: 8 to 30 percent
Percent of area covered with surface fragments: 20.0 percent
Depth to restrictive feature: 20 to 40 inches to lithic bedrock
Natural drainage class: Well drained
Runoff class: High
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.06 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum in profile: 1 percent
Available water storage in profile: Low (about 4.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 5c
Hydrologic Soil Group: D

Hydric soil rating: No

Data Source Information

Soil Survey Area: Oak Creek-San Francisco Peaks Area, Arizona, Part of Coconino County

Survey Area Data: Version 5, Sep 14, 2014

Oak Creek-San Francisco Peaks Area, Arizona, Part of Coconino County

12—Brolliar cobbly clay loam, deep variant, 0 to 5 percent slopes

Map Unit Setting

National map unit symbol: 1vhk4
Elevation: 6,870 to 7,560 feet
Mean annual precipitation: 18 to 24 inches
Mean annual air temperature: 43 to 49 degrees F
Frost-free period: 90 to 115 days
Farmland classification: Not prime farmland

Map Unit Composition

Brolliar, deep, and similar soils: 100 percent
*Estimates are based on observations, descriptions, and transects of
the mapunit.*

Description of Brolliar, Deep

Setting

Landform: Plains
Landform position (two-dimensional): Summit
Landform position (three-dimensional): Interfluve
Down-slope shape: Convex
Across-slope shape: Convex
Parent material: Residuum weathered from basalt

Typical profile

H1 - 0 to 3 inches: cobbly clay loam
H2 - 3 to 60 inches: clay

Properties and qualities

Slope: 0 to 5 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Well drained
Runoff class: Medium
Capacity of the most limiting layer to transmit water (Ksat):
Moderately low to moderately high (0.06 to 0.20 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum in profile: 1 percent
Available water storage in profile: Moderate (about 8.9 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 5c
Hydrologic Soil Group: C

Hydric soil rating: No

Data Source Information

Soil Survey Area: Oak Creek-San Francisco Peaks Area, Arizona, Part of
Coconino County

Survey Area Data: Version 5, Sep 14, 2014

Oak Creek-San Francisco Peaks Area, Arizona, Part of Coconino County

15A—Tortugas-Daze complex, 0 to 15 percent slopes

Map Unit Setting

National map unit symbol: 1vhkb
Elevation: 6,670 to 7,090 feet
Mean annual precipitation: 18 to 24 inches
Mean annual air temperature: 43 to 49 degrees F
Frost-free period: 90 to 115 days
Farmland classification: Not prime farmland

Map Unit Composition

Tortugas and similar soils: 55 percent
Daze and similar soils: 45 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Tortugas

Setting

Landform: Hills
Landform position (two-dimensional): Backslope, summit
Landform position (three-dimensional): Side slope, interfluve
Down-slope shape: Convex
Across-slope shape: Convex
Parent material: Alluvium and/or residuum weathered from limestone

Typical profile

H1 - 0 to 3 inches: cobbly loam
H2 - 3 to 14 inches: very cobbly loam
R - 14 to 24 inches: bedrock

Properties and qualities

Slope: 0 to 15 percent
Depth to restrictive feature: 6 to 20 inches to lithic bedrock
Natural drainage class: Well drained
Runoff class: Medium
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately high (0.00 to 0.60 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum in profile: 50 percent
Available water storage in profile: Very low (about 1.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 6c
Hydrologic Soil Group: D

Hydric soil rating: No

Description of Daze

Setting

Landform: Hills

Landform position (two-dimensional): Summit, shoulder

Landform position (three-dimensional): Interfluve

Down-slope shape: Convex

Across-slope shape: Convex

Parent material: Residuum weathered from limestone and sandstone

Typical profile

H1 - 0 to 3 inches: fine sandy loam

H2 - 3 to 7 inches: clay loam

H3 - 7 to 18 inches: clay

R - 18 to 28 inches: bedrock

Properties and qualities

Slope: 0 to 15 percent

Depth to restrictive feature: 10 to 20 inches to lithic bedrock

Natural drainage class: Well drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.06 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Available water storage in profile: Very low (about 2.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6c

Hydrologic Soil Group: D

Hydric soil rating: No

Data Source Information

Soil Survey Area: Oak Creek-San Francisco Peaks Area, Arizona, Part of Coconino County

Survey Area Data: Version 5, Sep 14, 2014

**OAK CREEK FLOOD WARNING SYSTEM
HYDROLOGY REPORT**

**ARIZONA DEPARTMENT OF WATER RESOURCES
ENGINEERING DIVISION
FLOOD MANAGEMENT SECTION**

**TR 90 - 4
SEPTEMBER 1990**

Table 2
 RUNOFF CURVE NUMBERS

Cover Type	Cover Condition	Hydrologic Soil Group	Curve Number
BARE ROCK	NO CONDITION		94
RIVERWASH	NO CONDITION		53
CINDERS/LAVA	POOR 0 - 30%		53
SPRUCE - FIR	GOOD 70 - 100%	B	41
MIXED CONIFER	GOOD 70 - 100%	B	41
MIXED CONIFER	GOOD 70 - 100%	C	51
MIXED CONIFER	FAIR 30 - 70%	A	48
MIXED CONIFER	FAIR 30 - 70%	B	53
MIXED CONIFER	FAIR 30 - 70%	C	65
MIXED CONIFER	FAIR 30 - 70%	D	75
MIXED CONIFER	POOR 0 - 30%	A	60
MIXED CONIFER	POOR 0 - 30%	B	71
MIXED CONIFER	POOR 0 - 30%	C	80
MIXED CONIFER	POOR 0 - 30%	D	87
PONDEROSA PINE	GOOD 70 - 100%	B	41
PONDEROSA PINE	GOOD 70 - 100%	C	51
PONDEROSA PINE	FAIR 30 - 70%	A	48
PONDEROSA PINE	FAIR 30 - 70%	B	53
PONDEROSA PINE	FAIR 30 - 70%	C	65
PONDEROSA PINE	FAIR 30 - 70%	D	75
PONDEROSA PINE	POOR 0 - 30%	B	71
PONDEROSA PINE	POOR 0 - 30%	C	80
PINON - JUNIPER	GOOD 70 - 100%	B	41
PINON - JUNIPER	GOOD 70 - 100%	C	61
PINON - JUNIPER	GOOD 70 - 100%	D	71
PINON - JUNIPER	FAIR 30 - 70%	A	40
PINON - JUNIPER	FAIR 30 - 70%	B	58
PINON - JUNIPER	FAIR 30 - 70%	C	73
PINON - JUNIPER	FAIR 30 - 70%	D	80
PINON - JUNIPER	POOR 0 - 30%	A	62
PINON - JUNIPER	POOR 0 - 30%	B	75
PINON - JUNIPER	POOR 0 - 30%	C	85
PINON - JUNIPER	POOR 0 - 30%	D	89
CHAPARRAL	GOOD 70 - 100%	B	52
CHAPARRAL	GOOD 70 - 100%	C	68
CHAPARRAL	GOOD 70 - 100%	D	78
CHAPARRAL	FAIR 30 - 70%	B	65
CHAPARRAL	FAIR 30 - 70%	C	77
CHAPARRAL	FAIR 30 - 70%	D	85
CHAPARRAL	POOR 0 - 30%	B	78
CHAPARRAL	POOR 0 - 30%	C	86
CHAPARRAL	POOR 0 - 30%	D	91
GRASSLAND	GOOD 70 - 100%	B	48
GRASSLAND	GOOD 70 - 100%	C	60
GRASSLAND	GOOD 70 - 100%	D	70
GRASSLAND	FAIR 30 - 70%	B	61
GRASSLAND	FAIR 30 - 70%	C	72
GRASSLAND	FAIR 30 - 70%	D	80
GRASSLAND	POOR 0 - 30%	B	74
GRASSLAND	POOR 0 - 30%	C	82
GRASSLAND	POOR 0 - 30%	D	89
FOREST PARK	FAIR 30 - 70%	A	55
FOREST PARK	FAIR 30 - 70%	C	69
FOREST PARK	POOR 0 - 30%	B	74
FOREST PARK	POOR 0 - 30%	D	89
DESERT GRASSLAND	GOOD 70 - 100%	B	62
DESERT GRASSLAND	GOOD 70 - 100%	C	74
DESERT GRASSLAND	GOOD 70 - 100%	D	85
DESERT GRASSLAND	FAIR 30 - 70%	B	71
DESERT GRASSLAND	FAIR 30 - 70%	C	81
DESERT GRASSLAND	FAIR 30 - 70%	D	89
DESERT GRASSLAND	POOR 0 - 30%	B	80
DESERT GRASSLAND	POOR 0 - 30%	C	87
DESERT GRASSLAND	POOR 0 - 30%	D	93
SONORA DESERT	GOOD 70 - 100%	A	49
SONORA DESERT	GOOD 70 - 100%	B	68
SONORA DESERT	GOOD 70 - 100%	C	79
SONORA DESERT	GOOD 70 - 100%	D	84
SONORA DESERT	FAIR 30 - 70%	A	55
SONORA DESERT	FAIR 30 - 70%	B	72
SONORA DESERT	FAIR 30 - 70%	C	81
SONORA DESERT	FAIR 30 - 70%	D	86
SONORA DESERT	POOR 0 - 30%	A	63
SONORA DESERT	POOR 0 - 30%	B	77
SONORA DESERT	POOR 0 - 30%	C	85
SONORA DESERT	POOR 0 - 30%	D	88
RIPARIAN	GOOD 70 - 100%	B	57
RIPARIAN	GOOD 70 - 100%	C	63
RIPARIAN	FAIR 30 - 70%	A	55
RIPARIAN	FAIR 30 - 70%	C	68
RIPARIAN SCRUB	FAIR 30 - 70%	A	53
MEADOW	GOOD 70 - 100%	D	70

Table 9-5 Runoff curve numbers for urban areas ^{1/}

Cover description cover type and hydrologic condition	Average percent impervious area ^{2/}	-- CN for hydrologic soil group --			
		A	B	C	D
Fully developed urban areas (vegetation established)					
Open space (lawns, parks, golf courses, cemeteries, etc.) ^{3/}					
Poor condition (grass cover < 50%)		68	79	86	89
Fair condition (grass cover 50% to 75%)		49	69	79	84
Good condition (grass cover > 75%)		39	61	74	80
Impervious areas:					
Paved parking lots, roofs, driveways, etc. (excluding right-of-way)		98	98	98	98
Streets and roads:					
Paved; curbs and storm sewers (excluding right-of-way)		98	98	98	98
Paved; open ditches (including right-of-way)		83	89	92	93
Gravel (including right-of-way)		76	85	89	91
Dirt (including right-of-way)		72	82	87	89
Western desert urban areas:					
Natural desert landscaping (pervious areas only) ^{4/}		63	77	85	88
Artificial desert landscaping (impervious weed barrier, desert shrub with 1- to 2-inch sand or gravel mulch and basin borders)		96	96	96	96
Urban districts:					
Commercial and business	85	89	92	94	95
Industrial	72	81	88	91	93
Residential districts by average lot size:					
1/8 acre or less (town houses)	65	77	85	90	92
1/4 acre	38	61	75	83	87
1/3 acre	30	57	72	81	86
1/2 acre	25	54	70	80	85
1 acre	20	51	68	79	84
2 acres	12	46	65	77	82
Developing urban areas					
Newly graded areas (pervious areas only, no vegetation)		77	86	91	94

1/ Average runoff condition, and $I_a = 0.2S$.

2/ The average percent impervious area shown was used to develop the composite CNs. Other assumptions are as follows: impervious areas are directly connected to the drainage system, impervious areas have a CN of 98, and pervious areas are considered equivalent to open space in good hydrologic condition.

3/ CNs shown are equivalent to those of pasture. Composite CNs may be computed for other combinations of open space type.

4/ Composite CNs for natural desert landscaping should be computed using figures 9-3 or 9-4 based on the impervious area percentage (CN=98) and the pervious area CN. The pervious area CNs are assumed equivalent to desert shrub in poor hydrologic condition.

Sub-1

Sheet Flow

Input Data	
Elev Start [ft]	7106
Elev End [ft]	7105
Length [ft]	70
n (Short Grass)	0.15
OUTPUT	
S [ft/ft]	0.01
Tt [hr]	0.178

Shallow Concentrated Flow

Unpaved	
Elev Start [ft]	7105
Elev End [ft]	7095
Length [ft]	335
OUTPUT	
S [ft/ft]	0.0299
V [ft/s]	2.79
Tt [min]	2.00
Tt [hr]	0.033

Open Channel Flow

INPUT DATA:	
Elev Start [ft]	7095
Elev End [ft]	7077
Length [ft]	695
Manning's n	0.040
Channel Slope [ft/ft]	0.0259
OUTPUT	
Area [sf]	23.50
Wetted Perimeter [ft]	41.06
Hydraulic Radius	0.57
Velocity [fps]	4.12
Tt [min]	2.81
Tt [hr]	0.047

Tc [hr]	0.258
Tc [min]	15.47
SCS Lag [hr]	0.155

Sub-1A

Sheet Flow

Input Data	
Elev Start [ft]	7113
Elev End [ft]	7111
Length [ft]	98
n (short grass)	0.15
OUTPUT	
S [ft/ft]	0.02
Tt [hr]	0.202

Shallow Concentrated Flow

Unpaved	
Elev Start [ft]	7111
Elev End [ft]	7098
Length [ft]	561
Output	
S [ft/ft]	0.0232
V [ft/s]	2.46
Tt [min]	3.81
Tt [hr]	0.063

Open Channel Flow

INPUT DATA:	
Elev Start [ft]	7098
Elev End [ft]	7070
Length [ft]	904
Manning's n	0.040
Channel Slope [ft/ft]	0.0310
Depth [ft]	1.00
OUTPUT DATA:	
Area [sf]	27.50
Wetted Perimeter [ft]	40.08
Hydraulic Radius	0.69
Velocity [fps]	5.09
Tt [min]	2.96
Tt [hr]	0.049

Tc [hr]	0.314
Tc [min]	18.87
SCS Lag [hr]	0.189

Sub-1B

Sheet Flow

Input Data	
Elev Start [ft]	7131
Elev End [ft]	7130
Length [ft]	36
n (Asphalt)	0.011
OUTPUT	
S [ft/ft]	0.03
Tt [hr]	0.010

Shallow Concentrated Flow

Unpaved	
Elev Start [ft]	7130
Elev End [ft]	7115
Length [ft]	490
Output	
S [ft/ft]	0.0306
V [ft/s]	2.82
Tt [min]	2.89
Tt [hr]	0.048

Open Channel Flow

INPUT DATA:	
Elev Start [ft]	7115
Elev End [ft]	7076
Length [ft]	1219
Channel Slope [ft/ft]	0.0320
Depth [ft]	1.00
OUTPUT DATA:	
Area [sf]	2.25
Wetted Perimeter [ft]	4.03
Hydraulic Radius	0.56
Velocity [fps]	9.01
Tt [min]	2.26
Tt [hr]	0.038

Tc [hr]	0.096
Tc [min]	10.00 (Min. 10 min)
SCS Lag [hr]	0.100

Woody Mountain Campground

Sub-2A

Sheet Flow

Input Data	
Elev Start [ft]	7088
Elev End [ft]	7087
Length [ft]	35
n (Asphalt)	0.011
OUTPUT	
S [ft/ft]	0.03
Tt [hr]	0.010

Shallow Concentrated Flow

Unpaved	
Elev Start [ft]	7087
Elev End [ft]	7080
Length [ft]	674
Output	
S [ft/ft]	0.0104
V [ft/s]	1.64
Tt [min]	6.83
Tt [hr]	0.114

Open Channel Flow

INPUT DATA:	
Elev Start [ft]	7080
Elev End [ft]	7040
Length [ft]	945
Manning's n	0.020
Channel Slope [ft/ft]	0.0423
Depth [ft]	1.00
OUTPUT DATA:	
Area [sf]	16.00
Wetted Perimeter [ft]	27.09
Hydraulic Radius	0.59
Velocity [fps]	10.76
Tt [min]	1.46
Tt [hr]	0.024

Tc [hr]	0.148
Tc [min]	10.00 (Min. 10 min)
SCS Lag [hr]	0.100

Woody Mountain Campground

Sub-2

Sheet Flow

Input Data	
Elev Start [ft]	7072
Elev End [ft]	7069
Length [ft]	97
n (dense grasses)	0.24
OUTPUT	
S [ft/ft]	0.03
Tt [hr]	0.247

Shallow Concentrated Flow

Unpaved	
Elev Start [ft]	7069
Elev End [ft]	7068
Length [ft]	203
Output	
S [ft/ft]	0.0049
V [ft/s]	1.13
Tt [min]	2.99
Tt [hr]	0.050

Open Channel Flow

INPUT DATA:	
Elev Start [ft]	7068
Elev End [ft]	7060
Length [ft]	125
Manning's n	0.040
Channel Slope [ft/ft]	0.0640
Depth [ft]	1.00
OUTPUT DATA:	
Area [sf]	7.00
Wetted Perimeter [ft]	12.20
Hydraulic Radius	0.57
Velocity [fps]	6.49
Tt [min]	0.32
Tt [hr]	0.005

Tc [hr]	0.302
Tc [min]	18.11
SCS Lag [hr]	0.181

Woody Mountain Campground

Sub-3A Existing Condition

Sheet Flow

Input Data		
Elev Start [ft]		7083
Elev End [ft]		7081
Length [ft]		42
n (dense grasses)		0.24
OUTPUT		
S [ft/ft]		0.05
Tt [hr]		0.106

Shallow Concentrated Flow

Unpaved		
Elev Start [ft]		7081
Elev End [ft]		7050
Length [ft]		1056
Output		
S [ft/ft]		0.0294
V [ft/s]		2.76
Tt [min]		6.37
Tt [hr]		0.106

Tc [hr]	0.212
Tc [min]	12.74
Tc [min] used	15.00
Tc [hr] used	0.25
SCS Lag [hr]	0.150

Woody Mountain Campground

Sub-3B Existing Condition

Sheet Flow

Input Data	
Elev Start [ft]	7082.6
Elev End [ft]	7082
Length [ft]	95
n (Dense Grasses)	0.25
OUTPUT	
S [ft/ft]	0.01
Tt [hr]	0.473

Shallow Concentrated Flow

Unpaved	
Elev Start [ft]	7082
Elev End [ft]	7072
Length [ft]	400
Output	
S [ft/ft]	0.0250
V [ft/s]	2.55
Tt [min]	2.61
Tt [hr]	0.044

Open Channel Flow

INPUT DATA:	
Elev Start [ft]	7072
Elev End [ft]	6988
Length [ft]	912
Manning's n	0.040
Channel Slope [ft/ft]	0.0921
Depth [ft]	2.00
OUTPUT DATA:	
Area [sf]	90.00
Wetted Perimeter [ft]	85.10
Hydraulic Radius	1.06
Velocity [fps]	11.70
Tt [min]	1.30
Tt [hr]	0.022

Tc [hr]	0.538
Tc [min]	32.30
SCS Lag [hr]	0.32

Woody Mountain Campground

Sub-3C Existing Condition

Sheet Flow

Input Data	
Elev Start [ft]	7082.00
Elev End [ft]	7081.25
Length [ft]	72
n (dense grasses)	0.03
OUTPUT	
S [ft/ft]	0.01
Tt [hr]	0.049

Shallow Concentrated Flow

Unpaved	
Elev Start [ft]	7081.25
Elev End [ft]	7079
Length [ft]	245
Output	
S [ft/ft]	0.0092
V [ft/s]	1.55
Tt [min]	2.64
Tt [hr]	0.044

Tc [hr]	0.093
Tc [min]	15.00 (Min. 15 min)
SCS Lag [hr]	0.15

Woody Mountain Campground

Sub-3A Proposed Condition

Sheet Flow

Input Data		
Elev Start [ft]		7083
Elev End [ft]		7081
Length [ft]		42
n (short grasses)		0.15
OUTPUT		
S [ft/ft]		0.05
Tt [hr]		0.073

Shallow Concentrated Flow

Unpaved		
Elev Start [ft]		7081
Elev End [ft]		7050
Length [ft]		1056
Output		
S [ft/ft]	0.0294	
V [ft/s]	2.76	
Tt [min]	6.37	
Tt [hr]	0.106	

Tc [hr]	0.179
Tc [min]	10.74
Tc [min] used	10.00
Tc [hr] used	0.17
SCS Lag [hr]	0.100

Woody Mountain Campground

Sub-3B Proposed Condition

Sheet Flow

Input Data	
Elev Start [ft]	7082.75
Elev End [ft]	7082
Length [ft]	43
n (dense grasses)	0.25
OUTPUT	
S [ft/ft]	0.02
Tt [hr]	0.167

Shallow Concentrated Flow

Unpaved	
Elev Start [ft]	7082
Elev End [ft]	7072
Length [ft]	448
Output	
S [ft/ft]	0.0223
V [ft/s]	2.41
Tt [min]	3.10
Tt [hr]	0.052

Open Channel Flow

INPUT DATA:	
Elev Start [ft]	7072
Elev End [ft]	7000
Length [ft]	548
Manning's n	0.040
Channel Slope [ft/ft]	0.1314
Depth [ft]	2.00
OUTPUT DATA:	
Top Width [ft]	85.00
Area [sf]	90.00
Wetted Perimeter [ft]	85.10
Hydraulic Radius	1.06
Velocity [fps]	13.98
Tt [min]	0.65
Tt [hr]	0.011

Tc [hr]	0.230
Tc [min]	13.78
SCS Lag [hr]	0.14

Woody Mountain Campground

Sub-3C Proposed Condition

Sheet Flow

Input Data	
Elev Start [ft]	7082
Elev End [ft]	7082
Length [ft]	72
n (dense grasses)	0.01
OUTPUT	
S [ft/ft]	0.01
Tt [hr]	0.030

Shallow Concentrated Flow

Unpaved	
Elev Start [ft]	7081.5
Elev End [ft]	7079
Length [ft]	245
Output	
S [ft/ft]	0.0102
V [ft/s]	1.63
Tt [min]	2.51
Tt [hr]	0.042

Tc [hr]	0.072
Tc [min]	10.00 (Min. 10 min)
SCS Lag [hr]	0.10

Woody Mountain Campground

Composite Curve Number (CN) Calculations-Existing Condition

Drainage Area ID	Total Area (ac)	Total Area (sq mi)	Soil Map Symbol	Hydrologic Soil Group	Cover Type	Cover Condition	SCS Curve Number	Area for Individual CN	Composite SCS CN
*1	7.01	0.011	2A	D	Open Space (<50% grass cover)	NA	89	1.29	86.55
			12	C	Open Space (<50% grass cover)	Fair	86	5.72	
*1A	28.94	0.045	2	D	Open Space (<50% grass cover)	NA	89	13.20	87.37
			12	C	Open Space (<50% grass cover)	NA	86	15.74	
Sub-1B	5.84	0.009	2	D	Paved Street	NA	98	1.90	93.23
				D	Paved Street w/ Open Ditches		93	1.90	
				D	Dirt (including ROW)	NA	89	2.04	
Sub-2	4.97	0.008	2	D	Residential - 1/8 Acre	NA	92	0.85	79.72
			2A	D	Residential - 1/8 Acre	Fair	92	1.07	
			12	C	Ponderosa Pine (Fair)	Fair	65	1.53	
					Open Space (50% -70% cover)	NA	79	1.53	
Sub-2A	4.53	0.007	2A	D	Dirt (including ROW)	NA	89	2.101	91.15
					Paved Street w/ Open Ditches	NA	93	2.43	
Sub-3A	5.14	0.008	12	C	Ponderosa Pine (Fair)	Fair	65	2.57	72.00
					Open Space (Fair)	NA	79	2.57	
Sub-3B	15.42	0.024	2A	D	Ponderosa Pine (Fair)	Fair	75	8.97	75.49
			12	C	Ponderosa Pine (Fair)	Fair	65	3.12	
					Open Space (Fair)	NA	79	3.12	
			12	C	Roofs	Fair	98	0.22	
Sub-3C	1.51	0.002	12	C	Ponderosa Pine (Fair)	Fair	65	0.65	75.74
					Open Space (Fair)	NA	79	0.65	
					Roofs	Fair	98	0.22	

* Drainage Areas 1 and 1A use the post burn curve numbers - Open Sapce with less than 50% grass cover

Woody Mountain Campground

Composite Curve Number (CN) Calculations-Proposed Condition

Drainage Area ID	Total Area (ac)	Total Area (sq mi)	Soil Map Symbol	Hydrologic Soil Group	Cover Type	Cover Condition	SCS Curve Number	Area for Individual CN	Composite SCS CN
*1	7.01	0.011	2A	D	Open Space (<50% grass cover)	NA	89	1.29	86.55
			12	C	Open Space (<50% grass cover)	Fair	86	5.72	
*1A	28.94	0.045	2	D	Open Space (<50% grass cover)	NA	89	13.20	87.37
			12	C	Open Space (<50% grass cover)	NA	86	15.74	
Sub-1B	5.84		2	D	Paved Street	NA	98	2.05	93.46
					Paved Street w/ Open Ditches	NA	93	1.90	
					Dirt (including ROW)	NA	89	1.89	
Sub-2	4.97	0.008	2	D	Residential - 1/8 Acre	NA	92	0.85	79.72
			2A	D	Residential - 1/8 Acre	Fair	92	1.07	
			12	C	Ponderosa Pine (Fair)	Fair	65	1.53	
					Open Space (<50% grass cover)	NA	79	1.53	
Sub-2A	4.53	0.007	2A	D	Dirt (including ROW)	NA	89	1.387	95.25
					Paved Street	NA	98	3.15	
Sub-3A	5.14	0.008	12	C	Ponderosa Pine (Fair)	Fair	65	1.75	78.72
					Open space (Fair)		79	1.75	
					Gravel		85	0.62	
					Rooftops/impervious areas	NA	98	1.02	
Sub-3B	15.42	0.024	2A	D	Ponderosa Pine (Fair)	Fair	75	3.97	86.44
					Open Space (Fair)		84	3.97	
					Permanent Pond		98	1.03	
			12	C	Ponderosa Pine (Fair)	Fair	65	2.03	
					Open space (Fair)		79	2.03	
					Gravel	NA	85	1.36	
12		Rooftops/impervious areas	Fair	98	1.97				
Sub-3C	1.51	0.002	12	C	Open Space (Fair)	Fair	79	0.45	92.30
					Roofs	Fair	98	1.06	

* Drainage Areas 1 and 1A use the post burn curve numbers - Open Sapce with less than 50% grass cover

Woody Mountain Campground

Drainage Area ID	Area			CN	Tc min	Tlag=0.6*Tc (hr)
	sq.ft	Acres	sq.miles			
Offsite						
Sub-1	305345	7.01	0.011	86.55	15.5	0.155
Sub-1A	1260517	28.94	0.045	87.37	18.9	0.189
Sub-1B	254229	5.84	0.009	93.23	10.0	0.100
Sub-2	216434	4.97	0.008	79.72	18.1	0.181
Sub-2A	197411	4.53	0.007	91.15	10.0	0.100
Onsite						
Sub-3A	223971	5.14	0.008	72.00	15.0	0.150
Sub-3B	671492	15.42	0.024	75.49	31.7	0.32
Sub-3C	65802	1.51	0.002	75.74	15.0	0.15

Woody Mountain Campground Drainage Area Summary-Proposed Conditions

Drainage Area ID	Area			CN	Tc min	Tlag=0.6*Tc (hr)
	sq.ft	Acres	sq.miles			
Offsite						
Sub-1	305345	7.01	0.011	86.55	15.5	0.155
Sub-1A	1260517	28.94	0.045	87.37	18.9	0.189
Sub-1B	254229	5.84	0.009	93.46	10.0	0.100
Sub-2	216434	4.97	0.008	79.72	18.1	0.181
Sub-2A	197411	4.53	0.007	95.25	10.0	0.100
Onsite						
Sub-3A	223971	5.14	0.008	78.72	10.0	0.100
Sub-3B	671492	15.42	0.024	86.44	24.2	0.242
Sub-3C	65802	1.51	0.002	92.30	10.0	0.100

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1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*       JAN 1997                *
*       VERSION 4.1             *
*
* RUN DATE  20JUN19  TIME  17:21:18 *
*
*****

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*****
*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET           *
* DAVIS, CALIFORNIA 95616     *
* (916) 756-1104             *
*
*****

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X   X  XXXXXXXX  XXXXX      X
X   X  X        X   X      XX
X   X  X        X           X
XXXXXXX  XXXX   X           XXXXX  X
X   X  X        X           X
X   X  X        X   X      X
X   X  XXXXXXXX  XXXXX      XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

*** FREE ***

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*DIAGRAM
1 ID Woody Mountain Campground
2 ID Proposed-Conditions with Detention Basin HEC-1 Model
3 ID 10-year, 6-hour Model
4 ID Woodson Engineering and Surveying
5 ID MAY 2019
6 ID PROPOSED CONDITION (WITH DETENTION BASIN)
7 IT 3 0 0 125
8 IO 5 0 0
9 IN 5 0 0
*

```

10 KK SUB-1
 11 BA 0.011
 12 PH 10 0.19 0.48 0.87 1.46 1.70 1.86 2.16
 13 LS 0 86.55
 14 UD 0.155
 *

15 KK SUB-2
 16 BA 0.008
 17 LS 0 79.72
 18 UD 0.181
 *

19 KK SUB-2A
 20 BA 0.007
 21 LS 0 95.25
 22 UD 0.1
 *

23 KK CP1A
 24 KM COMBINE HYDROGRAPHS FROM SUB-1, SUB-2 & SUB-2A
 25 HC 3
 *

26 KK SUB-3B
 27 KM RUNOFF FROM SUB-3B
 28 BA .024
 29 LS 0 86.44
 30 UD 0.24
 *

31 KK SUB-3C
 32 KM RUNOFF FROM SUB-3C
 33 BA .002
 34 LS 0 92.30
 35 UD 0.10
 *

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HEC-1 INPUT

PAGE 2

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

36 KK CP2
 37 KM COMBINE HYDROGRAPHS FROM SUB-3B, SUB-3C & CP1A
 38 HC 3
 *

39 KK BASIN4
 40 KM BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
 41 KM RUNOFF FROM BASIN 4
 42 BA .002

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43      LS      0   83.56
44      UD      .086
      *

45      KK      RCP26
46      KM      ROUTE CP26 TO CP27
47      RK      400   0.01   0.016       0       21       10       10
      *

48      KK      BASIN4A
49      KM      BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
50      KM      RUNOFF FROM BASIN 4A
51      BA      .002
52      LS      0   86.0
53      UD      .136
      *

54      KK      CP27
55      KM      COMBINE BASINS RCP26 & BASIN4A
56      HC      2
      *

57      KK      BASIN1A
58      KM      BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
59      KM      RUNOFF FROM BASIN 1A
60      BA      .001
61      LS      0   90.4
62      UD      .054
      *

63      KK      CP28
64      KM      COMBINE BASINS BASIN1A & CP27
65      HC      2
      *

66      KK      DB1
67      KM      BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
68      KM      DETENTION BASIN 1
69      RS      1   STOR       0
70      SV      0.0   0.02   0.09   0.15   0.23   0.31       0.39   0.40
71      SE      7052.8 7053.0 7053.5 7054.0 7054.5 7055.0 7055.5 7055.52
72      SQ      0.0   0.21   1.30   3.16   4.14   4.93       5.61   5.63
      *

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HEC-1 INPUT

PAGE 3

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

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73      KK      RDB1
74      KM      ROUTE DB1 TO CP30
75      RK      320   0.01   0.013       0   CIRC   0.5

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*
76      KK  BASIN4B
77      KM   BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
78      KM   RUNOFF FROM BASIN 4B
79      BA   .002
80      LS    0   87.81
81      UD   .071
      *

82      KK  BASIN3
83      KM   BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
84      KM   RUNOFF FROM BASIN 3
85      BA   .002
86      LS    0   90.80
87      UD   .071
      *

88      KK  SUB-1A
89      KM   RUNOFF FROM SUB-1A
90      BA   .045
91      LS    0   87.37
92      UD   .189
      *

93      KK  SUB-1B
94      KM   RUNOFF FROM SUB-1B
95      BA   .009
96      LS    0   93.46
97      UD   .10
      *

98      KK  CP1A1B
99      KM   COMBINE SUB-1A & SUB-1B
100     HC    2
      *

101     KK  RCP1A1B
102     KM   ROUTE CP1A1B TO CP30
103     RK   1200   0.01   0.013   0   CIRC   2.5
      *

104     KK  SUB-3A
105     KM   RUNOFF FROM SUB-3A
106     BA   .008
107     LS    0   78.72
108     UD   .10
      *

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

109	KK	CP30								
110	KM	COMBINE HYDROGRAPHS FROM BASINS 3, 4B, DB1, SUB-3A& CP1A1B								
111	HC	5								
	*									
112	KK	CPDBI								
113	KM	COMBINE ROUTED HYDROGRAPHS FROM CP30 &,CP1A WITH SUB-3B								
114	HC	2								
	*									
	*									
115	KK	DBWMC								
116	KM	DETENTION BASIN WEST OF WILDWOOD HILLS MOBILE HOME PARK								
117	RS	1	STOR	0						
118	SV	0.0	0.76	1.59	2.49	3.46	4.52	5.69	6.96	8.31
119	SE	6992.0	6993.0	6994.0	6995.0	6996.0	6997.0	6998.0	6999.0	7000.0
120	SQ	0.0	28.5	24.6	33.8	40.9	47.0	52.4	57.3	61.8
	*									
121	ZZ									

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW

NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW

```

10  SUB-1
    .
    .
15  .      SUB-2
    .      .
    .      .
19  .      .      SUB-2A
    .      .      .
    .      .      .
23  CP1A.....
    .
    .
26  .      SUB-3B
    .      .
    .      .
31  .      .      SUB-3C
    .      .      .
    .      .      .
36  CP2.....
    .
    .
39  .      BASIN4
    .      V

```

```

45      .      V
      .      RCP26
      .      .
48      .      .      BASIN4A
      .      .      .
54      .      CP27.....
      .      .
57      .      .      BASIN1A
      .      .      .
63      .      CP28.....
      .      V
      .      V
66      .      DB1
      .      V
      .      V
73      .      RDB1
      .      .
76      .      .      BASIN4B
      .      .      .
82      .      .      .      BASIN3
      .      .      .      .
88      .      .      .      .      SUB-1A
      .      .      .      .      .
93      .      .      .      .      .      SUB-1B
      .      .      .      .      .      .
98      .      .      .      .      CP1A1B.....
      .      .      .      .      V
101     .      .      .      .      V
      .      .      .      .      RCP1A1B
      .      .      .      .      .
104     .      .      .      .      .      SUB-3A
      .      .      .      .      .      .
109     .      CP30.....
      .      .
112     CPDBI.....
      .      V
      .      V
115     DBWMC

```

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*       JAN   1997             *
*       VERSION 4.1           *
*
* RUN DATE   20JUN19  TIME  17:21:18 *
*
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET           *
* DAVIS, CALIFORNIA 95616     *
* (916) 756-1104             *
*
*****

```

Woody Mountain Campground
Proposed-Conditions with Detention Basin HEC-1 Model
10-year, 6-hour Model
Woodson Engineering and Surveying
MAY 2019
PROPOSED CONDITION (WITH DETENTION BASIN)

```

8 IO      OUTPUT CONTROL VARIABLES
          IPRNT      5  PRINT CONTROL
          IPLOT      0  PLOT CONTROL
          QSCAL      0.  HYDROGRAPH PLOT SCALE

```

```

IT        HYDROGRAPH TIME DATA
          NMIN      3  MINUTES IN COMPUTATION INTERVAL
          IDATE     1  0  STARTING DATE
          ITIME     0000 STARTING TIME
          NQ        125 NUMBER OF HYDROGRAPH ORDINATES
          NDDATE    1  0  ENDING DATE
          NDTIME    0612 ENDING TIME
          ICENT     19  CENTURY MARK

          COMPUTATION INTERVAL .05 HOURS
          TOTAL TIME BASE     6.20 HOURS

```

```

ENGLISH UNITS
DRAINAGE AREA      SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION  FEET
FLOW               CUBIC FEET PER SECOND
STORAGE VOLUME    ACRE-FEET
SURFACE AREA      ACRES
TEMPERATURE       DEGREES FAHRENHEIT

```

1

RUNOFF SUMMARY
FLOW IN CUBIC FEET PER SECOND
TIME IN HOURS, AREA IN SQUARE MILES

+	OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
					6-HOUR	24-HOUR	72-HOUR			
+	HYDROGRAPH AT									
+		SUB-1	12.	3.20	1.	1.	1.	.01		
+	HYDROGRAPH AT									
+		SUB-2	5.	3.25	1.	1.	1.	.01		
+	HYDROGRAPH AT									
+		SUB-2A	15.	3.10	1.	1.	1.	.01		
+	3 COMBINED AT									
+		CP1A	29.	3.15	3.	3.	3.	.03		
+	HYDROGRAPH AT									
+		SUB-3B	21.	3.30	3.	2.	2.	.02		
+	HYDROGRAPH AT									
+		SUB-3C	4.	3.15	0.	0.	0.	.00		
+	3 COMBINED AT									
+		CP2	49.	3.20	6.	6.	6.	.05		
+	HYDROGRAPH AT									
+		BASIN4	2.	3.10	0.	0.	0.	.00		
+	ROUTED TO									
+		RCP26	2.	3.15	0.	0.	0.	.00		
+	HYDROGRAPH AT									
+		BASIN4A	2.	3.20	0.	0.	0.	.00		
+	2 COMBINED AT									
+		CP27	4.	3.15	0.	0.	0.	.00		
+	HYDROGRAPH AT									
+		BASIN1A	2.	3.10	0.	0.	0.	.00		
+	2 COMBINED AT									
+		CP28	6.	3.15	1.	0.	0.	.01		
+	ROUTED TO									
+		DB1	2.	3.45	0.	0.	0.	.01		
+									7053.69	3.45
+	ROUTED TO									
+		RDB1	2.	3.45	0.	0.	0.	.01		

+	HYDROGRAPH AT	BASIN4B	3.	3.10	0.	0.	0.	.00		
+	HYDROGRAPH AT	BASIN3	4.	3.10	0.	0.	0.	.00		
+	HYDROGRAPH AT	SUB-1A	47.	3.25	5.	5.	5.	.05		
+	HYDROGRAPH AT	SUB-1B	17.	3.10	1.	1.	1.	.01		
+	2 COMBINED AT	CP1A1B	60.	3.20	6.	6.	6.	.05		
+	ROUTED TO	RCP1A1B	59.	3.20	6.	6.	6.	.05		
+	HYDROGRAPH AT	SUB-3A	6.	3.15	1.	0.	0.	.01		
+	5 COMBINED AT	CP30	69.	3.20	8.	8.	8.	.07		
+	2 COMBINED AT	CPDBI	118.	3.20	14.	13.	13.	.12		
+	ROUTED TO	DBWMC	37.	3.65	13.	13.	13.	.12	6995.42	3.65
+										
1										

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	DT	INTERPOLATED TO		VOLUME
							COMPUTATION	INTERVAL	
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	PEAK	TIME TO PEAK	(IN)
RCP26	MANE	.79	2.18	187.57	.82	3.00	2.17	189.00	.82

CONTINUITY SUMMARY (AC-FT) - INFLOW= .8735E-01 EXCESS= .0000E+00 OUTFLOW= .8723E-01 BASIN STORAGE= .1745E-03 PERCENT ERROR= -.1

RDB1	MANE	.40	1.99	207.20	.86	3.00	1.99	207.00	.86
------	------	-----	------	--------	-----	------	------	--------	-----

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2303E+00 EXCESS= .0000E+00 OUTFLOW= .2300E+00 BASIN STORAGE= .3864E-03 PERCENT ERROR= .0

RCPLA1B MANE .52 59.64 192.98 1.11 3.00 58.58 192.00 1.11

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3186E+01 EXCESS= .0000E+00 OUTFLOW= .3184E+01 BASIN STORAGE= .3936E-02 PERCENT ERROR= -.1

*** NORMAL END OF HEC-1 ***

```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*       JAN 1997                *
*       VERSION 4.1              *
*
* RUN DATE 24JUN19 TIME 14:22:08 *
*
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET            *
* DAVIS, CALIFORNIA 95616      *
* (916) 756-1104               *
*
*****

```

```

X   X XXXXXXXX XXXXX      X
X   X X      X      X    XX
X   X X      X      X    X
XXXXXXX XXXX  X      XXXXX X
X   X X      X      X    X
X   X X      X      X    X
X   X XXXXXXXX XXXXX      XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

*** FREE ***

```

*DIAGRAM
1 ID Woody Mountain Campground
2 ID Proposed-Conditions with Detention Basin HEC-1 Model
3 ID 25-year, 6-hour Model
4 ID Woodson Engineering and Surveying
5 ID MAY 2019
6 ID PROPOSED CONDITION (WITH DETENTION BASIN)
7 IT 3 0 0 125
8 IO 5 0 0
9 IN 5 0 0
*

```

10 KK SUB-1
 11 BA 0.011
 12 PH 25 0.19 0.57 1.10 1.76 2.04 2.22 2.58
 13 LS 0 86.55
 14 UD 0.155
 *

15 KK SUB-2
 16 BA 0.008
 17 LS 0 79.72
 18 UD 0.181
 *

19 KK SUB-2A
 20 BA 0.007
 21 LS 0 95.25
 22 UD 0.1
 *

23 KK CP1A
 24 KM COMBINE HYDROGRAPHS FROM SUB-1, SUB-2 & SUB-2A
 25 HC 3
 *

26 KK SUB-3B
 27 KM RUNOFF FROM SUB-3B
 28 BA .024
 29 LS 0 86.44
 30 UD 0.24
 *

31 KK SUB-3C
 32 KM RUNOFF FROM SUB-3C
 33 BA .002
 34 LS 0 92.30
 35 UD 0.10
 *

1

HEC-1 INPUT

PAGE 2

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

36 KK CP2
 37 KM COMBINE HYDROGRAPHS FROM SUB-3B, SUB-3C & CP1A
 38 HC 3
 *

39 KK BASIN4
 40 KM BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
 41 KM RUNOFF FROM BASIN 4
 42 BA .002

```

43      LS      0    83.56
44      UD      .086
      *

45      KK      RCP26
46      KM      ROUTE CP26 TO CP27
47      RK      400    0.01    0.016      0    21    10    10
      *

48      KK      BASIN4A
49      KM      BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
50      KM      RUNOFF FROM BASIN 4A
51      BA      .002
52      LS      0    86.0
53      UD      .136
      *

54      KK      CP27
55      KM      COMBINE BASINS RCP26 & BASIN4A
56      HC      2
      *

57      KK      BASIN1A
58      KM      BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
59      KM      RUNOFF FROM BASIN 1A
60      BA      .001
61      LS      0    90.4
62      UD      .054
      *

63      KK      CP28
64      KM      COMBINE BASINS BASIN1A & CP27
65      HC      2
      *

66      KK      DB1
67      KM      BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
68      KM      DETENTION BASIN 1
69      RS      1    STOR      0
70      SV      0.0    0.02    0.09    0.15    0.23    0.31    0.39    0.40
71      SE      7052.8  7053.0  7053.5  7054.0  7054.5  7055.0  7055.5  7055.52
72      SQ      0.0    0.21    1.30    3.16    4.14    4.93    5.61    5.63
      *

```

1

HEC-1 INPUT

PAGE 3

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

73      KK      RDB1
74      KM      ROUTE DB1 TO CP30
75      RK      320    0.01    0.013      0    CIRC    0.5

```

```

*
76      KK  BASIN4B
77      KM   BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
78      KM   RUNOFF FROM BASIN 4B
79      BA   .002
80      LS   0   87.81
81      UD   .071
      *

82      KK  BASIN3
83      KM   BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
84      KM   RUNOFF FROM BASIN 3
85      BA   .002
86      LS   0   90.80
87      UD   .071
      *

88      KK  SUB-1A
89      KM   RUNOFF FROM SUB-1A
90      BA   .045
91      LS   0   87.37
92      UD   .189
      *

93      KK  SUB-1B
94      KM   RUNOFF FROM SUB-1B
95      BA   .009
96      LS   0   93.46
97      UD   .10
      *

98      KK  CP1A1B
99      KM   COMBINE SUB-1A & SUB-1B
100     HC   2
      *

101     KK  RCP1A1B
102     KM   ROUTE CP1A1B TO CP30
103     RK   1200   0.01   0.013   0   CIRC   2.5
      *

104     KK  SUB-3A
105     KM   RUNOFF FROM SUB-3A
106     BA   .008
107     LS   0   78.72
108     UD   .10
      *

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

109      KK   CP30
110      KM   COMBINE HYDROGRAPHS FROM BASINS 3, 4B, DB1, SUB-3A& CP1A1B
111      HC     5
          *

112      KK   CPDBI
113      KM   COMBINE ROUTED HYDROGRAPHS FROM CP30 &,CP1A WITH SUB-3B
114      HC     2
          *
          *

115      KK   DBWMC
116      KM   DETENTION BASIN WEST OF WILDWOOD HILLS MOBILE HOME PARK
117      RS     1   STOR     0
118      SV     0.0   0.76   1.59   2.49   3.46   4.52   5.69   6.96   8.31
119      SE  6992.0 6993.0 6994.0 6995.0 6996.0 6997.0 6998.0 6999.0 7000.0
120      SQ     0.0   28.5   24.6   33.8   40.9   47.0   52.4   57.3   61.8
          *
121      ZZ

```

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

```

INPUT
LINE  (V) ROUTING      (--->) DIVERSION OR PUMP FLOW

NO.   (.) CONNECTOR  (<---) RETURN OF DIVERTED OR PUMPED FLOW

10    SUB-1
      .
      .
15    .      SUB-2
      .      .
      .      .
19    .      .      SUB-2A
      .      .      .
      .      .      .
23    CP1A.....
      .
      .
26    .      SUB-3B
      .      .
      .      .
31    .      .      SUB-3C
      .      .      .
      .      .      .
36    CP2.....
      .
      .
39    .      BASIN4
      .      V

```

```

45      .      V
      .      RCP26
      .      .
48      .      .      BASIN4A
      .      .      .
54      .      CP27.....
      .      .
57      .      .      BASIN1A
      .      .      .
63      .      CP28.....
      .      V
      .      V
66      .      DB1
      .      V
      .      V
73      .      RDB1
      .      .
76      .      .      BASIN4B
      .      .      .
82      .      .      .      BASIN3
      .      .      .      .
88      .      .      .      .      SUB-1A
      .      .      .      .      .
93      .      .      .      .      .      SUB-1B
      .      .      .      .      .      .
98      .      .      .      .      CP1A1B.....
      .      .      .      .      V
101     .      .      .      .      V
      .      .      .      .      RCP1A1B
      .      .      .      .      .
104     .      .      .      .      .      SUB-3A
      .      .      .      .      .      .
109     .      CP30.....
      .      .
112     CPDBI.....
      .      V
      .      V
115     DBWMC

```

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*       JAN 1997 *
*       VERSION 4.1 *
*
* RUN DATE 24JUN19 TIME 14:22:08 *
*
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*
*****

```

Woody Mountain Campground
Proposed-Conditions with Detention Basin HEC-1 Model
25-year, 6-hour Model
Woodson Engineering and Surveying
MAY 2019
PROPOSED CONDITION (WITH DETENTION BASIN)

```

8 IO      OUTPUT CONTROL VARIABLES
          IPRNT      5  PRINT CONTROL
          IPLOT      0  PLOT CONTROL
          QSCAL      0.  HYDROGRAPH PLOT SCALE

IT        HYDROGRAPH TIME DATA
          NMIN      3  MINUTES IN COMPUTATION INTERVAL
          IDATE     1  0  STARTING DATE
          ITIME     0000 STARTING TIME
          NQ        125 NUMBER OF HYDROGRAPH ORDINATES
          NDDATE    1  0  ENDING DATE
          NDTIME    0612 ENDING TIME
          ICENT     19  CENTURY MARK

          COMPUTATION INTERVAL .05 HOURS
          TOTAL TIME BASE      6.20 HOURS

```

ENGLISH UNITS

```

DRAINAGE AREA      SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION  FEET
FLOW               CUBIC FEET PER SECOND
STORAGE VOLUME    ACRE-FEET
SURFACE AREA      ACRES
TEMPERATURE       DEGREES FAHRENHEIT

```

1

RUNOFF SUMMARY
FLOW IN CUBIC FEET PER SECOND
TIME IN HOURS, AREA IN SQUARE MILES

+	OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
					6-HOUR	24-HOUR	72-HOUR			
+	HYDROGRAPH AT	SUB-1	17.	3.20	2.	2.	2.	.01		
+	HYDROGRAPH AT	SUB-2	8.	3.25	1.	1.	1.	.01		
+	HYDROGRAPH AT	SUB-2A	19.	3.10	2.	2.	2.	.01		
+	3 COMBINED AT	CP1A	41.	3.15	4.	4.	4.	.03		
+	HYDROGRAPH AT	SUB-3B	30.	3.30	3.	3.	3.	.02		
+	HYDROGRAPH AT	SUB-3C	5.	3.15	0.	0.	0.	.00		
+	3 COMBINED AT	CP2	69.	3.20	8.	7.	7.	.05		
+	HYDROGRAPH AT	BASIN4	3.	3.15	0.	0.	0.	.00		
+	ROUTED TO	RCP26	3.	3.15	0.	0.	0.	.00		
+	HYDROGRAPH AT	BASIN4A	3.	3.20	0.	0.	0.	.00		
+	2 COMBINED AT	CP27	6.	3.15	1.	1.	1.	.00		
+	HYDROGRAPH AT	BASIN1A	3.	3.10	0.	0.	0.	.00		
+	2 COMBINED AT	CP28	8.	3.15	1.	1.	1.	.01		
+	ROUTED TO	DB1	3.	3.40	1.	1.	1.	.01	7054.01	3.40
+	ROUTED TO	RDB1	3.	3.40	1.	1.	1.	.01		

+	HYDROGRAPH AT	BASIN4B	4.	3.10	0.	0.	0.	.00		
+	HYDROGRAPH AT	BASIN3	5.	3.10	0.	0.	0.	.00		
+	HYDROGRAPH AT	SUB-1A	66.	3.25	7.	7.	7.	.05		
+	HYDROGRAPH AT	SUB-1B	23.	3.15	2.	2.	2.	.01		
+	2 COMBINED AT	CP1A1B	84.	3.20	9.	8.	8.	.05		
+	ROUTED TO	RCP1A1B	82.	3.20	9.	8.	8.	.05		
+	HYDROGRAPH AT	SUB-3A	9.	3.15	1.	1.	1.	.01		
+	5 COMBINED AT	CP30	99.	3.20	11.	10.	10.	.07		
+	2 COMBINED AT	CPDBI	168.	3.20	18.	18.	18.	.12		
+	ROUTED TO	DBWMC	46.	3.65	18.	17.	17.	.12	6996.75	3.65
+										
1										

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	INTERPOLATED TO		VOLUME	
						COMPUTATION	INTERVAL		
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)
RCP26	MANE	.64	3.20	189.74	1.15	3.00	3.20	189.00	1.15

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1226E+00 EXCESS= .0000E+00 OUTFLOW= .1226E+00 BASIN STORAGE= .1680E-03 PERCENT ERROR= -.2

RDB1	MANE	.42	3.17	203.94	1.20	3.00	3.17	204.00	1.20
------	------	-----	------	--------	------	------	------	--------	------

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3197E+00 EXCESS= .0000E+00 OUTFLOW= .3192E+00 BASIN STORAGE= .4648E-03 PERCENT ERROR= .0

RCPLA1B MANE .52 83.33 192.94 1.48 3.00 81.85 192.00 1.48

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4262E+01 EXCESS= .0000E+00 OUTFLOW= .4257E+01 BASIN STORAGE= .5004E-02 PERCENT ERROR= .0

*** NORMAL END OF HEC-1 ***

```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*       JAN 1997                *
*       VERSION 4.1              *
*
* RUN DATE  20JUN19  TIME  17:21:49 *
*
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS    *
* HYDROLOGIC ENGINEERING CENTER  *
* 609 SECOND STREET              *
* DAVIS, CALIFORNIA 95616        *
* (916) 756-1104                 *
*
*****

```

```

X   X  XXXXXXXX  XXXXX      X
X   X  X        X   X      XX
X   X  X        X          X
XXXXXXX  XXXX   X          XXXXX  X
X   X  X        X          X
X   X  X        X   X      X
X   X  XXXXXXXX  XXXXX      XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

*** FREE ***

```

*DIAGRAM
1 ID Woody Mountain Campground
2 ID Proposed-Conditions with Detention Basin HEC-1 Model
3 ID 100-year, 6-hour Model
4 ID Woodson Engineering and Surveying
5 ID MAY 2019
6 ID PROPOSED CONDITION (WITH DETENTION BASIN)
7 IT 3 0 0 125
8 IO 5 0 0
9 IN 5 0 0
*

```

10 KK SUB-1
 11 BA 0.011
 12 PH 1 0.19 0.71 1.37 2.21 2.56 2.76 3.18
 13 LS 0 86.55
 14 UD 0.155
 *

15 KK SUB-2
 16 BA 0.008
 17 LS 0 79.72
 18 UD 0.181
 *

19 KK SUB-2A
 20 BA 0.007
 21 LS 0 95.25
 22 UD 0.1
 *

23 KK CP1A
 24 KM COMBINE HYDROGRAPHS FROM SUB-1, SUB-2 & SUB-2A
 25 HC 3
 *

26 KK SUB-3B
 27 KM RUNOFF FROM SUB-3B
 28 BA .024
 29 LS 0 86.44
 30 UD 0.24
 *

31 KK SUB-3C
 32 KM RUNOFF FROM SUB-3C
 33 BA .002
 34 LS 0 92.30
 35 UD 0.10
 *

1

HEC-1 INPUT

PAGE 2

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

36 KK CP2
 37 KM COMBINE HYDROGRAPHS FROM SUB-3B, SUB-3C & CP1A
 38 HC 3
 *

39 KK BASIN4
 40 KM BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
 41 KM RUNOFF FROM BASIN 4
 42 BA .002

```

43      LS      0    83.56
44      UD      .086
      *

45      KK      RCP26
46      KM      ROUTE CP26 TO CP27
47      RK      400    0.01    0.016      0      21      10      10
      *

48      KK      BASIN4A
49      KM      BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
50      KM      RUNOFF FROM BASIN 4A
51      BA      .002
52      LS      0      86.0
53      UD      .136
      *

54      KK      CP27
55      KM      COMBINE BASINS RCP26 & BASIN4A
56      HC      2
      *

57      KK      BASIN1A
58      KM      BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
59      KM      RUNOFF FROM BASIN 1A
60      BA      .001
61      LS      0      90.4
62      UD      .054
      *

63      KK      CP28
64      KM      COMBINE BASINS BASIN1A & CP27
65      HC      2
      *

66      KK      DB1
67      KM      BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
68      KM      DETENTION BASIN 1
69      RS      1      STOR      0
70      SV      0.0    0.02    0.09    0.15    0.23    0.31      0.39    0.40
71      SE      7052.8  7053.0  7053.5  7054.0  7054.5  7055.0  7055.5  7055.52
72      SQ      0.0    0.21    1.30    3.16    4.14    4.93      5.61    5.63
      *

```

1

HEC-1 INPUT

PAGE 3

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

73      KK      RDB1
74      KM      ROUTE DB1 TO CP30
75      RK      320    0.01    0.013      0      CIRC    0.5

```

```

*
76      KK  BASIN4B
77      KM   BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
78      KM   RUNOFF FROM BASIN 4B
79      BA   .002
80      LS   0   87.81
81      UD   .071
      *

82      KK  BASIN3
83      KM   BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
84      KM   RUNOFF FROM BASIN 3
85      BA   .002
86      LS   0   90.80
87      UD   .071
      *

88      KK  SUB-1A
89      KM   RUNOFF FROM SUB-1A
90      BA   .045
91      LS   0   87.37
92      UD   .189
      *

93      KK  SUB-1B
94      KM   RUNOFF FROM SUB-1B
95      BA   .009
96      LS   0   93.46
97      UD   .10
      *

98      KK  CP1A1B
99      KM   COMBINE SUB-1A & SUB-1B
100     HC   2
      *

101     KK  RCP1A1B
102     KM   ROUTE CP1A1B TO CP30
103     RK   1200   0.01   0.013   0   CIRC   2.5
      *

104     KK  SUB-3A
105     KM   RUNOFF FROM SUB-3A
106     BA   .008
107     LS   0   78.72
108     UD   .10
      *

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

109	KK	CP30								
110	KM	COMBINE HYDROGRAPHS FROM BASINS 3, 4B, DB1, SUB-3A& CP1A1B								
111	HC	5								
	*									
112	KK	CPDBI								
113	KM	COMBINE ROUTED HYDROGRAPHS FROM CP30 &,CP1A WITH SUB-3B								
114	HC	2								
	*									
115	KK	DBWMC								
116	KM	DETENTION BASIN WEST OF WILDWOOD HILLS MOBILE HOME PARK								
117	RS	1	STOR	0						
118	SV	0.0	0.76	1.59	2.49	3.46	4.52	5.69	6.96	8.31
119	SE	6992.0	6993.0	6994.0	6995.0	6996.0	6997.0	6998.0	6999.0	7000.0
120	SQ	0.0	28.5	24.6	33.8	40.9	47.0	52.4	57.3	61.8
	*									
121	ZZ									

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW

NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW

```

10  SUB-1
    .
    .
15  .      SUB-2
    .      .
    .      .
19  .      .      SUB-2A
    .      .      .
    .      .      .
23  CP1A.....
    .
    .
26  .      SUB-3B
    .      .
    .      .
31  .      .      SUB-3C
    .      .      .
    .      .      .
36  CP2.....
    .
    .
39  .      BASIN4
    .      V
    .      V

```

```

45      .      RCP26
      .      .
      .      .
48      .      .      BASIN4A
      .      .      .
      .      .      .
54      .      CP27.....
      .      .
      .      .
57      .      .      BASIN1A
      .      .      .
      .      .      .
63      .      CP28.....
      .      V
      .      V
66      .      DB1
      .      V
      .      V
73      .      RDB1
      .      .
      .      .
76      .      .      BASIN4B
      .      .      .
      .      .      .
82      .      .      .      BASIN3
      .      .      .      .
      .      .      .      .
88      .      .      .      .      SUB-1A
      .      .      .      .      .
      .      .      .      .      .
93      .      .      .      .      .      SUB-1B
      .      .      .      .      .      .
      .      .      .      .      .      .
98      .      .      .      .      CP1A1B.....
      .      .      .      .      V
      .      .      .      .      V
101     .      .      .      .      RCP1A1B
      .      .      .      .      .
      .      .      .      .      .
104     .      .      .      .      .      SUB-3A
      .      .      .      .      .      .
      .      .      .      .      .      .
109     .      CP30.....
      .      .
      .      .
112     CPDBI.....
      .      V
      .      V
115     DBWMC

```

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
*       JAN 1997
*       VERSION 4.1
*
* RUN DATE 20JUN19 TIME 17:21:49
*
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****

```

```

Woody Mountain Campground
Proposed-Conditions with Detention Basin HEC-1 Model
100-year, 6-hour Model
Woodson Engineering and Surveying
MAY 2019
PROPOSED CONDITION (WITH DETENTION BASIN)

```

8 IO OUTPUT CONTROL VARIABLES

```

IPRNT      5 PRINT CONTROL
IPLOT      0 PLOT CONTROL
QSCAL     0. HYDROGRAPH PLOT SCALE

```

IT HYDROGRAPH TIME DATA

```

NMIN      3 MINUTES IN COMPUTATION INTERVAL
IDATE     1 0 STARTING DATE
ITIME     0000 STARTING TIME
NQ        125 NUMBER OF HYDROGRAPH ORDINATES
NDDATE    1 0 ENDING DATE
NDTIME    0612 ENDING TIME
ICENT     19 CENTURY MARK

```

```

COMPUTATION INTERVAL .05 HOURS
TOTAL TIME BASE      6.20 HOURS

```

ENGLISH UNITS

```

DRAINAGE AREA      SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION  FEET
FLOW                CUBIC FEET PER SECOND
STORAGE VOLUME     ACRE-FEET
SURFACE AREA       ACRES
TEMPERATURE        DEGREES FAHRENHEIT

```

1

```

RUNOFF SUMMARY
FLOW IN CUBIC FEET PER SECOND
TIME IN HOURS, AREA IN SQUARE MILES

```

+	OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
					6-HOUR	24-HOUR	72-HOUR			
+	HYDROGRAPH AT									
+		SUB-1	24.	3.20	2.	2.	2.	.01		
+	HYDROGRAPH AT									
+		SUB-2	12.	3.25	1.	1.	1.	.01		
+	HYDROGRAPH AT									
+		SUB-2A	24.	3.10	2.	2.	2.	.01		
+	3 COMBINED AT									
+		CP1A	56.	3.15	5.	5.	5.	.03		
+	HYDROGRAPH AT									
+		SUB-3B	42.	3.30	5.	5.	5.	.02		
+	HYDROGRAPH AT									
+		SUB-3C	6.	3.15	1.	0.	0.	.00		
+	3 COMBINED AT									
+		CP2	97.	3.20	11.	10.	10.	.05		
+	HYDROGRAPH AT									
+		BASIN4	5.	3.10	0.	0.	0.	.00		
+	ROUTED TO									
+		RCP26	5.	3.15	0.	0.	0.	.00		
+	HYDROGRAPH AT									
+		BASIN4A	4.	3.15	0.	0.	0.	.00		
+	2 COMBINED AT									
+		CP27	9.	3.15	1.	1.	1.	.00		
+	HYDROGRAPH AT									
+		BASIN1A	3.	3.10	0.	0.	0.	.00		
+	2 COMBINED AT									
+		CP28	12.	3.15	1.	1.	1.	.01		
+	ROUTED TO									
+		DB1	4.	3.40	1.	1.	1.	.01		
+									7054.42	3.40
+	ROUTED TO									
+		RDB1	4.	3.40	1.	1.	1.	.01		
+	HYDROGRAPH AT									

+		BASIN4B	6.	3.10	0.	0.	0.	.00		
	HYDROGRAPH AT									
+		BASIN3	7.	3.10	0.	0.	0.	.00		
	HYDROGRAPH AT									
+		SUB-1A	92.	3.25	9.	9.	9.	.05		
	HYDROGRAPH AT									
+		SUB-1B	29.	3.15	2.	2.	2.	.01		
	2 COMBINED AT									
+		CP1A1B	115.	3.20	12.	11.	11.	.05		
	ROUTED TO									
+		RCP1A1B	113.	3.20	12.	11.	11.	.05		
	HYDROGRAPH AT									
+		SUB-3A	14.	3.15	1.	1.	1.	.01		
	5 COMBINED AT									
+		CP30	137.	3.20	15.	14.	14.	.07		
	2 COMBINED AT									
+		CPDBI	234.	3.20	25.	24.	24.	.12		
	ROUTED TO									
+		DBWMC	55.	3.70	23.	22.	22.	.12		
+									6998.51	3.70
1										

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	INTERPOLATED TO COMPUTATION INTERVAL		VOLUME	
						DT	PEAK		
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)
RCP26	MANE	.60	4.66	187.74	1.63	3.00	4.62	189.00	1.63

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1740E+00 EXCESS= .0000E+00 OUTFLOW= .1741E+00 BASIN STORAGE= .2036E-03 PERCENT ERROR= -.2

RDB1	MANE	.44	3.98	204.47	1.68	3.00	3.98	204.00	1.68
------	------	-----	------	--------	------	------	------	--------	------

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4494E+00 EXCESS= .0000E+00 OUTFLOW= .4489E+00 BASIN STORAGE= .5692E-03 PERCENT ERROR= .0

RCP1A1B MANE .46 114.50 193.12 2.01 3.00 112.83 192.00 2.01

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5788E+01 EXCESS= .0000E+00 OUTFLOW= .5784E+01 BASIN STORAGE= .5657E-02 PERCENT ERROR= .0

*** NORMAL END OF HEC-1 ***

```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*       JAN 1997                *
*       VERSION 4.1              *
*
* RUN DATE 09MAY19 TIME 15:59:12 *
*
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET            *
* DAVIS, CALIFORNIA 95616      *
* (916) 756-1104               *
*
*****

```

```

X   X XXXXXXXX XXXXX      X
X   X X      X   X      XX
X   X X      X           X
XXXXXXX XXXX   X      XXXXX X
X   X X      X           X
X   X X      X   X      X
X   X XXXXXXXX XXXXX      XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

*** FREE ***

```

*DIAGRAM
1 ID Woody Mountain Campground
2 ID Existing-Conditions HEC-1 Model
3 ID 10-year, 6-hour Model
4 ID Woodson Engineering and Surveying
5 ID MAY 2019
6 ID EXISTING CONDITION
7 IT 3 0 0 125
8 IO 5 0 0
9 IN 5 0 0
*

```

10 KK SUB-1
 11 BA 0.011
 12 PH 10 0.19 0.48 0.87 1.46 1.70 1.86 2.16
 13 LS 0 86.55
 14 UD 0.155
 *

15 KK SUB-2
 16 BA 0.008
 17 LS 0 79.72
 18 UD 0.181
 *

19 KK SUB-2A
 20 BA 0.007
 21 LS 0 91.51
 22 UD 0.1
 *

23 KK CP1A
 24 KM COMBINE HYDROGRAPHS FROM SUB-1, SUB-2 & SUB-2A
 25 HC 3
 *

26 KK SUB-3B
 27 KM RUNOFF FROM SUB-3B
 28 BA .024
 29 LS 0 75.49
 30 UD 0.32
 *

31 KK SUB-3C
 32 KM RUNOFF FROM SUB-3C
 33 BA .002
 34 LS 0 75.74
 35 UD 0.15
 *

1

HEC-1 INPUT

PAGE 2

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

36 KK CP2
 37 KM COMBINE HYDROGRAPHS FROM SUB-3B, SUB-3C & CP1A
 38 HC 3
 *

39 KK BASIN4
 40 KM BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
 41 KM RUNOFF FROM BASIN 4
 42 BA .002

```

43      LS      0      83.56
44      UD      .086
      *

45      KK      RCP26
46      KM      ROUTE CP26 TO CP27
47      RK      400      0.01      0.016      0      21      10      10
      *

48      KK      BASIN4A
49      KM      BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
50      KM      RUNOFF FROM BASIN 4A
51      BA      .002
52      LS      0      86.0
53      UD      .136
      *

54      KK      CP27
55      KM      COMBINE BASINS RCP26 & BASIN4A
56      HC      2
      *

57      KK      BASIN1A
58      KM      BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
59      KM      RUNOFF FROM BASIN 1A
60      BA      .001
61      LS      0      90.4
62      UD      .054
      *

63      KK      CP28
64      KM      COMBINE BASINS BASIN1A & CP27
65      HC      2
      *

66      KK      DB1
67      KM      BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
68      KM      DETENTION BASIN 1
69      RS      1      STOR      0
70      SV      0.0      0.02      0.09      0.15      0.23      0.31      0.39      0.40
71      SE      7052.8      7053.0      7053.5      7054.0      7054.5      7055.0      7055.5      7055.52
72      SQ      0.0      0.21      1.30      3.16      4.14      4.93      5.61      5.63
      *

```

1

HEC-1 INPUT

PAGE 3

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

73      KK      RDB1
74      KM      ROUTE DB1 TO CP30
75      RK      320      0.01      0.013      0      CIRC      0.5

```

```

*
76      KK  BASIN4B
77      KM   BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
78      KM   RUNOFF FROM BASIN 4B
79      BA   .002
80      LS   0   87.81
81      UD   .071
      *

82      KK  BASIN3
83      KM   BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
84      KM   RUNOFF FROM BASIN 3
85      BA   .002
86      LS   0   90.80
87      UD   .071
      *

88      KK  SUB-1A
89      KM   RUNOFF FROM SUB-1A
90      BA   .045
91      LS   0   87.37
92      UD   .189
      *

93      KK  SUB-1B
94      KM   RUNOFF FROM SUB-1B
95      BA   .009
96      LS   0   93.23
97      UD   .10
      *

98      KK  CP1A1B
99      KM   COMBINE HYDROGRAPHS FROM SUB-1A & SUB-1B
100     HC   2
      *

101     KK  RCP1A1B
102     KM   ROUTE CP1A1B TO CP30
103     RK   1200   0.01   0.013   0   CIRC   2.5
      *

104     KK  SUB-3A
105     KM   RUNOFF FROM SUB-3A
106     BA   .008
107     LS   0   72.00
108     UD   .15
      *

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

109	KK	CP30
110	KM	COMBINE BASINS 3, 4B, DB1, & RCP1A1B
111	HC	5
	*	
112	KK	CP2A
113	KM	COMBINE HYDROGRAPHS FROM CP30 & CP2
114	HC	2
	*	
115	ZZ	

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
LINE		
NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
10	SUB-1	
	.	
	.	
15	.	SUB-2
	.	.
	.	.
19	.	SUB-2A
	.	.
	.	.
23	CP1A.....	
	.	
	.	
26	.	SUB-3B
	.	.
	.	.
31	.	SUB-3C
	.	.
	.	.
36	CP2.....	
	.	
	.	
39	.	BASIN4
	.	V
	.	V
45	.	RCP26
	.	.
	.	.
48	.	BASIN4A
	.	.
	.	.
54	.	CP27.....
	.	.

```

57      .      .      BASIN1A
      .      .      .
      .      .      .
63      .      CP28.....
      .      V
      .      V
66      .      DB1
      .      V
      .      V
73      .      RDB1
      .      .
      .      .
76      .      .      BASIN4B
      .      .      .
      .      .      .
82      .      .      .      BASIN3
      .      .      .      .
      .      .      .      .
88      .      .      .      .      SUB-1A
      .      .      .      .      .
      .      .      .      .      .
93      .      .      .      .      .      SUB-1B
      .      .      .      .      .      .
      .      .      .      .      .      .
98      .      .      .      .      .      CP1A1B.....
      .      .      .      .      .      V
      .      .      .      .      .      V
101     .      .      .      .      .      RCP1A1B
      .      .      .      .      .      .
      .      .      .      .      .      .
104     .      .      .      .      .      .      SUB-3A
      .      .      .      .      .      .      .
      .      .      .      .      .      .      .
109     .      .      CP30.....
      .      .      .
      .      .      .
112     CP2A.....

```

```

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION
1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JAN 1997 *
* VERSION 4.1 *
*
* RUN DATE 09MAY19 TIME 15:59:12 *
*
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*
*****

```

Woody Mountain Campground
 Existing-Conditions HEC-1 Model
 10-year, 6-hour Model
 Woodson Engineering and Surveying
 MAY 2019
 EXISTING CONDITION

8 IO OUTPUT CONTROL VARIABLES

IPRNT 5 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA

NMIN 3 MINUTES IN COMPUTATION INTERVAL
 IDATE 1 0 STARTING DATE
 ITIME 0000 STARTING TIME
 NQ 125 NUMBER OF HYDROGRAPH ORDINATES
 NDDATE 1 0 ENDING DATE
 NDTIME 0612 ENDING TIME
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .05 HOURS
 TOTAL TIME BASE 6.20 HOURS

ENGLISH UNITS

DRAINAGE AREA SQUARE MILES
 PRECIPITATION DEPTH INCHES
 LENGTH, ELEVATION FEET
 FLOW CUBIC FEET PER SECOND
 STORAGE VOLUME ACRE-FEET
 SURFACE AREA ACRES
 TEMPERATURE DEGREES FAHRENHEIT

1

RUNOFF SUMMARY
 FLOW IN CUBIC FEET PER SECOND
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
+	HYDROGRAPH AT								
+		SUB-1	12.	3.20	1.	1.	1.	.01	
+	HYDROGRAPH AT								
+		SUB-2	5.	3.25	1.	1.	1.	.01	
	HYDROGRAPH AT								

+		SUB-2A	12.	3.15	1.	1.	1.	.01		
+	3 COMBINED AT	CP1A	27.	3.15	3.	3.	3.	.03		
+	HYDROGRAPH AT	SUB-3B	7.	3.45	1.	1.	1.	.02		
+	HYDROGRAPH AT	SUB-3C	1.	3.20	0.	0.	0.	.00		
+	3 COMBINED AT	CP2	31.	3.20	4.	4.	4.	.05		
+	HYDROGRAPH AT	BASIN4	2.	3.10	0.	0.	0.	.00		
+	ROUTED TO	RCP26	2.	3.15	0.	0.	0.	.00		
+	HYDROGRAPH AT	BASIN4A	2.	3.20	0.	0.	0.	.00		
+	2 COMBINED AT	CP27	4.	3.15	0.	0.	0.	.00		
+	HYDROGRAPH AT	BASIN1A	2.	3.10	0.	0.	0.	.00		
+	2 COMBINED AT	CP28	6.	3.15	1.	0.	0.	.01		
+	ROUTED TO	DB1	2.	3.45	0.	0.	0.	.01		
+									7053.69	3.45
+	ROUTED TO	RDB1	2.	3.45	0.	0.	0.	.01		
+	HYDROGRAPH AT	BASIN4B	3.	3.10	0.	0.	0.	.00		
+	HYDROGRAPH AT	BASIN3	4.	3.10	0.	0.	0.	.00		
+	HYDROGRAPH AT	SUB-1A	47.	3.25	5.	5.	5.	.05		
+	HYDROGRAPH AT	SUB-1B	17.	3.10	1.	1.	1.	.01		

+	2 COMBINED AT	CP1A1B	60.	3.20	6.	6.	6.	.05
	ROUTED TO							
+		RCP1A1B	58.	3.20	6.	6.	6.	.05
	HYDROGRAPH AT							
+		SUB-3A	2.	3.25	0.	0.	0.	.01
	5 COMBINED AT							
+		CP30	66.	3.20	8.	7.	7.	.07
	2 COMBINED AT							
+		CP2A	97.	3.20	12.	11.	11.	.12

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	DT	INTERPOLATED TO COMPUTATION INTERVAL		VOLUME
							PEAK	TIME TO PEAK	
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)
RCP26	MANE	.79	2.18	187.57	.82	3.00	2.17	189.00	.82

CONTINUITY SUMMARY (AC-FT) - INFLOW= .8735E-01 EXCESS= .0000E+00 OUTFLOW= .8723E-01 BASIN STORAGE= .1745E-03 PERCENT ERROR= -.1

RDB1	MANE	.40	1.99	207.20	.86	3.00	1.99	207.00	.86
------	------	-----	------	--------	-----	------	------	--------	-----

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2303E+00 EXCESS= .0000E+00 OUTFLOW= .2300E+00 BASIN STORAGE= .3864E-03 PERCENT ERROR= .0

RCP1A1B	MANE	.64	59.35	193.37	1.10	3.00	58.41	192.00	1.10
---------	------	-----	-------	--------	------	------	-------	--------	------

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3177E+01 EXCESS= .0000E+00 OUTFLOW= .3173E+01 BASIN STORAGE= .4051E-02 PERCENT ERROR= .0

*** NORMAL END OF HEC-1 ***

```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*       JAN 1997                *
*       VERSION 4.1              *
*
* RUN DATE  24JUN19  TIME 14:18:33 *
*
*****

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```

*****
*
* U.S. ARMY CORPS OF ENGINEERS    *
* HYDROLOGIC ENGINEERING CENTER  *
* 609 SECOND STREET              *
* DAVIS, CALIFORNIA 95616        *
* (916) 756-1104                 *
*
*****

```

```

X   X  XXXXXXXX  XXXXX      X
X   X  X        X   X      XX
X   X  X        X          X
XXXXXXX  XXXX   X          XXXXX  X
X   X  X        X          X
X   X  X        X   X      X
X   X  XXXXXXXX  XXXXX      XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

*** FREE ***

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*DIAGRAM
1 ID Woody Mountain Campground
2 ID Existing-Conditions HEC-1 Model
3 ID 25-year, 6-hour Model
4 ID Woodson Engineering and Surveying
5 ID MAY 2019
6 ID EXISTING CONDITION
7 IT 3 0 0 125
8 IO 5 0 0
9 IN 5 0 0
*

```

10 KK SUB-1
 11 BA 0.011
 12 PH 25 0.19 0.57 1.10 1.76 2.04 2.22 2.58
 13 LS 0 86.55
 14 UD 0.155
 *

15 KK SUB-2
 16 BA 0.008
 17 LS 0 79.72
 18 UD 0.181
 *

19 KK SUB-2A
 20 BA 0.007
 21 LS 0 91.51
 22 UD 0.1
 *

23 KK CP1A
 24 KM COMBINE HYDROGRAPHS FROM SUB-1, SUB-2 & SUB-2A
 25 HC 3
 *

26 KK SUB-3B
 27 KM RUNOFF FROM SUB-3B
 28 BA .024
 29 LS 0 75.49
 30 UD 0.32
 *

31 KK SUB-3C
 32 KM RUNOFF FROM SUB-3C
 33 BA .002
 34 LS 0 75.74
 35 UD 0.15
 *

1

HEC-1 INPUT

PAGE 2

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

36 KK CP2
 37 KM COMBINE HYDROGRAPHS FROM SUB-3B, SUB-3C & CP1A
 38 HC 3
 *

39 KK BASIN4
 40 KM BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
 41 KM RUNOFF FROM BASIN 4
 42 BA .002

```

43      LS      0      83.56
44      UD      .086
      *

45      KK      RCP26
46      KM      ROUTE CP26 TO CP27
47      RK      400      0.01      0.016      0      21      10      10
      *

48      KK      BASIN4A
49      KM      BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
50      KM      RUNOFF FROM BASIN 4A
51      BA      .002
52      LS      0      86.0
53      UD      .136
      *

54      KK      CP27
55      KM      COMBINE BASINS RCP26 & BASIN4A
56      HC      2
      *

57      KK      BASIN1A
58      KM      BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
59      KM      RUNOFF FROM BASIN 1A
60      BA      .001
61      LS      0      90.4
62      UD      .054
      *

63      KK      CP28
64      KM      COMBINE BASINS BASIN1A & CP27
65      HC      2
      *

66      KK      DB1
67      KM      BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
68      KM      DETENTION BASIN 1
69      RS      1      STOR      0
70      SV      0.0      0.02      0.09      0.15      0.23      0.31      0.39      0.40
71      SE      7052.8      7053.0      7053.5      7054.0      7054.5      7055.0      7055.5      7055.52
72      SQ      0.0      0.21      1.30      3.16      4.14      4.93      5.61      5.63
      *

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1

HEC-1 INPUT

PAGE 3

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

73      KK      RDB1
74      KM      ROUTE DB1 TO CP30
75      RK      320      0.01      0.013      0      CIRC      0.5

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*
76      KK  BASIN4B
77      KM   BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
78      KM   RUNOFF FROM BASIN 4B
79      BA   .002
80      LS   0   87.81
81      UD   .071
      *

82      KK  BASIN3
83      KM   BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
84      KM   RUNOFF FROM BASIN 3
85      BA   .002
86      LS   0   90.80
87      UD   .071
      *

88      KK  SUB-1A
89      KM   RUNOFF FROM SUB-1A
90      BA   .045
91      LS   0   87.37
92      UD   .189
      *

93      KK  SUB-1B
94      KM   RUNOFF FROM SUB-1B
95      BA   .009
96      LS   0   93.23
97      UD   .10
      *

98      KK  CP1A1B
99      KM   COMBINE HYDROGRAPHS FROM SUB-1A & SUB-1B
100     HC   2
      *

101     KK  RCP1A1B
102     KM   ROUTE CP1A1B TO CP30
103     RK   1200   0.01   0.013   0   CIRC   2.5
      *

104     KK  SUB-3A
105     KM   RUNOFF FROM SUB-3A
106     BA   .008
107     LS   0   72.00
108     UD   .15
      *

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

109	KK	CP30
110	KM	COMBINE BASINS 3, 4B, DB1, & RCP1A1B
111	HC	5
	*	
112	KK	CP2A
113	KM	COMBINE HYDROGRAPHS FROM CP30 & CP2
114	HC	2
	*	
115	ZZ	

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
LINE		
NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
10	SUB-1	
	.	
	.	
15	.	SUB-2
	.	.
	.	.
19	.	SUB-2A
	.	.
	.	.
23	CP1A.....	
	.	
	.	
26	.	SUB-3B
	.	.
	.	.
31	.	SUB-3C
	.	.
	.	.
36	CP2.....	
	.	
	.	
39	.	BASIN4
	.	V
	.	V
45	.	RCP26
	.	.
	.	.
48	.	BASIN4A
	.	.
	.	.
54	.	CP27.....
	.	.

```

57      .      .      BASIN1A
      .      .      .
      .      .      .
63      .      CP28.....
      .      V
      .      V
66      .      DB1
      .      V
      .      V
73      .      RDB1
      .      .
      .      .
76      .      .      BASIN4B
      .      .      .
      .      .      .
82      .      .      .      BASIN3
      .      .      .      .
      .      .      .      .
88      .      .      .      .      SUB-1A
      .      .      .      .      .
      .      .      .      .      .
93      .      .      .      .      .      SUB-1B
      .      .      .      .      .      .
      .      .      .      .      .      .
98      .      .      .      .      .      CP1A1B.....
      .      .      .      .      .      V
      .      .      .      .      .      V
101     .      .      .      .      .      RCP1A1B
      .      .      .      .      .      .
      .      .      .      .      .      .
104     .      .      .      .      .      .      SUB-3A
      .      .      .      .      .      .      .
      .      .      .      .      .      .      .
109     .      .      CP30.....
      .      .      .
      .      .      .
112     CP2A.....

```

```

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION
1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*   JAN 1997                    *
*   VERSION 4.1                  *
*
* RUN DATE 24JUN19 TIME 14:18:33 *
*
*****

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*****
*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET            *
* DAVIS, CALIFORNIA 95616      *
* (916) 756-1104                *
*
*****

```

Woody Mountain Campground
 Existing-Conditions HEC-1 Model
 25-year, 6-hour Model
 Woodson Engineering and Surveying
 MAY 2019
 EXISTING CONDITION

8 IO OUTPUT CONTROL VARIABLES
 IPRNT 5 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
 NMIN 3 MINUTES IN COMPUTATION INTERVAL
 IDATE 1 0 STARTING DATE
 ITIME 0000 STARTING TIME
 NQ 125 NUMBER OF HYDROGRAPH ORDINATES
 NDDATE 1 0 ENDING DATE
 NDTIME 0612 ENDING TIME
 ICENT 19 CENTURY MARK

 COMPUTATION INTERVAL .05 HOURS
 TOTAL TIME BASE 6.20 HOURS

ENGLISH UNITS
 DRAINAGE AREA SQUARE MILES
 PRECIPITATION DEPTH INCHES
 LENGTH, ELEVATION FEET
 FLOW CUBIC FEET PER SECOND
 STORAGE VOLUME ACRE-FEET
 SURFACE AREA ACRES
 TEMPERATURE DEGREES FAHRENHEIT

1

RUNOFF SUMMARY
 FLOW IN CUBIC FEET PER SECOND
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
+	HYDROGRAPH AT								
+		SUB-1	17.	3.20	2.	2.	2.	.01	
+	HYDROGRAPH AT								
+		SUB-2	8.	3.25	1.	1.	1.	.01	
	HYDROGRAPH AT								

+		SUB-2A	16.	3.15	1.	1.	1.	.01		
+	3 COMBINED AT	CP1A	38.	3.15	4.	4.	4.	.03		
+	HYDROGRAPH AT	SUB-3B	12.	3.40	2.	2.	2.	.02		
+	HYDROGRAPH AT	SUB-3C	2.	3.20	0.	0.	0.	.00		
+	3 COMBINED AT	CP2	46.	3.20	6.	5.	5.	.05		
+	HYDROGRAPH AT	BASIN4	3.	3.15	0.	0.	0.	.00		
+	ROUTED TO	RCP26	3.	3.15	0.	0.	0.	.00		
+	HYDROGRAPH AT	BASIN4A	3.	3.20	0.	0.	0.	.00		
+	2 COMBINED AT	CP27	6.	3.15	1.	1.	1.	.00		
+	HYDROGRAPH AT	BASIN1A	3.	3.10	0.	0.	0.	.00		
+	2 COMBINED AT	CP28	8.	3.15	1.	1.	1.	.01		
+	ROUTED TO	DB1	3.	3.40	1.	1.	1.	.01		
+									7054.01	3.40
+	ROUTED TO	RDB1	3.	3.40	1.	1.	1.	.01		
+	HYDROGRAPH AT	BASIN4B	4.	3.10	0.	0.	0.	.00		
+	HYDROGRAPH AT	BASIN3	5.	3.10	0.	0.	0.	.00		
+	HYDROGRAPH AT	SUB-1A	66.	3.25	7.	7.	7.	.05		
+	HYDROGRAPH AT	SUB-1B	22.	3.15	2.	2.	2.	.01		

+	2 COMBINED AT	CP1A1B	83.	3.20	9.	8.	8.	.05
	ROUTED TO							
+		RCP1A1B	82.	3.20	9.	8.	8.	.05
	HYDROGRAPH AT							
+		SUB-3A	5.	3.25	0.	0.	0.	.01
	5 COMBINED AT							
+		CP30	95.	3.20	10.	10.	10.	.07
	2 COMBINED AT							
+		CP2A	141.	3.20	16.	16.	16.	.12

1

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	DT	INTERPOLATED TO COMPUTATION INTERVAL		VOLUME
							PEAK	TIME TO PEAK	
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)
RCP26	MANE	.64	3.20	189.74	1.15	3.00	3.20	189.00	1.15

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1226E+00 EXCESS= .0000E+00 OUTFLOW= .1226E+00 BASIN STORAGE= .1680E-03 PERCENT ERROR= -.2

RDB1	MANE	.42	3.17	203.94	1.20	3.00	3.17	204.00	1.20
------	------	-----	------	--------	------	------	------	--------	------

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3197E+00 EXCESS= .0000E+00 OUTFLOW= .3192E+00 BASIN STORAGE= .4648E-03 PERCENT ERROR= .0

RCP1A1B	MANE	.56	83.07	192.93	1.47	3.00	81.68	192.00	1.48
---------	------	-----	-------	--------	------	------	-------	--------	------

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4252E+01 EXCESS= .0000E+00 OUTFLOW= .4247E+01 BASIN STORAGE= .5026E-02 PERCENT ERROR= .0

*** NORMAL END OF HEC-1 ***

```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*       JAN 1997                *
*       VERSION 4.1              *
*
* RUN DATE 09MAY19 TIME 15:59:32 *
*
*****

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*****
*
* U.S. ARMY CORPS OF ENGINEERS   *
* HYDROLOGIC ENGINEERING CENTER  *
* 609 SECOND STREET              *
* DAVIS, CALIFORNIA 95616        *
* (916) 756-1104                 *
*
*****

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X   X XXXXXXXX XXXXX           X
X   X X      X      X         XX
X   X X      X      X         X
XXXXXXX XXXX   X      XXXXX   X
X   X X      X      X         X
X   X X      X      X         X
X   X XXXXXXXX XXXXX           XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

*** FREE ***

```

*DIAGRAM
1 ID Woody Mountain Campground
2 ID Existing-Conditions HEC-1 Model
3 ID 100-year, 6-hour Model
4 ID Woodson Engineering and Surveying
5 ID MAY 2019
6 ID EXISTING CONDITION
7 IT 3 0 0 125
8 IO 5 0 0
9 IN 5 0 0
*

```

10 KK SUB-1
 11 BA 0.011
 12 PH 1 0.19 0.71 1.37 2.21 2.56 2.76 3.18
 13 LS 0 86.55
 14 UD 0.155
 *

15 KK SUB-2
 16 BA 0.008
 17 LS 0 79.72
 18 UD 0.181
 *

19 KK SUB-2A
 20 BA 0.007
 21 LS 0 91.51
 22 UD 0.1
 *

23 KK CP1A
 24 KM COMBINE HYDROGRAPHS FROM SUB-1, SUB-2 & SUB-2A
 25 HC 3
 *

26 KK SUB-3B
 27 KM RUNOFF FROM SUB-3B
 28 BA .024
 29 LS 0 75.49
 30 UD 0.32
 *

31 KK SUB-3C
 32 KM RUNOFF FROM SUB-3C
 33 BA .002
 34 LS 0 75.74
 35 UD 0.15
 *

1

HEC-1 INPUT

PAGE 2

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

36 KK CP2
 37 KM COMBINE HYDROGRAPHS FROM SUB-3B, SUB-3C & CP1A
 38 HC 3
 *

39 KK BASIN4
 40 KM BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
 41 KM RUNOFF FROM BASIN 4
 42 BA .002

```

43      LS      0      83.56
44      UD      .086
      *

45      KK      RCP26
46      KM      ROUTE CP26 TO CP27
47      RK      400      0.01      0.016      0      21      10      10
      *

48      KK      BASIN4A
49      KM      BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
50      KM      RUNOFF FROM BASIN 4A
51      BA      .002
52      LS      0      86.0
53      UD      .136
      *

54      KK      CP27
55      KM      COMBINE BASINS RCP26 & BASIN4A
56      HC      2
      *

57      KK      BASIN1A
58      KM      BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
59      KM      RUNOFF FROM BASIN 1A
60      BA      .001
61      LS      0      90.4
62      UD      .054
      *

63      KK      CP28
64      KM      COMBINE BASINS BASIN1A & CP27
65      HC      2
      *

66      KK      DB1
67      KM      BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
68      KM      DETENTION BASIN 1
69      RS      1      STOR      0
70      SV      0.0      0.02      0.09      0.15      0.23      0.31      0.39      0.40
71      SE      7052.8      7053.0      7053.5      7054.0      7054.5      7055.0      7055.5      7055.52
72      SQ      0.0      0.21      1.30      3.16      4.14      4.93      5.61      5.63
      *

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1

HEC-1 INPUT

PAGE 3

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

73      KK      RDB1
74      KM      ROUTE DB1 TO CP30
75      RK      320      0.01      0.013      0      CIRC      0.5

```

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*
76      KK  BASIN4B
77      KM   BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
78      KM   RUNOFF FROM BASIN 4B
79      BA   .002
80      LS   0   87.81
81      UD   .071
      *

82      KK  BASIN3
83      KM   BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
84      KM   RUNOFF FROM BASIN 3
85      BA   .002
86      LS   0   90.80
87      UD   .071
      *

88      KK  SUB-1A
89      KM   RUNOFF FROM SUB-1A
90      BA   .045
91      LS   0   87.37
92      UD   .189
      *

93      KK  SUB-1B
94      KM   RUNOFF FROM SUB-1B
95      BA   .009
96      LS   0   93.23
97      UD   .10
      *

98      KK  CP1A1B
99      KM   COMBINE HYDROGRAPHS FROM SUB-1A & SUB-1B
100     HC   2
      *

101     KK  RCP1A1B
102     KM   ROUTE CP1A1B TO CP30
103     RK   1200   0.01   0.013   0   CIRC   2.5
      *

104     KK  SUB-3A
105     KM   RUNOFF FROM SUB-3A
106     BA   .008
107     LS   0   72.00
108     UD   .15
      *

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

109	KK	CP30
110	KM	COMBINE BASINS 3, 4B, DB1, & RCP1A1B
111	HC	5
	*	
112	KK	CP2A
113	KM	COMBINE HYDROGRAPHS FROM CP30 & CP2
114	HC	2
	*	
115	ZZ	

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
LINE		
NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
10	SUB-1	
	.	
	.	
15	.	SUB-2
	.	.
	.	.
19	.	SUB-2A
	.	.
	.	.
23	CP1A.....	
	.	
	.	
26	.	SUB-3B
	.	.
	.	.
31	.	SUB-3C
	.	.
	.	.
36	CP2.....	
	.	
	.	
39	.	BASIN4
	.	V
	.	V
45	.	RCP26
	.	.
	.	.
48	.	BASIN4A
	.	.
	.	.
54	.	CP27.....
	.	.

```

57      .      .      BASIN1A
      .      .      .
      .      .      .
63      .      CP28.....
      .      V
      .      V
66      .      DB1
      .      V
      .      V
73      .      RDB1
      .      .
      .      .
76      .      .      BASIN4B
      .      .      .
      .      .      .
82      .      .      .      BASIN3
      .      .      .      .
      .      .      .      .
88      .      .      .      .      SUB-1A
      .      .      .      .      .
      .      .      .      .      .
93      .      .      .      .      .      SUB-1B
      .      .      .      .      .      .
      .      .      .      .      .      .
98      .      .      .      .      .      CP1A1B.....
      .      .      .      .      .      V
      .      .      .      .      .      V
101     .      .      .      .      .      RCP1A1B
      .      .      .      .      .      .
      .      .      .      .      .      .
104     .      .      .      .      .      .      SUB-3A
      .      .      .      .      .      .      .
      .      .      .      .      .      .      .
109     .      .      CP30.....
      .      .
      .      .
112     CP2A.....

```

```

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION
1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JAN 1997 *
* VERSION 4.1 *
*
* RUN DATE 09MAY19 TIME 15:59:32 *
*
*****

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*****
*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*
*****

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Woody Mountain Campground
 Existing-Conditions HEC-1 Model
 100-year, 6-hour Model
 Woodson Engineering and Surveying
 MAY 2019
 EXISTING CONDITION

8 IO OUTPUT CONTROL VARIABLES
 IPRNT 5 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
 NMIN 3 MINUTES IN COMPUTATION INTERVAL
 IDATE 1 0 STARTING DATE
 ITIME 0000 STARTING TIME
 NQ 125 NUMBER OF HYDROGRAPH ORDINATES
 NDDATE 1 0 ENDING DATE
 NDTIME 0612 ENDING TIME
 ICENT 19 CENTURY MARK

 COMPUTATION INTERVAL .05 HOURS
 TOTAL TIME BASE 6.20 HOURS

ENGLISH UNITS
 DRAINAGE AREA SQUARE MILES
 PRECIPITATION DEPTH INCHES
 LENGTH, ELEVATION FEET
 FLOW CUBIC FEET PER SECOND
 STORAGE VOLUME ACRE-FEET
 SURFACE AREA ACRES
 TEMPERATURE DEGREES FAHRENHEIT

1

RUNOFF SUMMARY
 FLOW IN CUBIC FEET PER SECOND
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
+	HYDROGRAPH AT								
+		SUB-1	24.	3.20	2.	2.	2.	.01	
+	HYDROGRAPH AT								
+		SUB-2	12.	3.25	1.	1.	1.	.01	
	HYDROGRAPH AT								

+		SUB-2A	22.	3.15	2.	2.	2.	.01		
	3 COMBINED AT									
+		CP1A	54.	3.15	5.	5.	5.	.03		
	HYDROGRAPH AT									
+		SUB-3B	20.	3.40	3.	3.	3.	.02		
	HYDROGRAPH AT									
+		SUB-3C	3.	3.20	0.	0.	0.	.00		
	3 COMBINED AT									
+		CP2	67.	3.20	8.	8.	8.	.05		
	HYDROGRAPH AT									
+		BASIN4	5.	3.10	0.	0.	0.	.00		
	ROUTED TO									
+		RCP26	5.	3.15	0.	0.	0.	.00		
	HYDROGRAPH AT									
+		BASIN4A	4.	3.15	0.	0.	0.	.00		
	2 COMBINED AT									
+		CP27	9.	3.15	1.	1.	1.	.00		
	HYDROGRAPH AT									
+		BASIN1A	3.	3.10	0.	0.	0.	.00		
	2 COMBINED AT									
+		CP28	12.	3.15	1.	1.	1.	.01		
	ROUTED TO									
+		DB1	4.	3.40	1.	1.	1.	.01		
+									7054.42	3.40
	ROUTED TO									
+		RDB1	4.	3.40	1.	1.	1.	.01		
	HYDROGRAPH AT									
+		BASIN4B	6.	3.10	0.	0.	0.	.00		
	HYDROGRAPH AT									
+		BASIN3	7.	3.10	0.	0.	0.	.00		
	HYDROGRAPH AT									
+		SUB-1A	92.	3.25	9.	9.	9.	.05		
	HYDROGRAPH AT									
+		SUB-1B	29.	3.15	2.	2.	2.	.01		

+	2 COMBINED AT	CP1A1B	115.	3.20	12.	11.	11.	.05
	ROUTED TO							
+		RCP1A1B	113.	3.20	12.	11.	11.	.05
	HYDROGRAPH AT							
+		SUB-3A	8.	3.20	1.	1.	1.	.01
	5 COMBINED AT							
+		CP30	132.	3.20	14.	14.	14.	.07
	2 COMBINED AT							
+		CP2A	199.	3.20	22.	22.	22.	.12

1

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	DT	INTERPOLATED TO COMPUTATION INTERVAL		VOLUME
							PEAK	TIME TO PEAK	
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)
RCP26	MANE	.60	4.66	187.74	1.63	3.00	4.62	189.00	1.63

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1740E+00 EXCESS= .0000E+00 OUTFLOW= .1741E+00 BASIN STORAGE= .2036E-03 PERCENT ERROR= -.2

RDB1	MANE	.44	3.98	204.47	1.68	3.00	3.98	204.00	1.68
------	------	-----	------	--------	------	------	------	--------	------

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4494E+00 EXCESS= .0000E+00 OUTFLOW= .4489E+00 BASIN STORAGE= .5692E-03 PERCENT ERROR= .0

RCP1A1B	MANE	.43	114.50	192.75	2.00	3.00	112.68	192.00	2.00
---------	------	-----	--------	--------	------	------	--------	--------	------

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5777E+01 EXCESS= .0000E+00 OUTFLOW= .5773E+01 BASIN STORAGE= .5669E-02 PERCENT ERROR= .0

*** NORMAL END OF HEC-1 ***

```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*       JAN 1997                *
*       VERSION 4.1              *
*
* RUN DATE 09MAY19 TIME 16:03:06 *
*
*****

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*****
*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET           *
* DAVIS, CALIFORNIA 95616     *
* (916) 756-1104             *
*
*****

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X   X XXXXXXXX XXXXX      X
X   X X      X      X    XX
X   X X      X      X    X
XXXXXXX XXXX  X      XXXXX X
X   X X      X      X    X
X   X X      X      X    X
X   X XXXXXXXX XXXXX      XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

*** FREE ***

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*DIAGRAM
1 ID Woody Mountain Campground
2 ID Proposed-Conditions without Detention Basin HEC-1 Model
3 ID 10-year, 6-hour Model
4 ID Woodson Engineering and Surveying
5 ID MAY 2019
6 ID PROPOSED CONDITION (WITHOUT DETENTION BASIN)
7 IT 3 0 0 125
8 IO 5 0 0
9 IN 5 0 0
*

```

10 KK SUB-1
 11 BA 0.011
 12 PH 10 0.19 0.48 0.87 1.46 1.70 1.86 2.16
 13 LS 0 86.55
 14 UD 0.155
 *

15 KK SUB-2
 16 BA 0.008
 17 LS 0 79.72
 18 UD 0.181
 *

19 KK SUB-2A
 20 BA 0.007
 21 LS 0 95.25
 22 UD 0.1
 *

23 KK CP1A
 24 KM COMBINE HYDROGRAPHS FROM SUB-1, SUB-2 & SUB-2A
 25 HC 3
 *

26 KK SUB-3B
 27 KM RUNOFF FROM SUB-3B
 28 BA .024
 29 LS 0 86.44
 30 UD 0.24
 *

31 KK SUB-3C
 32 KM RUNOFF FROM SUB-3C
 33 BA .002
 34 LS 0 92.30
 35 UD 0.10
 *

1

HEC-1 INPUT

PAGE 2

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

36 KK CP2
 37 KM COMBINE HYDROGRAPHS FROM SUB-3B, SUB-3C & CP1A
 38 HC 3
 *

39 KK BASIN4
 40 KM BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
 41 KM RUNOFF FROM BASIN 4
 42 BA .002

```

43      LS      0    83.56
44      UD      .086
      *

45      KK      RCP26
46      KM      ROUTE CP26 TO CP27
47      RK      400    0.01    0.016      0    21    10    10
      *

48      KK      BASIN4A
49      KM      BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
50      KM      RUNOFF FROM BASIN 4A
51      BA      .002
52      LS      0    86.0
53      UD      .136
      *

54      KK      CP27
55      KM      COMBINE BASINS RCP26 & BASIN4A
56      HC      2
      *

57      KK      BASIN1A
58      KM      BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
59      KM      RUNOFF FROM BASIN 1A
60      BA      .001
61      LS      0    90.4
62      UD      .054
      *

63      KK      CP28
64      KM      COMBINE BASINS BASIN1A & CP27
65      HC      2
      *

66      KK      DB1
67      KM      BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
68      KM      DETENTION BASIN 1
69      RS      1    STOR      0
70      SV      0.0    0.02    0.09    0.15    0.23    0.31    0.39    0.40
71      SE      7052.8  7053.0  7053.5  7054.0  7054.5  7055.0  7055.5  7055.52
72      SQ      0.0    0.21    1.30    3.16    4.14    4.93    5.61    5.63
      *

```

1

HEC-1 INPUT

PAGE 3

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

73      KK      RDB1
74      KM      ROUTE DB1 TO CP30
75      RK      320    0.01    0.013      0    CIRC    0.5

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*
76      KK  BASIN4B
77      KM  BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
78      KM  RUNOFF FROM BASIN 4B
79      BA  .002
80      LS  0   87.81
81      UD  .071
      *

82      KK  BASIN3
83      KM  BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
84      KM  RUNOFF FROM BASIN 3
85      BA  .002
86      LS  0   90.80
87      UD  .071
      *

88      KK  SUB-1A
89      KM  RUNOFF FROM SUB-1A
90      BA  .045
91      LS  0   87.37
92      UD  .189
      *

93      KK  SUB-1B
94      KM  RUNOFF FROM SUB-1B
95      BA  .009
96      LS  0   93.46
97      UD  .10
      *

98      KK  CP1A1B
99      KM  COMBINE SUB-1A & SUB-1B
100     HC  2
      *

101     KK  RCP1A1B
102     KM  ROUTE CP1A1B TO CP30
103     RK  1200  0.01  0.013  0  CIRC  2.5
      *

104     KK  SUB-3A
105     KM  RUNOFF FROM SUB-3A
106     BA  .008
107     LS  0   78.72
108     UD  .10
      *

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

109	KK	CP30
110	KM	COMBINE HYDROGRAPHS FROM BASINS 3, 4B, DB1, SUB-3A& CP1A1B
111	HC	5
	*	
112	KK	CP2A
113	KM	COMBINE HYDROGRAPHS FROM CP30 & CP-2
114	HC	2
	*	
115	ZZ	

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
LINE		
NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
10	SUB-1	
	.	
	.	
15	.	SUB-2
	.	.
	.	.
19	.	SUB-2A
	.	.
	.	.
23	CP1A.....	
	.	
	.	
26	.	SUB-3B
	.	.
	.	.
31	.	SUB-3C
	.	.
	.	.
36	CP2.....	
	.	
	.	
39	.	BASIN4
	.	V
	.	V
45	.	RCP26
	.	.
	.	.
48	.	BASIN4A
	.	.
	.	.
54	.	CP27.....
	.	.

```

57      .      .      BASIN1A
      .      .      .
      .      .      .
63      .      CP28.....
      .      V
      .      V
66      .      DB1
      .      V
      .      V
73      .      RDB1
      .      .
      .      .
76      .      .      BASIN4B
      .      .      .
      .      .      .
82      .      .      .      BASIN3
      .      .      .      .
      .      .      .      .
88      .      .      .      .      SUB-1A
      .      .      .      .      .
      .      .      .      .      .
93      .      .      .      .      .      SUB-1B
      .      .      .      .      .      .
      .      .      .      .      .      .
98      .      .      .      .      .      CP1A1B.....
      .      .      .      .      .      V
      .      .      .      .      .      V
101     .      .      .      .      .      RCP1A1B
      .      .      .      .      .      .
      .      .      .      .      .      .
104     .      .      .      .      .      .      SUB-3A
      .      .      .      .      .      .      .
      .      .      .      .      .      .      .
109     .      .      CP30.....
      .      .      .
      .      .      .
112     CP2A.....

```

```

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION
1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JAN 1997 *
* VERSION 4.1 *
*
* RUN DATE 09MAY19 TIME 16:03:06 *
*
*****

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```

*****
*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*
*****

```

Woody Mountain Campground
Proposed-Conditions without Detention Basin HEC-1 Model
10-year, 6-hour Model
Woodson Engineering and Surveying
MAY 2019
PROPOSED CONDITION (WITHOUT DETENTION BASIN)

8 IO OUTPUT CONTROL VARIABLES
 IPRNT 5 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
 NMIN 3 MINUTES IN COMPUTATION INTERVAL
 IDATE 1 0 STARTING DATE
 ITIME 0000 STARTING TIME
 NQ 125 NUMBER OF HYDROGRAPH ORDINATES
 NDDATE 1 0 ENDING DATE
 NDTIME 0612 ENDING TIME
 ICENT 19 CENTURY MARK

 COMPUTATION INTERVAL .05 HOURS
 TOTAL TIME BASE 6.20 HOURS

ENGLISH UNITS
DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW CUBIC FEET PER SECOND
STORAGE VOLUME ACRE-FEET
SURFACE AREA ACRES
TEMPERATURE DEGREES FAHRENHEIT

1

RUNOFF SUMMARY
FLOW IN CUBIC FEET PER SECOND
TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
+	HYDROGRAPH AT								
+		SUB-1	12.	3.20	1.	1.	1.	.01	
+	HYDROGRAPH AT								
+		SUB-2	5.	3.25	1.	1.	1.	.01	
	HYDROGRAPH AT								

+		SUB-2A	15.	3.10	1.	1.	1.	.01		
+	3 COMBINED AT	CP1A	29.	3.15	3.	3.	3.	.03		
+	HYDROGRAPH AT	SUB-3B	21.	3.30	3.	2.	2.	.02		
+	HYDROGRAPH AT	SUB-3C	4.	3.15	0.	0.	0.	.00		
+	3 COMBINED AT	CP2	49.	3.20	6.	6.	6.	.05		
+	HYDROGRAPH AT	BASIN4	2.	3.10	0.	0.	0.	.00		
+	ROUTED TO	RCP26	2.	3.15	0.	0.	0.	.00		
+	HYDROGRAPH AT	BASIN4A	2.	3.20	0.	0.	0.	.00		
+	2 COMBINED AT	CP27	4.	3.15	0.	0.	0.	.00		
+	HYDROGRAPH AT	BASIN1A	2.	3.10	0.	0.	0.	.00		
+	2 COMBINED AT	CP28	6.	3.15	1.	0.	0.	.01		
+	ROUTED TO	DB1	2.	3.45	0.	0.	0.	.01		
+									7053.69	3.45
+	ROUTED TO	RDB1	2.	3.45	0.	0.	0.	.01		
+	HYDROGRAPH AT	BASIN4B	3.	3.10	0.	0.	0.	.00		
+	HYDROGRAPH AT	BASIN3	4.	3.10	0.	0.	0.	.00		
+	HYDROGRAPH AT	SUB-1A	47.	3.25	5.	5.	5.	.05		
+	HYDROGRAPH AT	SUB-1B	17.	3.10	1.	1.	1.	.01		

+	2 COMBINED AT	CP1A1B	60.	3.20	6.	6.	6.	.05
	ROUTED TO							
+		RCP1A1B	59.	3.20	6.	6.	6.	.05
	HYDROGRAPH AT							
+		SUB-3A	6.	3.15	1.	0.	0.	.01
	5 COMBINED AT							
+		CP30	69.	3.20	8.	8.	8.	.07
	2 COMBINED AT							
+		CP2A	118.	3.20	14.	13.	13.	.12

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	DT	INTERPOLATED TO COMPUTATION INTERVAL		VOLUME
							PEAK	TIME TO PEAK	
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)
RCP26	MANE	.79	2.18	187.57	.82	3.00	2.17	189.00	.82

CONTINUITY SUMMARY (AC-FT) - INFLOW= .8735E-01 EXCESS= .0000E+00 OUTFLOW= .8723E-01 BASIN STORAGE= .1745E-03 PERCENT ERROR= -.1

RDB1	MANE	.40	1.99	207.20	.86	3.00	1.99	207.00	.86
------	------	-----	------	--------	-----	------	------	--------	-----

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2303E+00 EXCESS= .0000E+00 OUTFLOW= .2300E+00 BASIN STORAGE= .3864E-03 PERCENT ERROR= .0

RCP1A1B	MANE	.52	59.64	192.98	1.11	3.00	58.58	192.00	1.11
---------	------	-----	-------	--------	------	------	-------	--------	------

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3186E+01 EXCESS= .0000E+00 OUTFLOW= .3184E+01 BASIN STORAGE= .3936E-02 PERCENT ERROR= -.1

*** NORMAL END OF HEC-1 ***

```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
*       JAN 1997
*       VERSION 4.1
*
* RUN DATE 09MAY19 TIME 15:59:12
*
*****

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```

*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****

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X   X XXXXXXXX XXXXX      X
X   X X      X      X    XX
X   X X      X      X    X
XXXXXXX XXXX  X      XXXXX  X
X   X X      X      X    X
X   X X      X      X    X
X   X XXXXXXXX XXXXX      XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

*** FREE ***

```

*DIAGRAM
1 ID Woody Mountain Campground
2 ID Existing-Conditions HEC-1 Model
3 ID 10-year, 6-hour Model
4 ID Woodson Engineering and Surveying
5 ID MAY 2019
6 ID EXISTING CONDITION
7 IT 3 0 0 125
8 IO 5 0 0
9 IN 5 0 0
*

```

10 KK SUB-1
 11 BA 0.011
 12 PH 10 0.19 0.48 0.87 1.46 1.70 1.86 2.16
 13 LS 0 86.55
 14 UD 0.155
 *

15 KK SUB-2
 16 BA 0.008
 17 LS 0 79.72
 18 UD 0.181
 *

19 KK SUB-2A
 20 BA 0.007
 21 LS 0 91.51
 22 UD 0.1
 *

23 KK CP1A
 24 KM COMBINE HYDROGRAPHS FROM SUB-1, SUB-2 & SUB-2A
 25 HC 3
 *

26 KK SUB-3B
 27 KM RUNOFF FROM SUB-3B
 28 BA .024
 29 LS 0 75.49
 30 UD 0.32
 *

31 KK SUB-3C
 32 KM RUNOFF FROM SUB-3C
 33 BA .002
 34 LS 0 75.74
 35 UD 0.15
 *

1

HEC-1 INPUT

PAGE 2

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

36 KK CP2
 37 KM COMBINE HYDROGRAPHS FROM SUB-3B, SUB-3C & CP1A
 38 HC 3
 *

39 KK BASIN4
 40 KM BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
 41 KM RUNOFF FROM BASIN 4
 42 BA .002

```

43      LS      0      83.56
44      UD      .086
      *

45      KK      RCP26
46      KM      ROUTE CP26 TO CP27
47      RK      400      0.01      0.016      0      21      10      10
      *

48      KK      BASIN4A
49      KM      BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
50      KM      RUNOFF FROM BASIN 4A
51      BA      .002
52      LS      0      86.0
53      UD      .136
      *

54      KK      CP27
55      KM      COMBINE BASINS RCP26 & BASIN4A
56      HC      2
      *

57      KK      BASIN1A
58      KM      BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
59      KM      RUNOFF FROM BASIN 1A
60      BA      .001
61      LS      0      90.4
62      UD      .054
      *

63      KK      CP28
64      KM      COMBINE BASINS BASIN1A & CP27
65      HC      2
      *

66      KK      DB1
67      KM      BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
68      KM      DETENTION BASIN 1
69      RS      1      STOR      0
70      SV      0.0      0.02      0.09      0.15      0.23      0.31      0.39      0.40
71      SE      7052.8      7053.0      7053.5      7054.0      7054.5      7055.0      7055.5      7055.52
72      SQ      0.0      0.21      1.30      3.16      4.14      4.93      5.61      5.63
      *

```

1

HEC-1 INPUT

PAGE 3

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

73      KK      RDB1
74      KM      ROUTE DB1 TO CP30
75      RK      320      0.01      0.013      0      CIRC      0.5

```

```

*
76      KK  BASIN4B
77      KM   BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
78      KM   RUNOFF FROM BASIN 4B
79      BA   .002
80      LS   0   87.81
81      UD   .071
      *

82      KK  BASIN3
83      KM   BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
84      KM   RUNOFF FROM BASIN 3
85      BA   .002
86      LS   0   90.80
87      UD   .071
      *

88      KK  SUB-1A
89      KM   RUNOFF FROM SUB-1A
90      BA   .045
91      LS   0   87.37
92      UD   .189
      *

93      KK  SUB-1B
94      KM   RUNOFF FROM SUB-1B
95      BA   .009
96      LS   0   93.23
97      UD   .10
      *

98      KK  CP1A1B
99      KM   COMBINE HYDROGRAPHS FROM SUB-1A & SUB-1B
100     HC   2
      *

101     KK  RCP1A1B
102     KM   ROUTE CP1A1B TO CP30
103     RK   1200   0.01   0.013   0   CIRC   2.5
      *

104     KK  SUB-3A
105     KM   RUNOFF FROM SUB-3A
106     BA   .008
107     LS   0   72.00
108     UD   .15
      *

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

109	KK	CP30
110	KM	COMBINE BASINS 3, 4B, DB1, & RCP1A1B
111	HC	5
	*	
112	KK	CP2A
113	KM	COMBINE HYDROGRAPHS FROM CP30 & CP2
114	HC	2
	*	
115	ZZ	

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
LINE		
NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
10	SUB-1	
	.	
	.	
15	.	SUB-2
	.	.
	.	.
19	.	SUB-2A
	.	.
	.	.
23	CP1A.....	
	.	
	.	
26	.	SUB-3B
	.	.
	.	.
31	.	SUB-3C
	.	.
	.	.
36	CP2.....	
	.	
	.	
39	.	BASIN4
	.	V
	.	V
45	.	RCP26
	.	.
	.	.
48	.	BASIN4A
	.	.
	.	.
54	.	CP27.....
	.	.

```

57      .      .      BASIN1A
      .      .      .
      .      .      .
63      .      CP28.....
      .      V
      .      V
66      .      DB1
      .      V
      .      V
73      .      RDB1
      .      .
      .      .
76      .      .      BASIN4B
      .      .      .
      .      .      .
82      .      .      .      BASIN3
      .      .      .      .
      .      .      .      .
88      .      .      .      .      SUB-1A
      .      .      .      .      .
      .      .      .      .      .
93      .      .      .      .      .      SUB-1B
      .      .      .      .      .      .
      .      .      .      .      .      .
98      .      .      .      .      .      CP1A1B.....
      .      .      .      .      .      V
      .      .      .      .      .      V
101     .      .      .      .      .      RCP1A1B
      .      .      .      .      .      .
      .      .      .      .      .      .
104     .      .      .      .      .      .      SUB-3A
      .      .      .      .      .      .      .
      .      .      .      .      .      .      .
109     .      .      CP30.....
      .      .      .
      .      .      .
112     CP2A.....

```

```

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION
1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JAN 1997 *
* VERSION 4.1 *
*
* RUN DATE 09MAY19 TIME 15:59:12 *
*
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*
*****

```

Woody Mountain Campground
 Existing-Conditions HEC-1 Model
 10-year, 6-hour Model
 Woodson Engineering and Surveying
 MAY 2019
 EXISTING CONDITION

8 IO OUTPUT CONTROL VARIABLES

IPRNT 5 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA

NMIN 3 MINUTES IN COMPUTATION INTERVAL
 IDATE 1 0 STARTING DATE
 ITIME 0000 STARTING TIME
 NQ 125 NUMBER OF HYDROGRAPH ORDINATES
 NDDATE 1 0 ENDING DATE
 NDTIME 0612 ENDING TIME
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .05 HOURS
 TOTAL TIME BASE 6.20 HOURS

ENGLISH UNITS

DRAINAGE AREA SQUARE MILES
 PRECIPITATION DEPTH INCHES
 LENGTH, ELEVATION FEET
 FLOW CUBIC FEET PER SECOND
 STORAGE VOLUME ACRE-FEET
 SURFACE AREA ACRES
 TEMPERATURE DEGREES FAHRENHEIT

1

RUNOFF SUMMARY
 FLOW IN CUBIC FEET PER SECOND
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
+	HYDROGRAPH AT								
+		SUB-1	12.	3.20	1.	1.	1.	.01	
+	HYDROGRAPH AT								
+		SUB-2	5.	3.25	1.	1.	1.	.01	
	HYDROGRAPH AT								

+		SUB-2A	12.	3.15	1.	1.	1.	.01		
+	3 COMBINED AT	CP1A	27.	3.15	3.	3.	3.	.03		
+	HYDROGRAPH AT	SUB-3B	7.	3.45	1.	1.	1.	.02		
+	HYDROGRAPH AT	SUB-3C	1.	3.20	0.	0.	0.	.00		
+	3 COMBINED AT	CP2	31.	3.20	4.	4.	4.	.05		
+	HYDROGRAPH AT	BASIN4	2.	3.10	0.	0.	0.	.00		
+	ROUTED TO	RCP26	2.	3.15	0.	0.	0.	.00		
+	HYDROGRAPH AT	BASIN4A	2.	3.20	0.	0.	0.	.00		
+	2 COMBINED AT	CP27	4.	3.15	0.	0.	0.	.00		
+	HYDROGRAPH AT	BASIN1A	2.	3.10	0.	0.	0.	.00		
+	2 COMBINED AT	CP28	6.	3.15	1.	0.	0.	.01		
+	ROUTED TO	DB1	2.	3.45	0.	0.	0.	.01		
+									7053.69	3.45
+	ROUTED TO	RDB1	2.	3.45	0.	0.	0.	.01		
+	HYDROGRAPH AT	BASIN4B	3.	3.10	0.	0.	0.	.00		
+	HYDROGRAPH AT	BASIN3	4.	3.10	0.	0.	0.	.00		
+	HYDROGRAPH AT	SUB-1A	47.	3.25	5.	5.	5.	.05		
+	HYDROGRAPH AT	SUB-1B	17.	3.10	1.	1.	1.	.01		

+	2 COMBINED AT	CP1A1B	60.	3.20	6.	6.	6.	.05
	ROUTED TO							
+		RCP1A1B	58.	3.20	6.	6.	6.	.05
	HYDROGRAPH AT							
+		SUB-3A	2.	3.25	0.	0.	0.	.01
	5 COMBINED AT							
+		CP30	66.	3.20	8.	7.	7.	.07
	2 COMBINED AT							
+		CP2A	97.	3.20	12.	11.	11.	.12

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	DT	INTERPOLATED TO COMPUTATION INTERVAL		VOLUME
							PEAK	TIME TO PEAK	
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)
RCP26	MANE	.79	2.18	187.57	.82	3.00	2.17	189.00	.82

CONTINUITY SUMMARY (AC-FT) - INFLOW= .8735E-01 EXCESS= .0000E+00 OUTFLOW= .8723E-01 BASIN STORAGE= .1745E-03 PERCENT ERROR= -.1

RDB1	MANE	.40	1.99	207.20	.86	3.00	1.99	207.00	.86
------	------	-----	------	--------	-----	------	------	--------	-----

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2303E+00 EXCESS= .0000E+00 OUTFLOW= .2300E+00 BASIN STORAGE= .3864E-03 PERCENT ERROR= .0

RCP1A1B	MANE	.64	59.35	193.37	1.10	3.00	58.41	192.00	1.10
---------	------	-----	-------	--------	------	------	-------	--------	------

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3177E+01 EXCESS= .0000E+00 OUTFLOW= .3173E+01 BASIN STORAGE= .4051E-02 PERCENT ERROR= .0

*** NORMAL END OF HEC-1 ***

```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*       JAN 1997                *
*       VERSION 4.1              *
*
* RUN DATE 09MAY19 TIME 16:03:27 *
*
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET            *
* DAVIS, CALIFORNIA 95616      *
* (916) 756-1104               *
*
*****

```

```

X   X XXXXXXXX XXXXX           X
X   X X           X   X       XX
X   X X           X           X
XXXXXXX XXXX   X           XXXXX X
X   X X           X           X
X   X X           X   X       X
X   X XXXXXXXX XXXXX           XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

*** FREE ***

```

*DIAGRAM
1 ID Woody Mountain Campground
2 ID Proposed-Conditions without Detention Basin HEC-1 Model
3 ID 100-year, 6-hour Model
4 ID Woodson Engineering and Surveying
5 ID Feb 2019
6 ID PROPOSED CONDITION (WITHOUT DETENTION BASIN)
7 IT 3 0 0 125
8 IO 5 0 0
9 IN 5 0 0
*

```

10 KK SUB-1
 11 BA 0.011
 12 PH 1 0.19 0.71 1.37 2.21 2.56 2.76 3.18
 13 LS 0 86.55
 14 UD 0.155
 *

15 KK SUB-2
 16 BA 0.008
 17 LS 0 79.72
 18 UD 0.181
 *

19 KK SUB-2A
 20 BA 0.007
 21 LS 0 95.25
 22 UD 0.1
 *

23 KK CP1A
 24 KM COMBINE HYDROGRAPHS FROM SUB-1, SUB-2 & SUB-2A
 25 HC 3
 *

26 KK SUB-3B
 27 KM RUNOFF FROM SUB-3B
 28 BA .024
 29 LS 0 86.44
 30 UD 0.24
 *

31 KK SUB-3C
 32 KM RUNOFF FROM SUB-3C
 33 BA .002
 34 LS 0 92.30
 35 UD 0.10
 *

1

HEC-1 INPUT

PAGE 2

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

36 KK CP2
 37 KM COMBINE HYDROGRAPHS FROM SUB-3B, SUB-3C & CP1A
 38 HC 3
 *

39 KK BASIN4
 40 KM BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
 41 KM RUNOFF FROM BASIN 4
 42 BA .002

```

43      LS      0    83.56
44      UD      .086
      *

45      KK      RCP26
46      KM      ROUTE CP26 TO CP27
47      RK      400    0.01    0.016      0      21      10      10
      *

48      KK      BASIN4A
49      KM      BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
50      KM      RUNOFF FROM BASIN 4A
51      BA      .002
52      LS      0      86.0
53      UD      .136
      *

54      KK      CP27
55      KM      COMBINE BASINS RCP26 & BASIN4A
56      HC      2
      *

57      KK      BASIN1A
58      KM      BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
59      KM      RUNOFF FROM BASIN 1A
60      BA      .001
61      LS      0      90.4
62      UD      .054
      *

63      KK      CP28
64      KM      COMBINE BASINS BASIN1A & CP27
65      HC      2
      *

66      KK      DB1
67      KM      BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
68      KM      DETENTION BASIN 1
69      RS      1      STOR      0
70      SV      0.0    0.02    0.09    0.15    0.23    0.31      0.39    0.40
71      SE      7052.8  7053.0  7053.5  7054.0  7054.5  7055.0  7055.5  7055.52
72      SQ      0.0    0.21    1.30    3.16    4.14    4.93      5.61    5.63
      *

```

1

HEC-1 INPUT

PAGE 3

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

73      KK      RDB1
74      KM      ROUTE DB1 TO CP30
75      RK      320    0.01    0.013      0      CIRC    0.5

```

```

*
76      KK  BASIN4B
77      KM   BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
78      KM   RUNOFF FROM BASIN 4B
79      BA   .002
80      LS    0   87.81
81      UD   .071
      *

82      KK  BASIN3
83      KM   BASIN REFERENCED FROM PRESIDIO IN PINES STUDY
84      KM   RUNOFF FROM BASIN 3
85      BA   .002
86      LS    0   90.80
87      UD   .071
      *

88      KK  SUB-1A
89      KM   RUNOFF FROM SUB-1A
90      BA   .045
91      LS    0   87.37
92      UD   .189
      *

93      KK  SUB-1B
94      KM   RUNOFF FROM SUB-1B
95      BA   .009
96      LS    0   93.46
97      UD   .10
      *

98      KK  CP1A1B
99      KM   COMBINE SUB-1A & SUB-1B
100     HC    2
      *

101     KK  RCP1A1B
102     KM   ROUTE CP1A1B TO CP30
103     RK   1200   0.01   0.013   0   CIRC   2.5
      *

104     KK  SUB-3A
105     KM   RUNOFF FROM SUB-3A
106     BA   .008
107     LS    0   78.72
108     UD   .10
      *

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

109	KK	CP30
110	KM	COMBINE HYDROGRAPHS FROM BASINS 3, 4B, DB1, SUB-3A& CP1A1B
111	HC	5
	*	
112	KK	CP2A
113	KM	COMBINE HYDROGRAPHS FROM CP30 & CP-2
114	HC	2
	*	
115	ZZ	

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
LINE		
NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
10	SUB-1	
	.	
	.	
15	.	SUB-2
	.	.
	.	.
19	.	SUB-2A
	.	.
	.	.
23	CP1A.....	
	.	
	.	
26	.	SUB-3B
	.	.
	.	.
31	.	SUB-3C
	.	.
	.	.
36	CP2.....	
	.	
	.	
39	.	BASIN4
	.	V
	.	V
45	.	RCP26
	.	.
	.	.
48	.	BASIN4A
	.	.
	.	.
54	.	CP27.....
	.	.

```

57      .      .      BASIN1A
      .      .      .
      .      .      .
63      .      CP28.....
      .      V
      .      V
66      .      DB1
      .      V
      .      V
73      .      RDB1
      .      .
      .      .
76      .      .      BASIN4B
      .      .      .
      .      .      .
82      .      .      .      BASIN3
      .      .      .      .
      .      .      .      .
88      .      .      .      .      SUB-1A
      .      .      .      .      .
      .      .      .      .      .
93      .      .      .      .      .      SUB-1B
      .      .      .      .      .      .
      .      .      .      .      .      .
98      .      .      .      .      .      CP1A1B.....
      .      .      .      .      .      V
      .      .      .      .      .      V
101     .      .      .      .      .      RCP1A1B
      .      .      .      .      .      .
      .      .      .      .      .      .
104     .      .      .      .      .      .      SUB-3A
      .      .      .      .      .      .      .
      .      .      .      .      .      .      .
109     .      .      CP30.....
      .      .
      .      .
112     CP2A.....

```

```

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION
1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JAN 1997 *
* VERSION 4.1 *
*
* RUN DATE 09MAY19 TIME 16:03:27 *
*
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*
*****

```

Woody Mountain Campground
 Proposed-Conditions without Detention Basin HEC-1 Model
 100-year, 6-hour Model
 Woodson Engineering and Surveying
 Feb 2019
 PROPOSED CONDITION (WITHOUT DETENTION BASIN)

8 IO OUTPUT CONTROL VARIABLES
 IPRNT 5 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
 NMIN 3 MINUTES IN COMPUTATION INTERVAL
 IDATE 1 0 STARTING DATE
 ITIME 0000 STARTING TIME
 NQ 125 NUMBER OF HYDROGRAPH ORDINATES
 NDDATE 1 0 ENDING DATE
 NDTIME 0612 ENDING TIME
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .05 HOURS
 TOTAL TIME BASE 6.20 HOURS

ENGLISH UNITS
 DRAINAGE AREA SQUARE MILES
 PRECIPITATION DEPTH INCHES
 LENGTH, ELEVATION FEET
 FLOW CUBIC FEET PER SECOND
 STORAGE VOLUME ACRE-FEET
 SURFACE AREA ACRES
 TEMPERATURE DEGREES FAHRENHEIT

1

RUNOFF SUMMARY
 FLOW IN CUBIC FEET PER SECOND
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
+	HYDROGRAPH AT								
+		SUB-1	24.	3.20	2.	2.	2.	.01	
+	HYDROGRAPH AT								
+		SUB-2	12.	3.25	1.	1.	1.	.01	
	HYDROGRAPH AT								

+		SUB-2A	24.	3.10	2.	2.	2.	.01		
+	3 COMBINED AT	CP1A	56.	3.15	5.	5.	5.	.03		
+	HYDROGRAPH AT	SUB-3B	42.	3.30	5.	5.	5.	.02		
+	HYDROGRAPH AT	SUB-3C	6.	3.15	1.	0.	0.	.00		
+	3 COMBINED AT	CP2	97.	3.20	11.	10.	10.	.05		
+	HYDROGRAPH AT	BASIN4	5.	3.10	0.	0.	0.	.00		
+	ROUTED TO	RCP26	5.	3.15	0.	0.	0.	.00		
+	HYDROGRAPH AT	BASIN4A	4.	3.15	0.	0.	0.	.00		
+	2 COMBINED AT	CP27	9.	3.15	1.	1.	1.	.00		
+	HYDROGRAPH AT	BASIN1A	3.	3.10	0.	0.	0.	.00		
+	2 COMBINED AT	CP28	12.	3.15	1.	1.	1.	.01		
+	ROUTED TO	DB1	4.	3.40	1.	1.	1.	.01		
+									7054.42	3.40
+	ROUTED TO	RDB1	4.	3.40	1.	1.	1.	.01		
+	HYDROGRAPH AT	BASIN4B	6.	3.10	0.	0.	0.	.00		
+	HYDROGRAPH AT	BASIN3	7.	3.10	0.	0.	0.	.00		
+	HYDROGRAPH AT	SUB-1A	92.	3.25	9.	9.	9.	.05		
+	HYDROGRAPH AT	SUB-1B	29.	3.15	2.	2.	2.	.01		

+	2 COMBINED AT	CP1A1B	115.	3.20	12.	11.	11.	.05
	ROUTED TO							
+		RCP1A1B	113.	3.20	12.	11.	11.	.05
	HYDROGRAPH AT							
+		SUB-3A	14.	3.15	1.	1.	1.	.01
	5 COMBINED AT							
+		CP30	137.	3.20	15.	14.	14.	.07
	2 COMBINED AT							
+		CP2A	234.	3.20	25.	24.	24.	.12

1

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	DT	INTERPOLATED TO COMPUTATION INTERVAL		VOLUME
							PEAK	TIME TO PEAK	
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)
RCP26	MANE	.60	4.66	187.74	1.63	3.00	4.62	189.00	1.63

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1740E+00 EXCESS= .0000E+00 OUTFLOW= .1741E+00 BASIN STORAGE= .2036E-03 PERCENT ERROR= -.2

RDB1	MANE	.44	3.98	204.47	1.68	3.00	3.98	204.00	1.68
------	------	-----	------	--------	------	------	------	--------	------

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4494E+00 EXCESS= .0000E+00 OUTFLOW= .4489E+00 BASIN STORAGE= .5692E-03 PERCENT ERROR= .0

RCP1A1B	MANE	.46	114.50	193.12	2.01	3.00	112.83	192.00	2.01
---------	------	-----	--------	--------	------	------	--------	--------	------

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5788E+01 EXCESS= .0000E+00 OUTFLOW= .5784E+01 BASIN STORAGE= .5657E-02 PERCENT ERROR= .0

*** NORMAL END OF HEC-1 ***

Woody Mountain Campground

LID Basin -1: Elevation Volume Summary

Elev.	Area		Increase in Depth (ft)	Incremental Area (sq.ft)	Incremental Volume (cu.ft)	Cumulative Volume	
	(sq.ft)	(ac)				(cu.ft)	(ac-ft)
7036.5	5324	0.12	0	0	0	0	0.00
7037	5947	0.14	0.5	5636	2818	2818	0.06
7037.5	6591	0.15	0.5	6269	3135	5952	0.14
7038	7235	0.17	0.5	6913	3457	9409	0.22

ROCV

LID Basin -2: Elevation Volume Summary

Elev.	Area		Increase in Depth (ft)	Incremental Area (sq.ft)	Incremental Volume (cu.ft)	Cumulative Volume	
	(sq.ft)	(ac)				(cu.ft)	(ac-ft)
7020.5	1866	0.04	0	0	0	0	0.00
7021	2291	0.05	0.5	2079	1039	1039	0.02
7021.5	2738	0.06	0.5	2515	1257	2297	0.05
7022	3185	0.07	1	2962	2962	4001	0.09

ROCV

LID Basin -3: Elevation Volume Summary

Elev.	Area		Increase in Depth (ft)	Incremental Area (sq.ft)	Incremental Volume (cu.ft)	Cumulative Volume	
	(sq.ft)	(ac)				(cu.ft)	(ac-ft)
7055.5	2033	0.05	0	0	0	0	0.00
7056	2314	0.05	0.5	2174	1087	1087	0.02
7056.5	2617	0.06	0.5	2466	1233	2320	0.05
7057	2920	0.07	0.5	2769	1384	3704	0.09

ROCV

Summary of Impervious Areas

Description	Area (sf)
RV Sites	33600
Park Model	16154
Tent Sites	6132
Asphalt	63389
Site Amenities	4188
Ramada	1200
Trash Enclosures	1708
Bath House	1842
Impervious Road	1888
Total	130101

Summary of ROCV Calculations

Total ROCV (for 1")= 10842 CF

Impervious area in drainage area Sub-3A (SF)= 44300

ROCV required (Sub-3A) (CF)= 3692

ROCV provided in LID basin 3 (CF)= 3704

Thus, ROCV provided for SUB-3A (3704 CF) > ROCV required for SUB-3A (3692 CF)

Impervious area in Drainage area Sub-3B (SF)= 85801

ROCV required (Sub-3B) (CF)= 7150

ROCV provided in LID basins 1 & 2 (CF)= 8249

Thus, ROCV provided for SUB-3B (8914 CF) > ROCV required for SUB-3B (7150 CF)

APPENDIX C

- Detention Basin Stage Volume Calculations
 - Detention Basin Outlet Pipes Calculations
 - Culvert Analysis Results
- Detention Basin Emergency Spillway Weir-1
- Detention Basin Emergency Spillway Weir-2
- Detention Basin Emergency Spillway Weir Channel-1
- Detention Basin Emergency Spillway Weir Channel-2
 - LID Basin 1 Weir
 - LID Basin 2 Weir
 - LID Basin 3 Weir
- Channel Analysis Results

Woody Mountain Campground

Detention Basin Stage-Volume Summary

Elev.	Area		Increase in Depth	Incremental Area	Incremental Volume	Cumulative Volume	
	(sq.ft)	(ac)				(ft)	(sq.ft)
6992	31543	0.72	0	0	0	0	0.00
6993	34546	0.79	1	33045	33045	33045	0.76
6994	37594	0.86	1	36070	36070	69115	1.59
6995	40785	0.94	1	39190	39190	108304	2.49
6996	44131	1.01	1	42458	42458	150762	3.46
6997	47978	1.10	1	46055	46055	196817	4.52
6998	53773	1.23	1	50876	50876	247692	5.69
6998.5	55301.5	1.27	0.5	54537	27269	274961	6.31
6999	56830	1.30	1	55302	55302	302994	6.96
7000	61411	1.41	1	59121	59121	362114	8.31

Woody Mountain Campground

Detention Basin Outlet-Flow Calculations

Outlet-1

Orifice Dia.	21	in
Orifice Dia.	1.75	ft
Orifice area	2.40	sq.ft
No. of openings	1	
Elev-Inv. In	6992.00	
Elev-Inv. Out	6987.15	
Length=	54.65	
Slope=	0.0887	
Centroid	6992.875	
Orifice-top	6993.75	
Orifice Co-eff	0.6	
G (gravity)	32.2	ft/s
pipe material	cmp	
Outlet-1 Flow		
Elev.	Flow (cfs)	Flow Type
6992	0	Pipe Flow
6993	15.9	Pipe Flow
6994	12.28	Orifice
6995	16.87	Orifice
6996	20.46	Orifice
6997	23.51	Orifice
6998	26.21	Orifice
6999	28.65	Orifice
7000	30.90	Orifice

Outlet-2

Orifice Dia.	21	in
Orifice Dia.	1.75	ft
Orifice area	2.40	sq.ft
No. of openings	1	
Elev-Inv. In	6992	
Elev-Inv. Out	6989.17	
Length=	50.78	
Slope=	0.0557	
Centroid	6992.875	
Orifice-top	6993.75	
Orifice Co-eff	0.6	
G (gravity)	32.2	ft/s
Outlet-2 Flow		
Elev.	Flow (cfs)	Flow Type
6992	0	Pipe Flow
6993	12.6	Pipe Flow
6994	12.28	Orifice
6995	16.87	Orifice
6996	20.46	Orifice
6997	23.51	Orifice
6998	26.21	Orifice
6999	28.65	Orifice
7000	30.90	Orifice

Total outflow=Outlet-1+Outlet-2

Elev.	Flow (cfs)
6992	0.00
6993	28.50
6994	24.56
6995	33.75
6996	40.93
6997	47.02
6998	52.41
6999	57.30
7000	61.80

10-yr WSE	6995.42	
Combined flow rate from outlets-1&2=		37 cfs
Approximate flow rate from outlet-1=		18.5 cfs
Approximate flow rate from outlet-2=		18.5 cfs
100-yr WSE	6998.51	
Combined flow rate from outlets-1&2=		55 cfs
Approximate flow rate from outlet-1=		27.5 cfs
Approximate flow rate from outlet-2=		27.5 cfs

Culvert Report

BASIN CULVERT 1 (BC1)-Q25

Invert Elev Dn (ft)	= 6998.50
Pipe Length (ft)	= 31.03
Slope (%)	= 3.19
Invert Elev Up (ft)	= 6999.49
Rise (in)	= 24.0
Shape	= Circular
Span (in)	= 24.0
No. Barrels	= 1
n-Value	= 0.024
Culvert Type	= Circular Corrugate Metal Pipe
Culvert Entrance	= Projecting
Coeff. K,M,c,Y,k	= 0.034, 1.5, 0.0553, 0.54, 0.9

Calculations

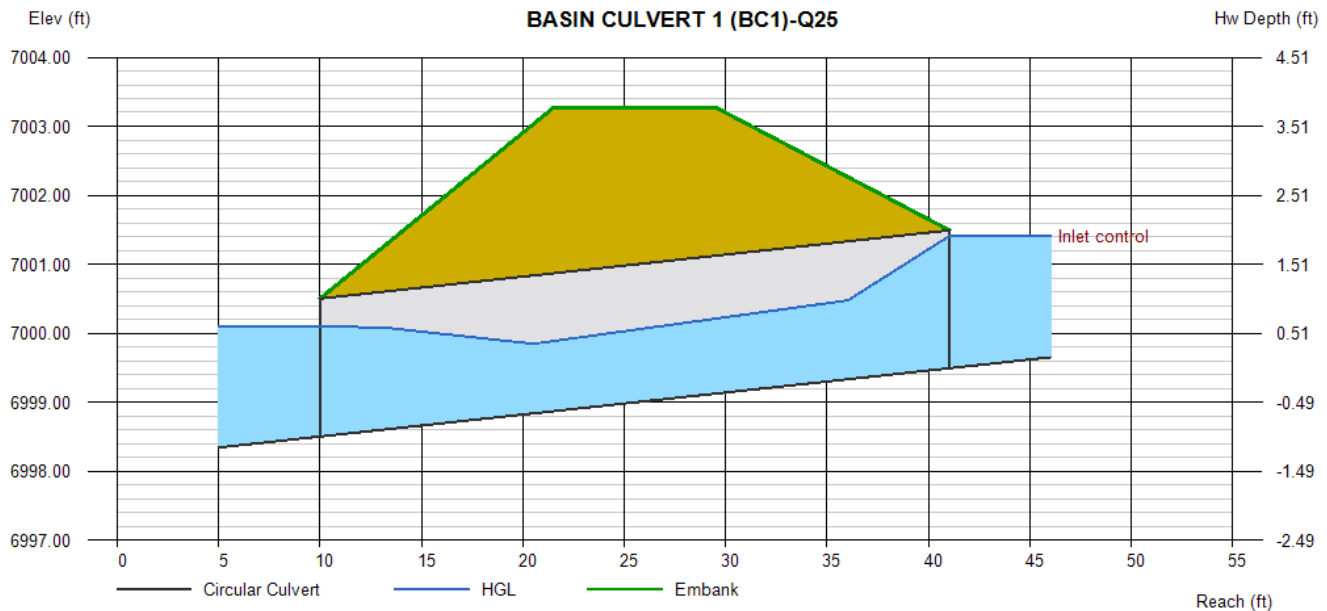
Qmin (cfs)	= 11.00
Qmax (cfs)	= 15.00
Tailwater Elev (ft)	= (dc+D)/2

Highlighted

Qtotal (cfs)	= 11.00
Qpipe (cfs)	= 11.00
Qovertop (cfs)	= 0.00
Veloc Dn (ft/s)	= 4.10
Veloc Up (ft/s)	= 5.66
HGL Dn (ft)	= 7000.09
HGL Up (ft)	= 7000.68
Hw Elev (ft)	= 7001.41
Hw/D (ft)	= 0.96
Flow Regime	= Inlet Control

Embankment

Top Elevation (ft)	= 7003.27
Top Width (ft)	= 8.00
Crest Width (ft)	= 100.00



Culvert Report

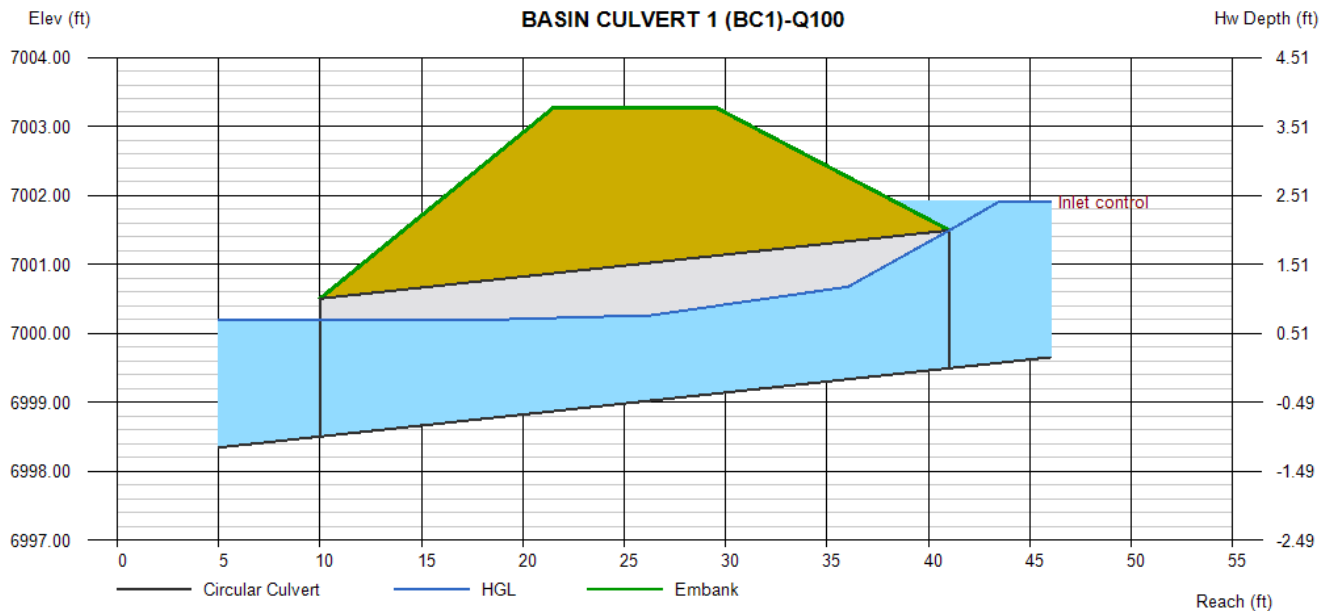
BASIN CULVERT 1 (BC1)-Q100

Invert Elev Dn (ft)	=	6998.50
Pipe Length (ft)	=	31.03
Slope (%)	=	3.19
Invert Elev Up (ft)	=	6999.49
Rise (in)	=	24.0
Shape	=	Circular
Span (in)	=	24.0
No. Barrels	=	1
n-Value	=	0.024
Culvert Type	=	Circular Corrugate Metal Pipe
Culvert Entrance	=	Projecting
Coeff. K,M,c,Y,k	=	0.034, 1.5, 0.0553, 0.54, 0.9

Calculations	
Qmin (cfs)	= 5.00
Qmax (cfs)	= 15.00
Tailwater Elev (ft)	= (dc+D)/2

Embankment	
Top Elevation (ft)	= 7003.27
Top Width (ft)	= 8.00
Crest Width (ft)	= 100.00

Highlighted	
Qtotal (cfs)	= 15.00
Qpipe (cfs)	= 15.00
Qovertop (cfs)	= 0.00
Veloc Dn (ft/s)	= 5.28
Veloc Up (ft/s)	= 6.41
HGL Dn (ft)	= 7000.20
HGL Up (ft)	= 7000.89
Hw Elev (ft)	= 7001.91
Hw/D (ft)	= 1.21
Flow Regime	= Inlet Control



Culvert Report

BASIN CULVERT 2 (BC2)-Q25

Invert Elev Dn (ft)	= 6999.38
Pipe Length (ft)	= 35.46
Slope (%)	= 4.20
Invert Elev Up (ft)	= 7000.87
Rise (in)	= 36.0
Shape	= Circular
Span (in)	= 36.0
No. Barrels	= 2
n-Value	= 0.024
Culvert Type	= Circular Corrugate Metal Pipe
Culvert Entrance	= Projecting
Coeff. K,M,c,Y,k	= 0.034, 1.5, 0.0553, 0.54, 0.9

Embankment

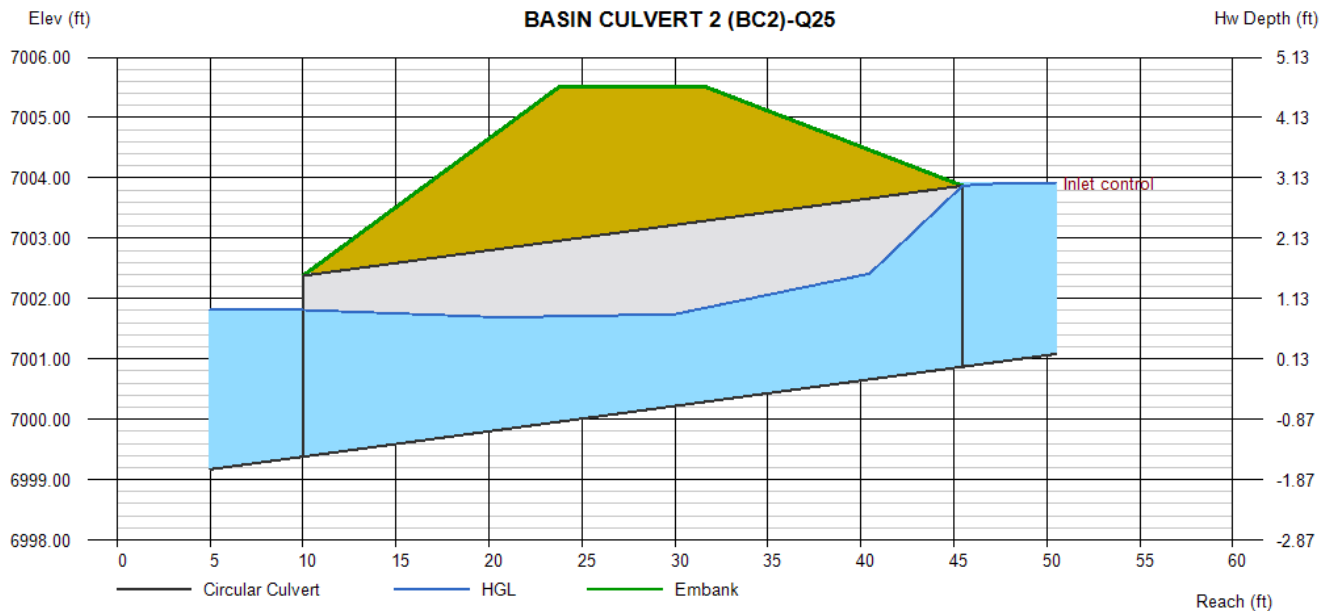
Top Elevation (ft)	= 7005.50
Top Width (ft)	= 8.00
Crest Width (ft)	= 100.00

Calculations

Qmin (cfs)	= 66.00
Qmax (cfs)	= 100.00
Tailwater Elev (ft)	= (dc+D)/2

Highlighted

Qtotal (cfs)	= 66.00
Qpipe (cfs)	= 66.00
Qovertop (cfs)	= 0.00
Veloc Dn (ft/s)	= 5.38
Veloc Up (ft/s)	= 7.15
HGL Dn (ft)	= 7001.81
HGL Up (ft)	= 7002.73
Hw Elev (ft)	= 7003.92
Hw/D (ft)	= 1.02
Flow Regime	= Inlet Control



Culvert Report

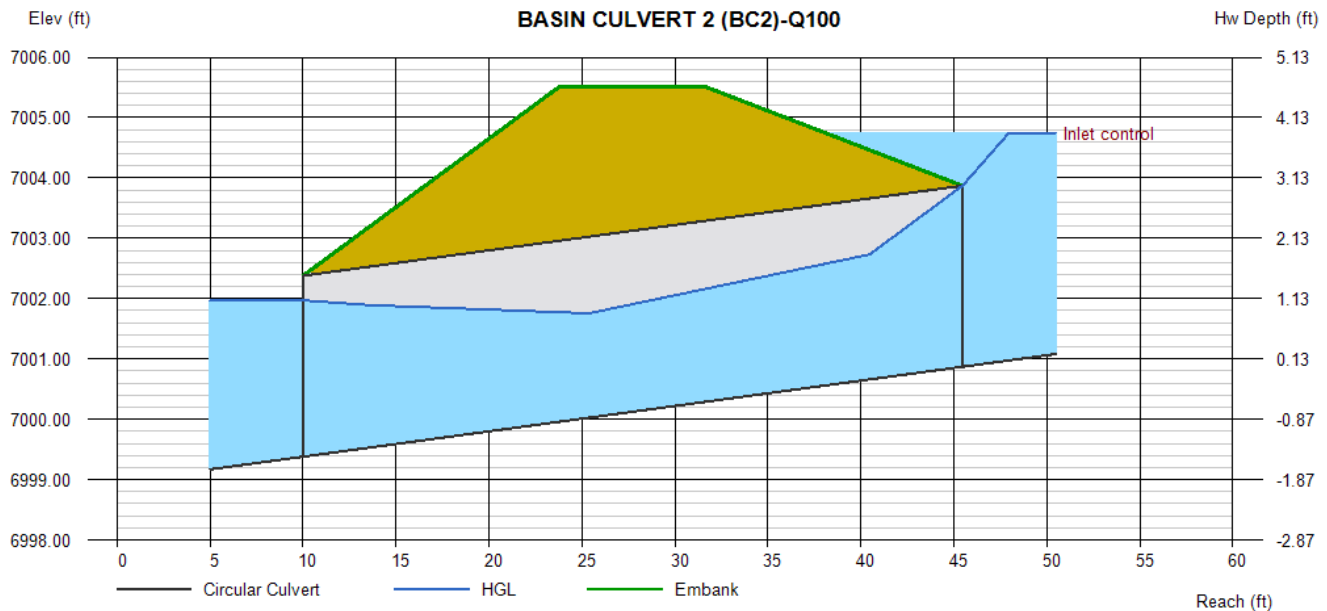
BASIN CULVERT 2 (BC2)-Q100

Invert Elev Dn (ft)	= 6999.38
Pipe Length (ft)	= 35.46
Slope (%)	= 4.20
Invert Elev Up (ft)	= 7000.87
Rise (in)	= 36.0
Shape	= Circular
Span (in)	= 36.0
No. Barrels	= 2
n-Value	= 0.024
Culvert Type	= Circular Corrugate Metal Pipe
Culvert Entrance	= Projecting
Coeff. K,M,c,Y,k	= 0.034, 1.5, 0.0553, 0.54, 0.9

Calculations	
Qmin (cfs)	= 50.00
Qmax (cfs)	= 100.00
Tailwater Elev (ft)	= (dc+D)/2

Highlighted	
Qtotal (cfs)	= 90.00
Qpipe (cfs)	= 90.00
Qovertop (cfs)	= 0.00
Veloc Dn (ft/s)	= 6.93
Veloc Up (ft/s)	= 8.16
HGL Dn (ft)	= 7001.97
HGL Up (ft)	= 7003.05
Hw Elev (ft)	= 7004.75
Hw/D (ft)	= 1.29
Flow Regime	= Inlet Control

Embankment	
Top Elevation (ft)	= 7005.50
Top Width (ft)	= 8.00
Crest Width (ft)	= 100.00



Culvert Report

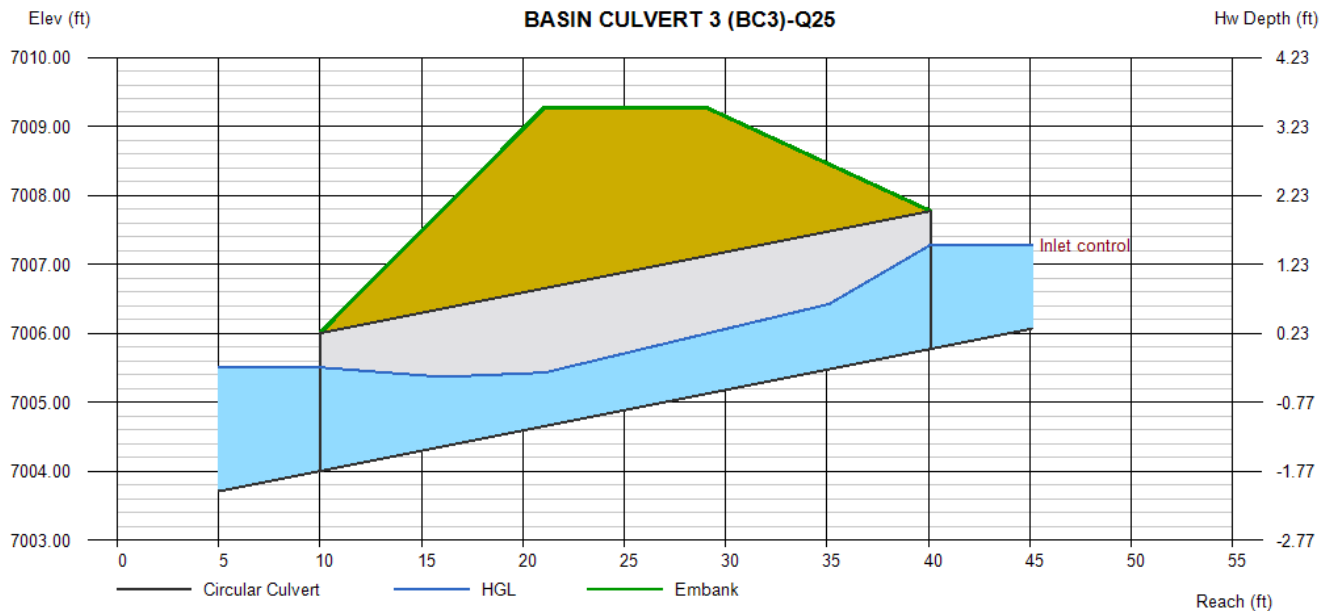
BASIN CULVERT 3 (BC3)-Q25

Invert Elev Dn (ft)	= 7004.00
Pipe Length (ft)	= 30.10
Slope (%)	= 5.88
Invert Elev Up (ft)	= 7005.77
Rise (in)	= 24.0
Shape	= Circular
Span (in)	= 24.0
No. Barrels	= 1
n-Value	= 0.024
Culvert Type	= Circular Corrugate Metal Pipe
Culvert Entrance	= Projecting
Coeff. K,M,c,Y,k	= 0.034, 1.5, 0.0553, 0.54, 0.9

Calculations	
Qmin (cfs)	= 8.00
Qmax (cfs)	= 12.00
Tailwater Elev (ft)	= (dc+D)/2

Highlighted	
Qtotal (cfs)	= 8.00
Qpipe (cfs)	= 8.00
Qovertop (cfs)	= 0.00
Veloc Dn (ft/s)	= 3.16
Veloc Up (ft/s)	= 5.06
HGL Dn (ft)	= 7005.50
HGL Up (ft)	= 7006.78
Hw Elev (ft)	= 7007.28
Hw/D (ft)	= 0.75
Flow Regime	= Inlet Control

Embankment	
Top Elevation (ft)	= 7009.27
Top Width (ft)	= 8.00
Crest Width (ft)	= 100.00



Culvert Report

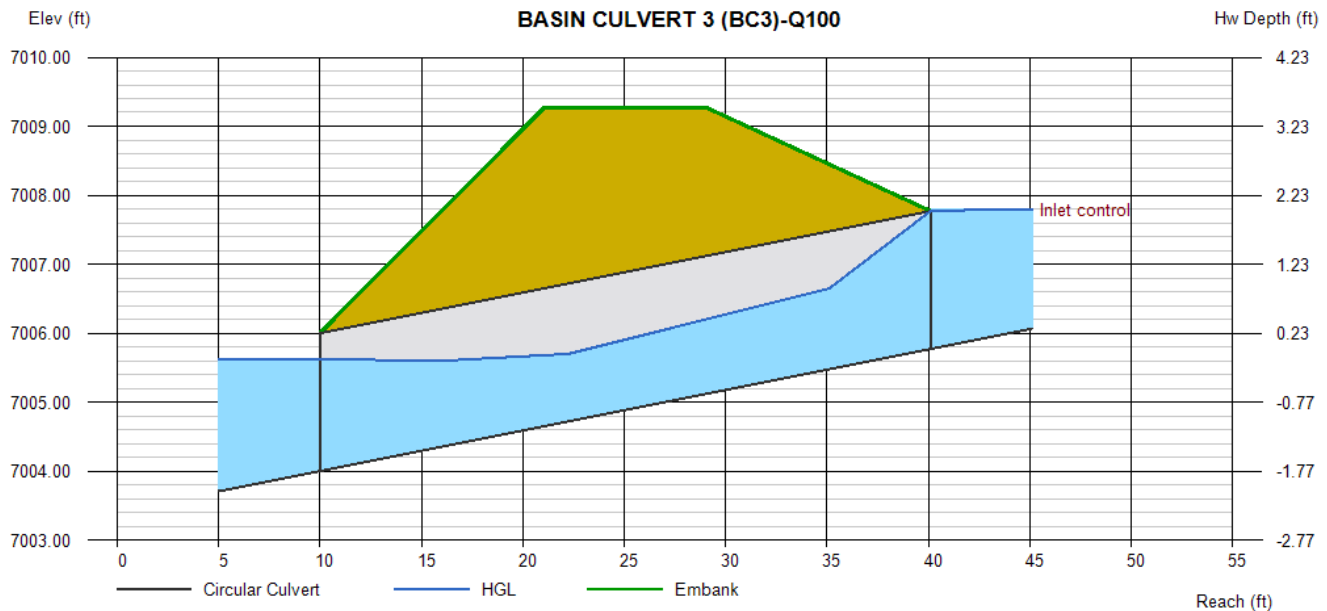
BASIN CULVERT 3 (BC3)-Q100

Invert Elev Dn (ft)	= 7004.00
Pipe Length (ft)	= 30.10
Slope (%)	= 5.88
Invert Elev Up (ft)	= 7005.77
Rise (in)	= 24.0
Shape	= Circular
Span (in)	= 24.0
No. Barrels	= 1
n-Value	= 0.024
Culvert Type	= Circular Corrugate Metal Pipe
Culvert Entrance	= Projecting
Coeff. K,M,c,Y,k	= 0.034, 1.5, 0.0553, 0.54, 0.9

Calculations	
Qmin (cfs)	= 8.00
Qmax (cfs)	= 12.00
Tailwater Elev (ft)	= (dc+D)/2

Highlighted	
Qtotal (cfs)	= 12.00
Qpipe (cfs)	= 12.00
Qovertop (cfs)	= 0.00
Veloc Dn (ft/s)	= 4.40
Veloc Up (ft/s)	= 5.85
HGL Dn (ft)	= 7005.62
HGL Up (ft)	= 7007.01
Hw Elev (ft)	= 7007.79
Hw/D (ft)	= 1.01
Flow Regime	= Inlet Control

Embankment	
Top Elevation (ft)	= 7009.27
Top Width (ft)	= 8.00
Crest Width (ft)	= 100.00



Culvert Report

BASIN CULVERT 4 (BC4)-Q25

Invert Elev Dn (ft) = 6999.00
 Pipe Length (ft) = 50.00
 Slope (%) = 1.00
 Invert Elev Up (ft) = 6999.50
 Rise (in) = 36.0
 Shape = Box
 Span (in) = 96.0
 No. Barrels = 1
 n-Value = 0.024
 Culvert Type = 90D Headwall,
 Chamfered or Beveled Inlet Edges

Culvert Entrance = 90D headwall w/3/4-in chamfers
 Coeff. K,M,c,Y,k = 0.515, 0.667, 0.0375, 0.79, 0.2

Embankment

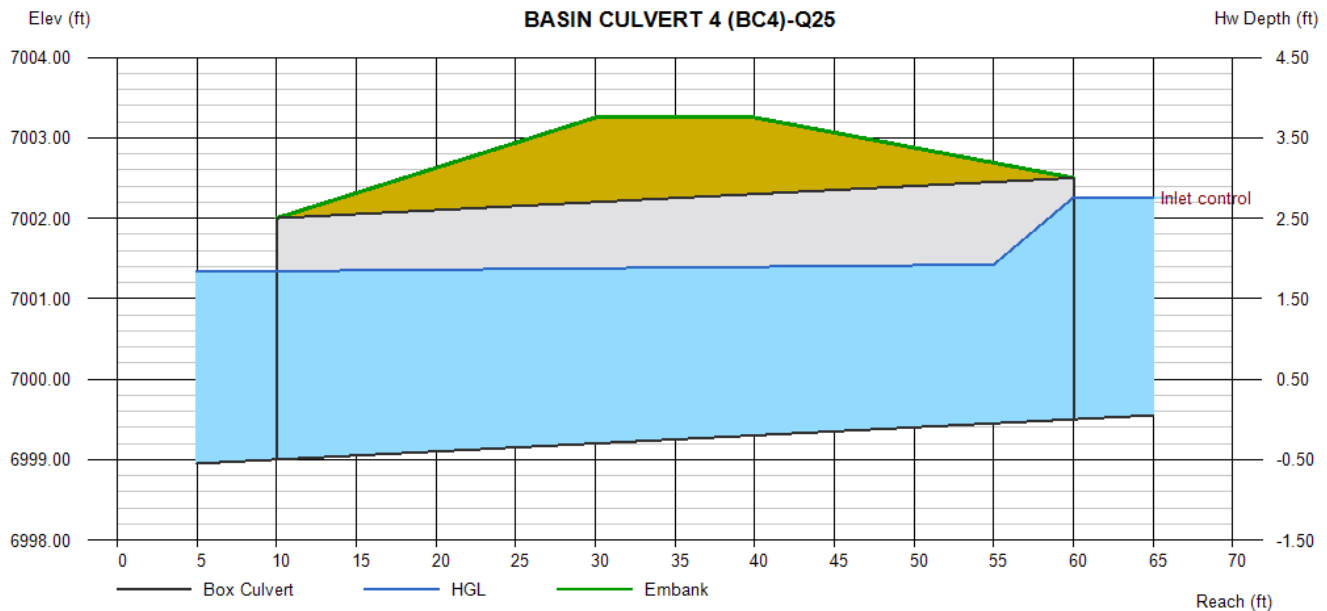
Top Elevation (ft) = 7003.25
 Top Width (ft) = 10.00
 Crest Width (ft) = 100.00

Calculations

Qmin (cfs) = 99.00
 Qmax (cfs) = 137.00
 Tailwater Elev (ft) = (dc+D)/2

Highlighted

Qtotal (cfs) = 99.00
 Qpipe (cfs) = 99.00
 Qovertop (cfs) = 0.00
 Veloc Dn (ft/s) = 5.29
 Veloc Up (ft/s) = 6.41
 HGL Dn (ft) = 7001.34
 HGL Up (ft) = 7001.43
 Hw Elev (ft) = 7002.26
 Hw/D (ft) = 0.92
 Flow Regime = Inlet Control



Culvert Report

BASIN CULVERT 4 (BC4)-Q100

Invert Elev Dn (ft) = 6999.00
 Pipe Length (ft) = 50.00
 Slope (%) = 1.00
 Invert Elev Up (ft) = 6999.50
 Rise (in) = 36.0
 Shape = Box
 Span (in) = 96.0
 No. Barrels = 1
 n-Value = 0.024
 Culvert Type = 90D Headwall,
 Chamfered or Beveled Inlet Edges

Culvert Entrance = 90D headwall w/3/4-in chamfers
 Coeff. K,M,c,Y,k = 0.515, 0.667, 0.0375, 0.79, 0.2

Embankment

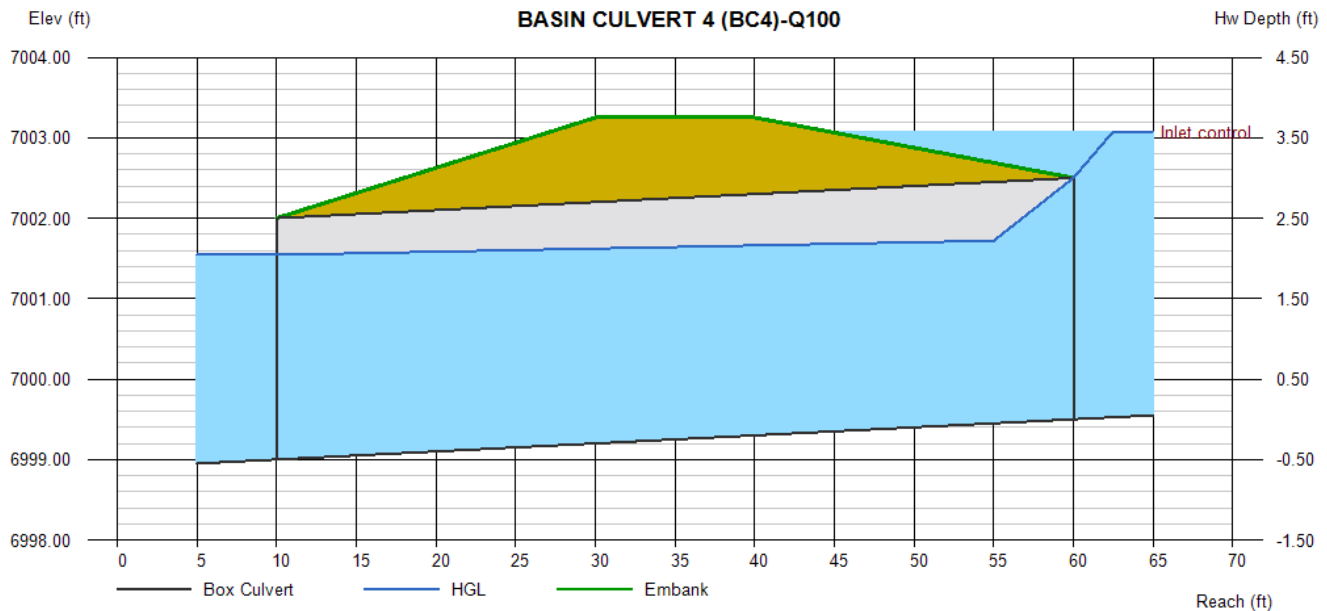
Top Elevation (ft) = 7003.25
 Top Width (ft) = 10.00
 Crest Width (ft) = 100.00

Calculations

Qmin (cfs) = 99.00
 Qmax (cfs) = 137.00
 Tailwater Elev (ft) = (dc+D)/2

Highlighted

Qtotal (cfs) = 137.00
 Qpipe (cfs) = 137.00
 Qovertop (cfs) = 0.00
 Veloc Dn (ft/s) = 6.73
 Veloc Up (ft/s) = 7.65
 HGL Dn (ft) = 7001.54
 HGL Up (ft) = 7001.74
 Hw Elev (ft) = 7003.08
 Hw/D (ft) = 1.19
 Flow Regime = Inlet Control



Culvert Report

Culvert 1 (Q25)

Invert Elev Dn (ft)	= 7016.25
Pipe Length (ft)	= 36.83
Slope (%)	= 10.16
Invert Elev Up (ft)	= 7019.99
Rise (in)	= 30.0
Shape	= Circular
Span (in)	= 30.0
No. Barrels	= 2
n-Value	= 0.024
Culvert Type	= Circular Corrugate Metal Pipe
Culvert Entrance	= Projecting
Coeff. K,M,c,Y,k	= 0.034, 1.5, 0.0553, 0.54, 0.9

Embankment

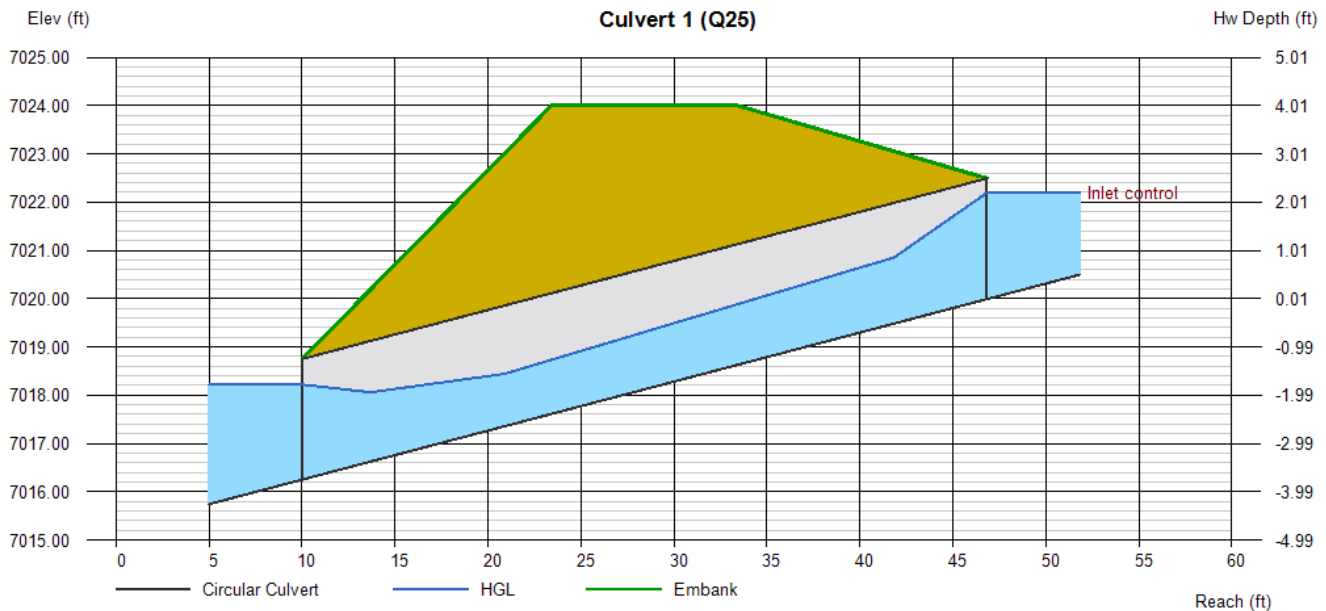
Top Elevation (ft)	= 7024.00
Top Width (ft)	= 10.00
Crest Width (ft)	= 200.00

Calculations

Qmin (cfs)	= 36.00
Qmax (cfs)	= 48.00
Tailwater Elev (ft)	= (dc+D)/2

Highlighted

Qtotal (cfs)	= 36.00
Qpipe (cfs)	= 36.00
Qovertop (cfs)	= 0.00
Veloc Dn (ft/s)	= 4.34
Veloc Up (ft/s)	= 6.17
HGL Dn (ft)	= 7018.22
HGL Up (ft)	= 7021.43
Hw Elev (ft)	= 7022.19
Hw/D (ft)	= 0.88
Flow Regime	= Inlet Control



Culvert Report

Culvert 1 (Q100)

Invert Elev Dn (ft)	= 7016.25
Pipe Length (ft)	= 36.83
Slope (%)	= 10.16
Invert Elev Up (ft)	= 7019.99
Rise (in)	= 30.0
Shape	= Circular
Span (in)	= 30.0
No. Barrels	= 2
n-Value	= 0.024
Culvert Type	= Circular Corrugate Metal Pipe
Culvert Entrance	= Projecting
Coeff. K,M,c,Y,k	= 0.034, 1.5, 0.0553, 0.54, 0.9

Embankment

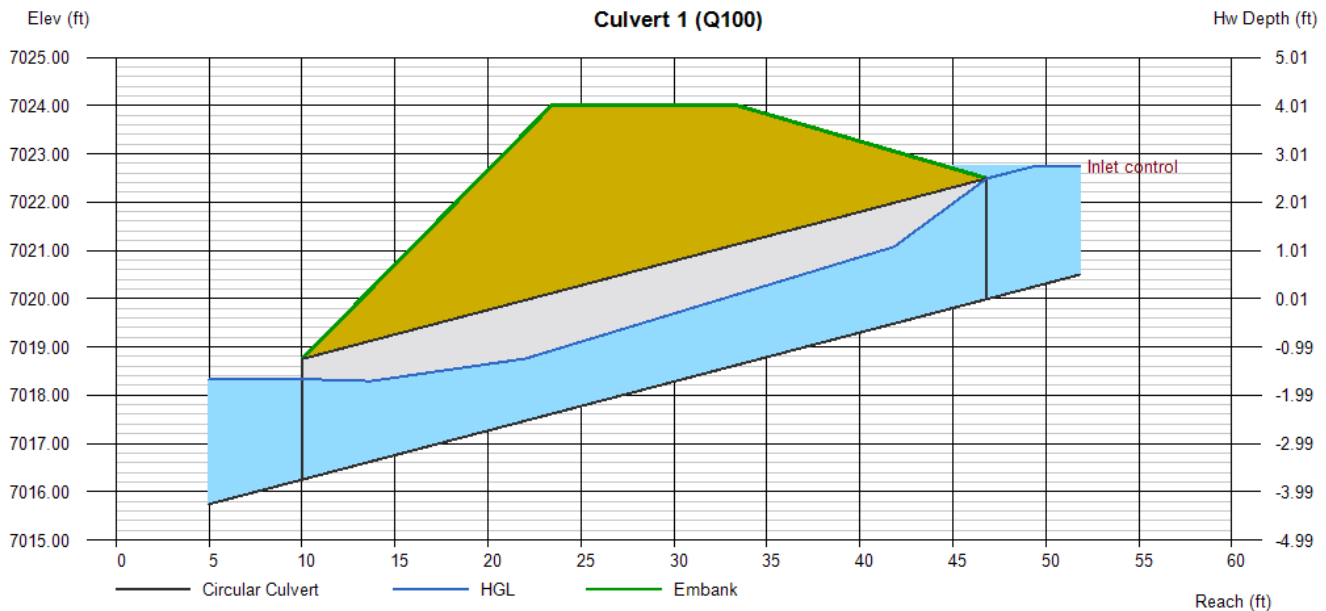
Top Elevation (ft)	= 7024.00
Top Width (ft)	= 10.00
Crest Width (ft)	= 100.00

Calculations

Qmin (cfs)	= 28.00
Qmax (cfs)	= 48.00
Tailwater Elev (ft)	= (dc+D)/2

Highlighted

Qtotal (cfs)	= 48.00
Qpipe (cfs)	= 48.00
Qovertop (cfs)	= 0.00
Veloc Dn (ft/s)	= 5.49
Veloc Up (ft/s)	= 6.90
HGL Dn (ft)	= 7018.33
HGL Up (ft)	= 7021.66
Hw Elev (ft)	= 7022.73
Hw/D (ft)	= 1.10
Flow Regime	= Inlet Control



Culvert Report

Culvert 2 (Q25)

Invert Elev Dn (ft)	= 7014.73
Pipe Length (ft)	= 30.96
Slope (%)	= 4.78
Invert Elev Up (ft)	= 7016.21
Rise (in)	= 24.0
Shape	= Circular
Span (in)	= 24.0
No. Barrels	= 1
n-Value	= 0.024
Culvert Type	= Circular Corrugate Metal Pipe
Culvert Entrance	= Projecting
Coeff. K,M,c,Y,k	= 0.034, 1.5, 0.0553, 0.54, 0.9

Embankment

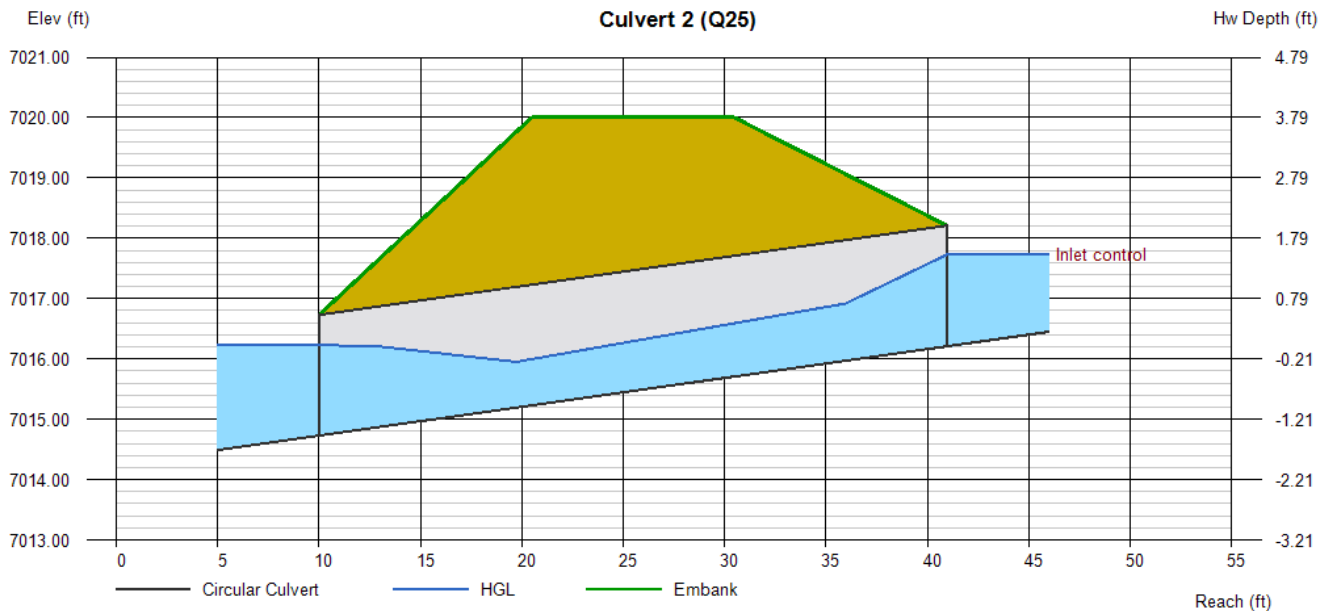
Top Elevation (ft)	= 7020.00
Top Width (ft)	= 10.00
Crest Width (ft)	= 100.00

Calculations

Qmin (cfs)	= 5.00
Qmax (cfs)	= 12.00
Tailwater Elev (ft)	= (dc+D)/2

Highlighted

Qtotal (cfs)	= 8.00
Qpipe (cfs)	= 8.00
Qovertop (cfs)	= 0.00
Veloc Dn (ft/s)	= 3.16
Veloc Up (ft/s)	= 5.06
HGL Dn (ft)	= 7016.23
HGL Up (ft)	= 7017.22
Hw Elev (ft)	= 7017.73
Hw/D (ft)	= 0.76
Flow Regime	= Inlet Control



Culvert Report

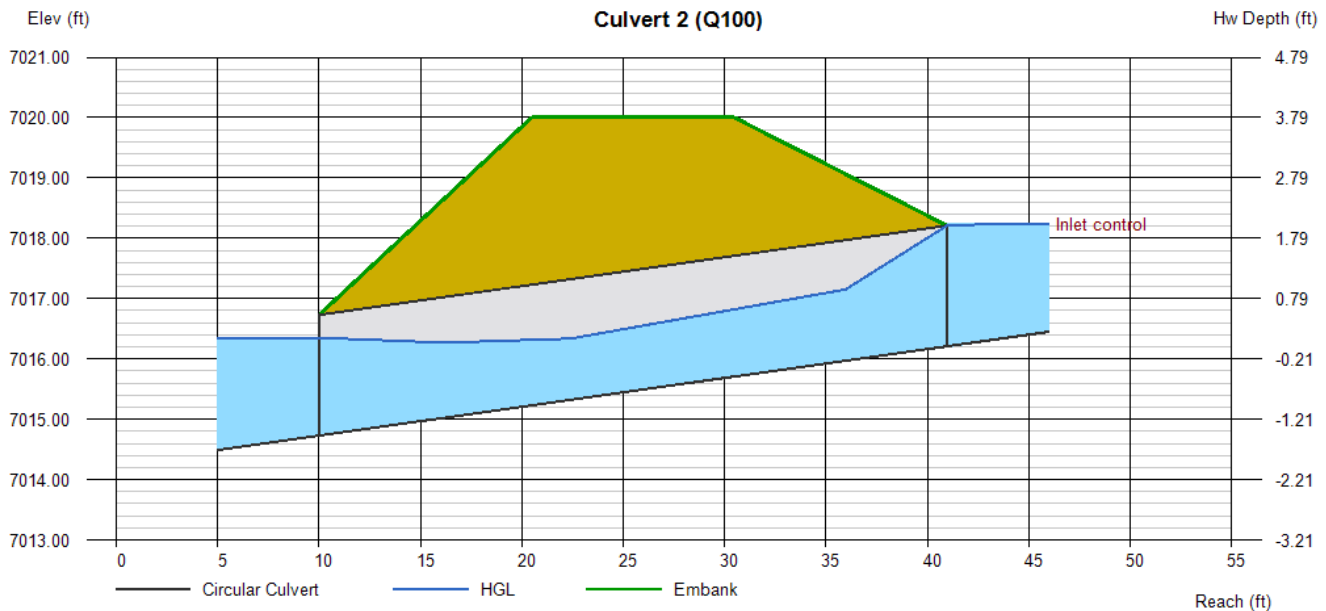
Culvert 2 (Q100)

Invert Elev Dn (ft)	= 7014.73
Pipe Length (ft)	= 30.96
Slope (%)	= 4.78
Invert Elev Up (ft)	= 7016.21
Rise (in)	= 24.0
Shape	= Circular
Span (in)	= 24.0
No. Barrels	= 1
n-Value	= 0.024
Culvert Type	= Circular Corrugate Metal Pipe
Culvert Entrance	= Projecting
Coeff. K,M,c,Y,k	= 0.034, 1.5, 0.0553, 0.54, 0.9

Calculations	
Qmin (cfs)	= 6.00
Qmax (cfs)	= 12.00
Tailwater Elev (ft)	= (dc+D)/2

Highlighted	
Qtotal (cfs)	= 12.00
Qpipe (cfs)	= 12.00
Qovertop (cfs)	= 0.00
Veloc Dn (ft/s)	= 4.40
Veloc Up (ft/s)	= 5.85
HGL Dn (ft)	= 7016.35
HGL Up (ft)	= 7017.45
Hw Elev (ft)	= 7018.24
Hw/D (ft)	= 1.01
Flow Regime	= Inlet Control

Embankment	
Top Elevation (ft)	= 7020.00
Top Width (ft)	= 10.00
Crest Width (ft)	= 100.00



Culvert Report

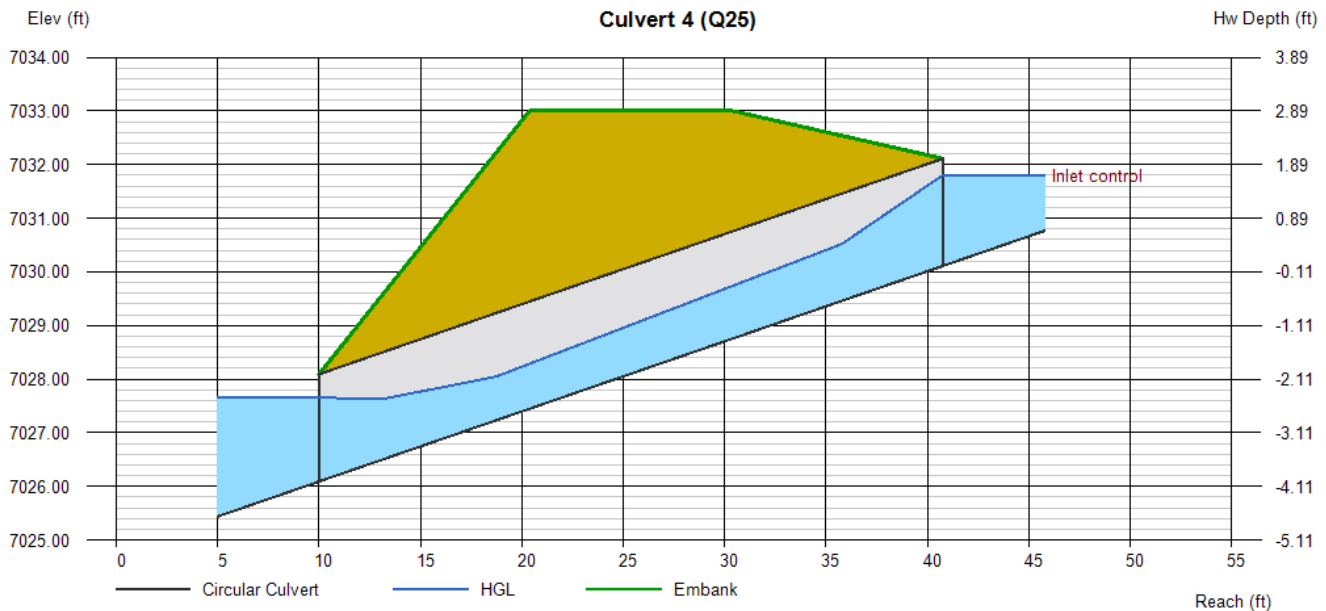
Culvert 4 (Q25)

Invert Elev Dn (ft)	=	7026.09
Pipe Length (ft)	=	30.76
Slope (%)	=	13.07
Invert Elev Up (ft)	=	7030.11
Rise (in)	=	24.0
Shape	=	Circular
Span (in)	=	24.0
No. Barrels	=	2
n-Value	=	0.024
Culvert Type	=	Circular Corrugate Metal Pipe
Culvert Entrance	=	Projecting
Coeff. K,M,c,Y,k	=	0.034, 1.5, 0.0553, 0.54, 0.9

Calculations	
Qmin (cfs)	= 20.00
Qmax (cfs)	= 28.00
Tailwater Elev (ft)	= (dc+D)/2

Highlighted	
Qtotal (cfs)	= 20.00
Qpipe (cfs)	= 20.00
Qovertop (cfs)	= 0.00
Veloc Dn (ft/s)	= 3.79
Veloc Up (ft/s)	= 5.46
HGL Dn (ft)	= 7027.66
HGL Up (ft)	= 7031.24
Hw Elev (ft)	= 7031.80
Hw/D (ft)	= 0.85
Flow Regime	= Inlet Control

Embankment	
Top Elevation (ft)	= 7033.00
Top Width (ft)	= 10.00
Crest Width (ft)	= 100.00



Culvert Report

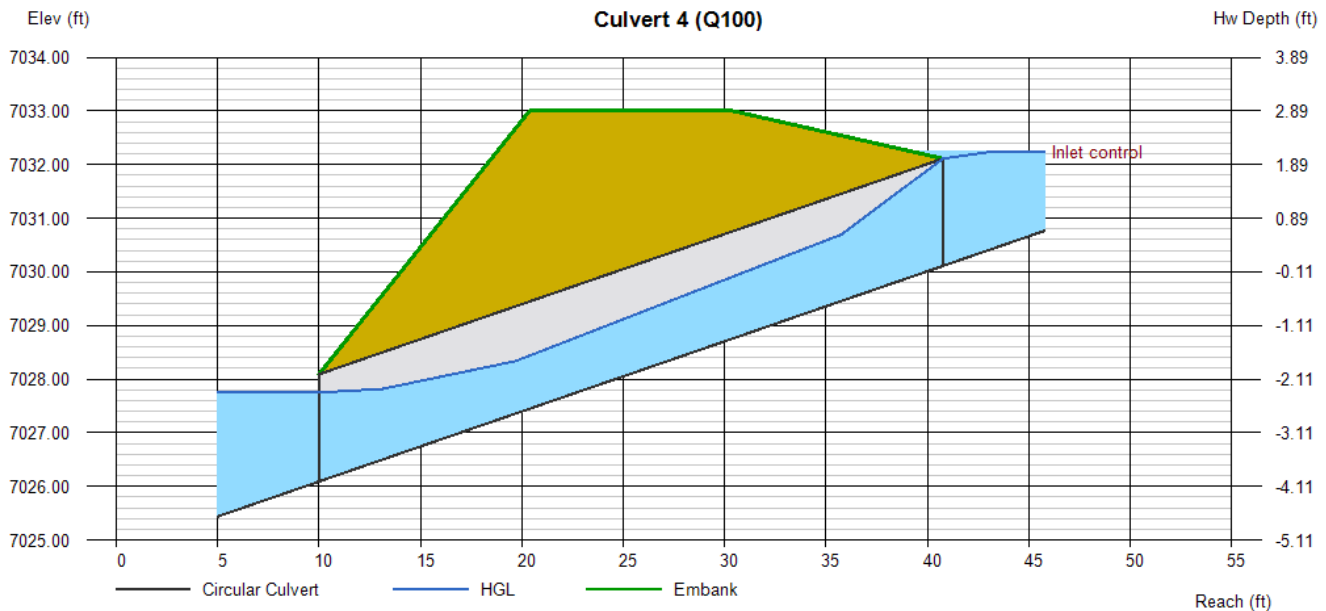
Culvert 4 (Q100)

Invert Elev Dn (ft)	= 7026.09
Pipe Length (ft)	= 30.76
Slope (%)	= 13.07
Invert Elev Up (ft)	= 7030.11
Rise (in)	= 24.0
Shape	= Circular
Span (in)	= 24.0
No. Barrels	= 2
n-Value	= 0.024
Culvert Type	= Circular Corrugate Metal Pipe
Culvert Entrance	= Projecting
Coeff. K,M,c,Y,k	= 0.034, 1.5, 0.0553, 0.54, 0.9

Calculations	
Qmin (cfs)	= 20.00
Qmax (cfs)	= 28.00
Tailwater Elev (ft)	= (dc+D)/2

Highlighted	
Qtotal (cfs)	= 27.00
Qpipe (cfs)	= 27.00
Qovertop (cfs)	= 0.00
Veloc Dn (ft/s)	= 4.84
Veloc Up (ft/s)	= 6.13
HGL Dn (ft)	= 7027.75
HGL Up (ft)	= 7031.43
Hw Elev (ft)	= 7032.25
Hw/D (ft)	= 1.07
Flow Regime	= Inlet Control

Embankment	
Top Elevation (ft)	= 7033.00
Top Width (ft)	= 10.00
Crest Width (ft)	= 100.00



Culvert Report

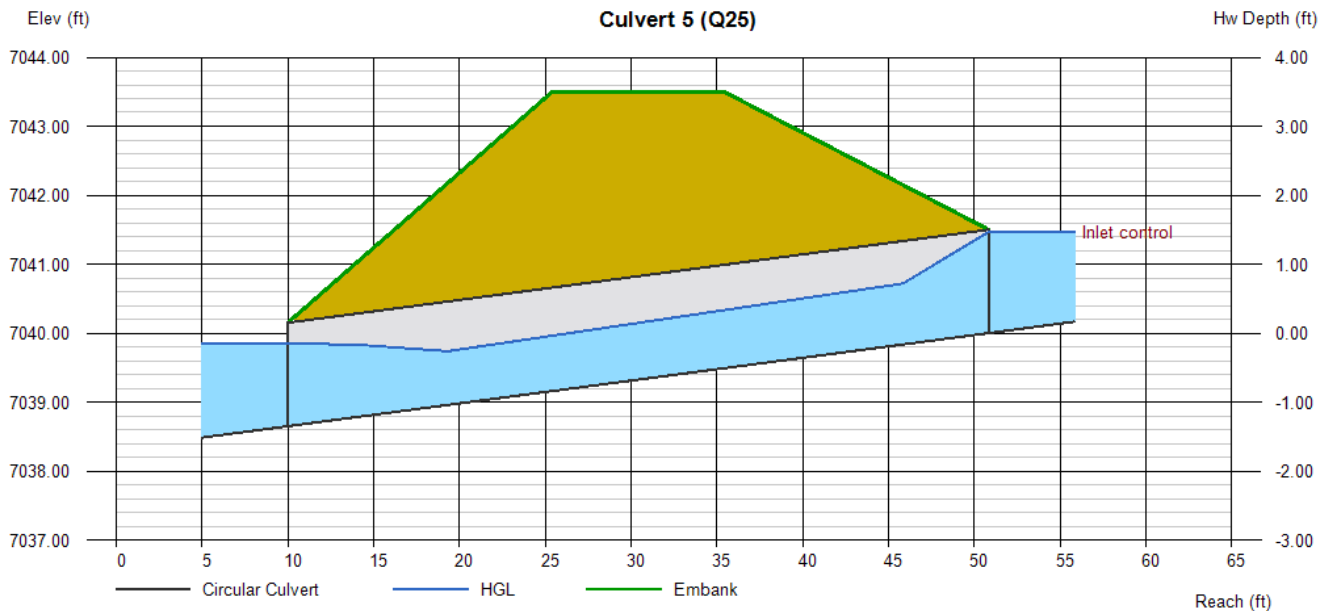
Culvert 5 (Q25)

Invert Elev Dn (ft) = 7038.65
 Pipe Length (ft) = 40.83
 Slope (%) = 3.31
 Invert Elev Up (ft) = 7040.00
 Rise (in) = 18.0
 Shape = Circular
 Span (in) = 18.0
 No. Barrels = 2
 n-Value = 0.024
 Culvert Type = Circular Corrugate Metal Pipe
 Culvert Entrance = Projecting
 Coeff. K,M,c,Y,k = 0.034, 1.5, 0.0553, 0.54, 0.9

Calculations
 Qmin (cfs) = 11.00
 Qmax (cfs) = 15.00
 Tailwater Elev (ft) = (dc+D)/2

Highlighted
 Qtotal (cfs) = 11.00
 Qpipe (cfs) = 11.00
 Qovertop (cfs) = 0.00
 Veloc Dn (ft/s) = 3.62
 Veloc Up (ft/s) = 4.94
 HGL Dn (ft) = 7039.85
 HGL Up (ft) = 7040.90
 Hw Elev (ft) = 7041.47
 Hw/D (ft) = 0.98
 Flow Regime = Inlet Control

Embankment
 Top Elevation (ft) = 7043.50
 Top Width (ft) = 10.00
 Crest Width (ft) = 100.00



Culvert Report

Culvert 5 (Q100)

Invert Elev Dn (ft)	= 7038.65
Pipe Length (ft)	= 40.83
Slope (%)	= 3.31
Invert Elev Up (ft)	= 7040.00
Rise (in)	= 18.0
Shape	= Circular
Span (in)	= 18.0
No. Barrels	= 2
n-Value	= 0.024
Culvert Type	= Circular Corrugate Metal Pipe
Culvert Entrance	= Projecting
Coeff. K,M,c,Y,k	= 0.034, 1.5, 0.0553, 0.54, 0.9

Embankment

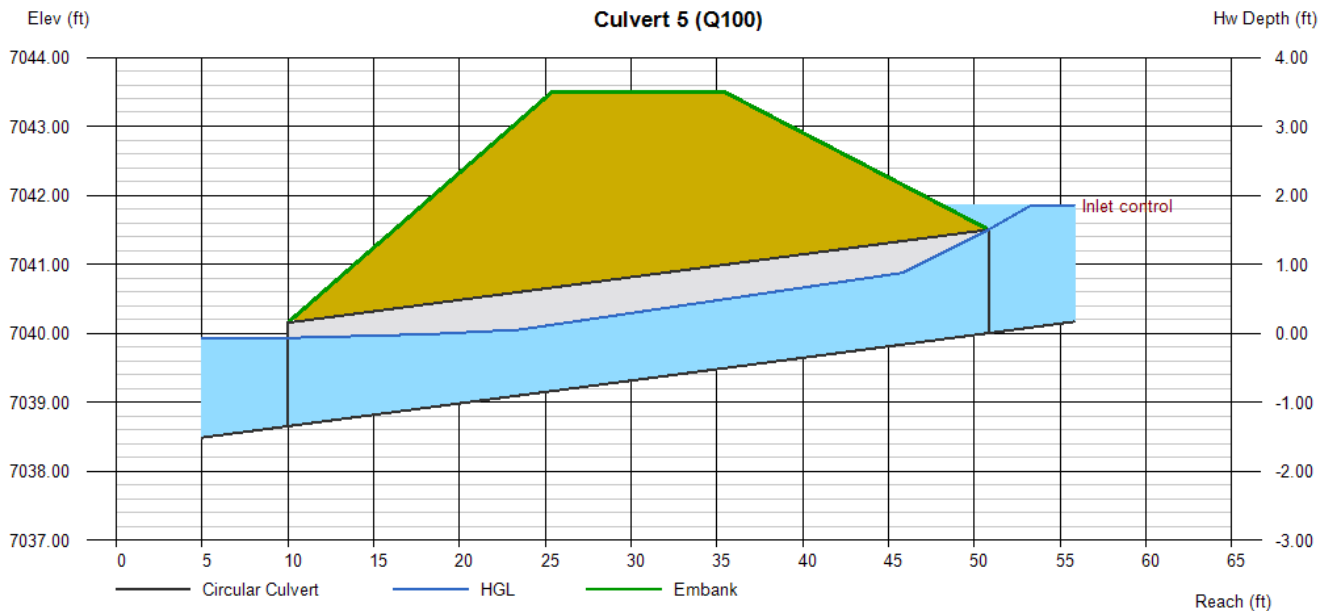
Top Elevation (ft)	= 7043.50
Top Width (ft)	= 10.00
Crest Width (ft)	= 100.00

Calculations

Qmin (cfs)	= 11.00
Qmax (cfs)	= 15.00
Tailwater Elev (ft)	= (dc+D)/2

Highlighted

Qtotal (cfs)	= 15.00
Qpipe (cfs)	= 15.00
Qovertop (cfs)	= 0.00
Veloc Dn (ft/s)	= 4.67
Veloc Up (ft/s)	= 5.62
HGL Dn (ft)	= 7039.93
HGL Up (ft)	= 7041.06
Hw Elev (ft)	= 7041.86
Hw/D (ft)	= 1.24
Flow Regime	= Inlet Control



Culvert Report

Culvert 6 (Q25)

Invert Elev Dn (ft)	=	7020.50
Pipe Length (ft)	=	83.06
Slope (%)	=	16.39
Invert Elev Up (ft)	=	7034.11
Rise (in)	=	18.0
Shape	=	Circular
Span (in)	=	18.0
No. Barrels	=	2
n-Value	=	0.024
Culvert Type	=	Circular Corrugate Metal Pipe
Culvert Entrance	=	Projecting
Coeff. K,M,c,Y,k	=	0.034, 1.5, 0.0553, 0.54, 0.9

Embankment

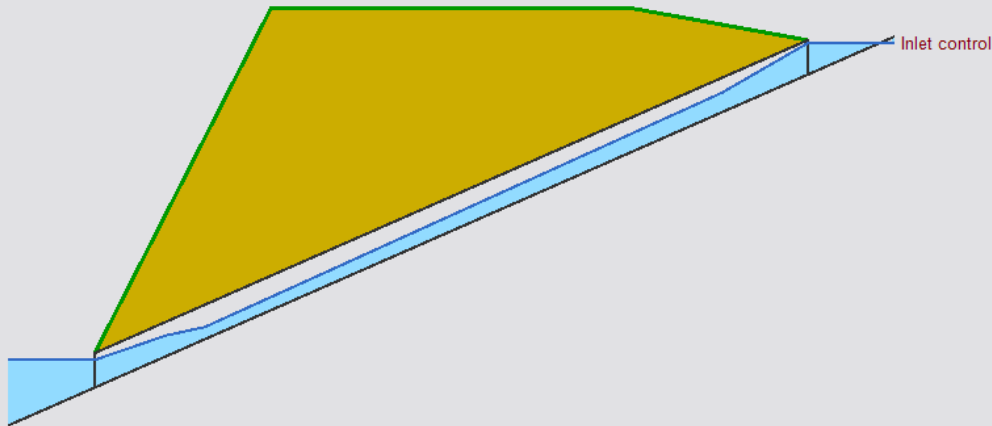
Top Elevation (ft)	=	7037.00
Top Width (ft)	=	42.00
Crest Width (ft)	=	100.00

Calculations

Qmin (cfs)	=	11.00
Qmax (cfs)	=	15.00
Tailwater Elev (ft)	=	(dc+D)/2

Highlighted

Qtotal (cfs)	=	11.00
Qpipe (cfs)	=	11.00
Qovertop (cfs)	=	0.00
Veloc Dn (ft/s)	=	3.62
Veloc Up (ft/s)	=	4.94
HGL Dn (ft)	=	7021.70
HGL Up (ft)	=	7035.01
Hw Elev (ft)	=	7035.48
Hw/D (ft)	=	0.91
Flow Regime	=	Inlet Control



Culvert Report

Culvert 6 (Q100)

Invert Elev Dn (ft)	= 7020.50
Pipe Length (ft)	= 83.06
Slope (%)	= 16.39
Invert Elev Up (ft)	= 7034.11
Rise (in)	= 18.0
Shape	= Circular
Span (in)	= 18.0
No. Barrels	= 2
n-Value	= 0.024
Culvert Type	= Circular Corrugate Metal Pipe
Culvert Entrance	= Projecting
Coeff. K,M,c,Y,k	= 0.034, 1.5, 0.0553, 0.54, 0.9

Embankment

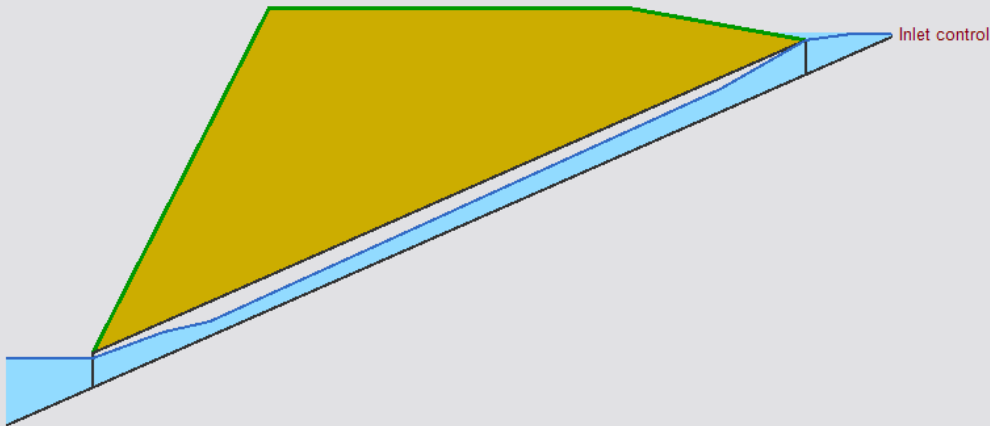
Top Elevation (ft)	= 7037.00
Top Width (ft)	= 42.00
Crest Width (ft)	= 100.00

Calculations

Qmin (cfs)	= 7.00
Qmax (cfs)	= 15.00
Tailwater Elev (ft)	= (dc+D)/2

Highlighted

Qtotal (cfs)	= 15.00
Qpipe (cfs)	= 15.00
Qovertop (cfs)	= 0.00
Veloc Dn (ft/s)	= 4.67
Veloc Up (ft/s)	= 5.62
HGL Dn (ft)	= 7021.78
HGL Up (ft)	= 7035.17
Hw Elev (ft)	= 7035.87
Hw/D (ft)	= 1.17
Flow Regime	= Inlet Control



Weir Report

Detention Basin Emergency Spillway Weir-1 (Q100)

Trapezoidal Weir

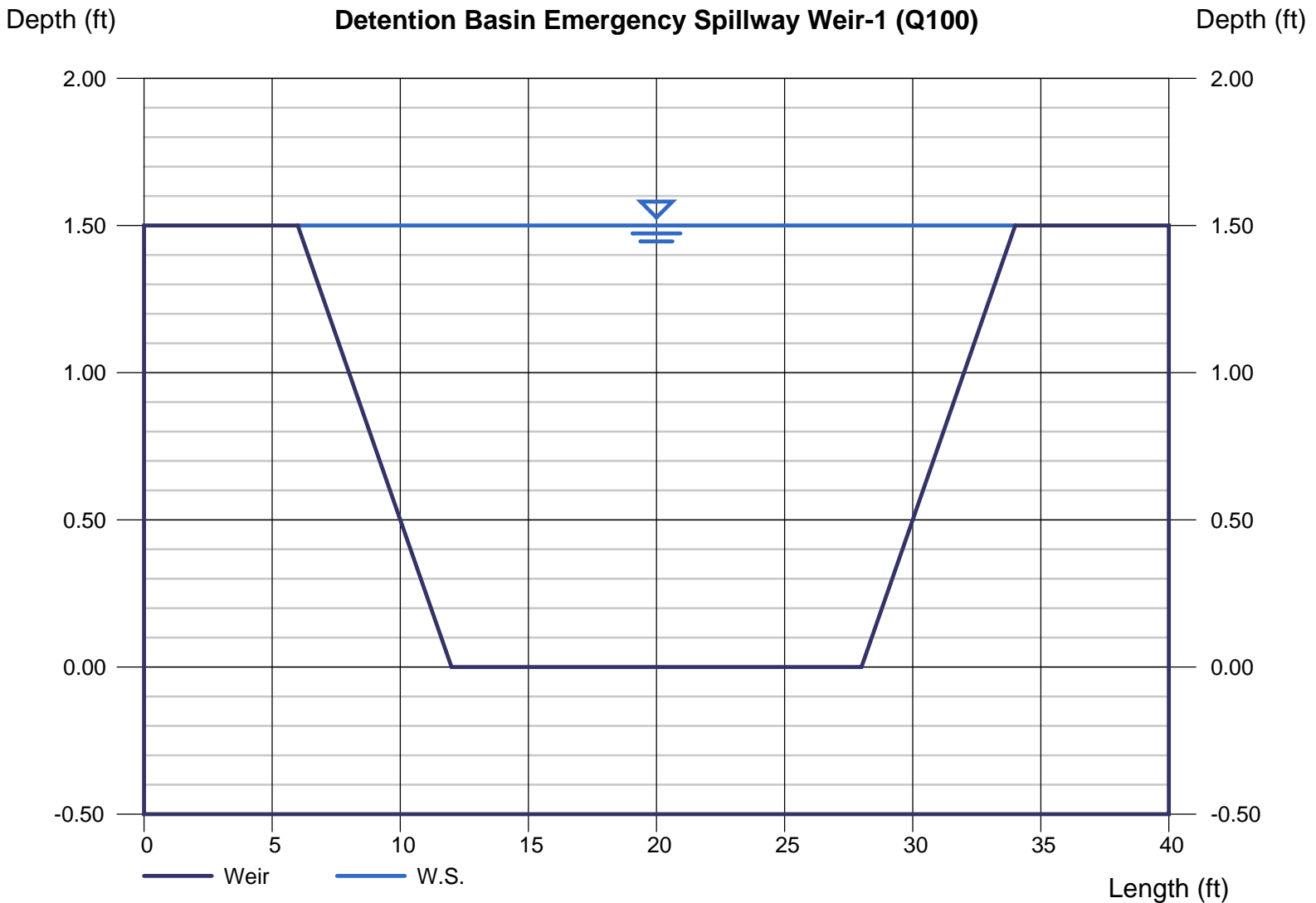
Crest = Sharp
Bottom Length (ft) = 16.00
Total Depth (ft) = 1.50
Side Slope (z:1) = 4.00

Highlighted

Depth (ft) = 1.50
Q (cfs) = 118.00
Area (sqft) = 33.00
Velocity (ft/s) = 3.58
Top Width (ft) = 28.00

Calculations

Weir Coeff. Cw = 3.10
Compute by: Known Q
Known Q (cfs) = 118.00



Weir Report

Detention Basin Emergency Spillway Weir-2 (Q100)

Trapezoidal Weir

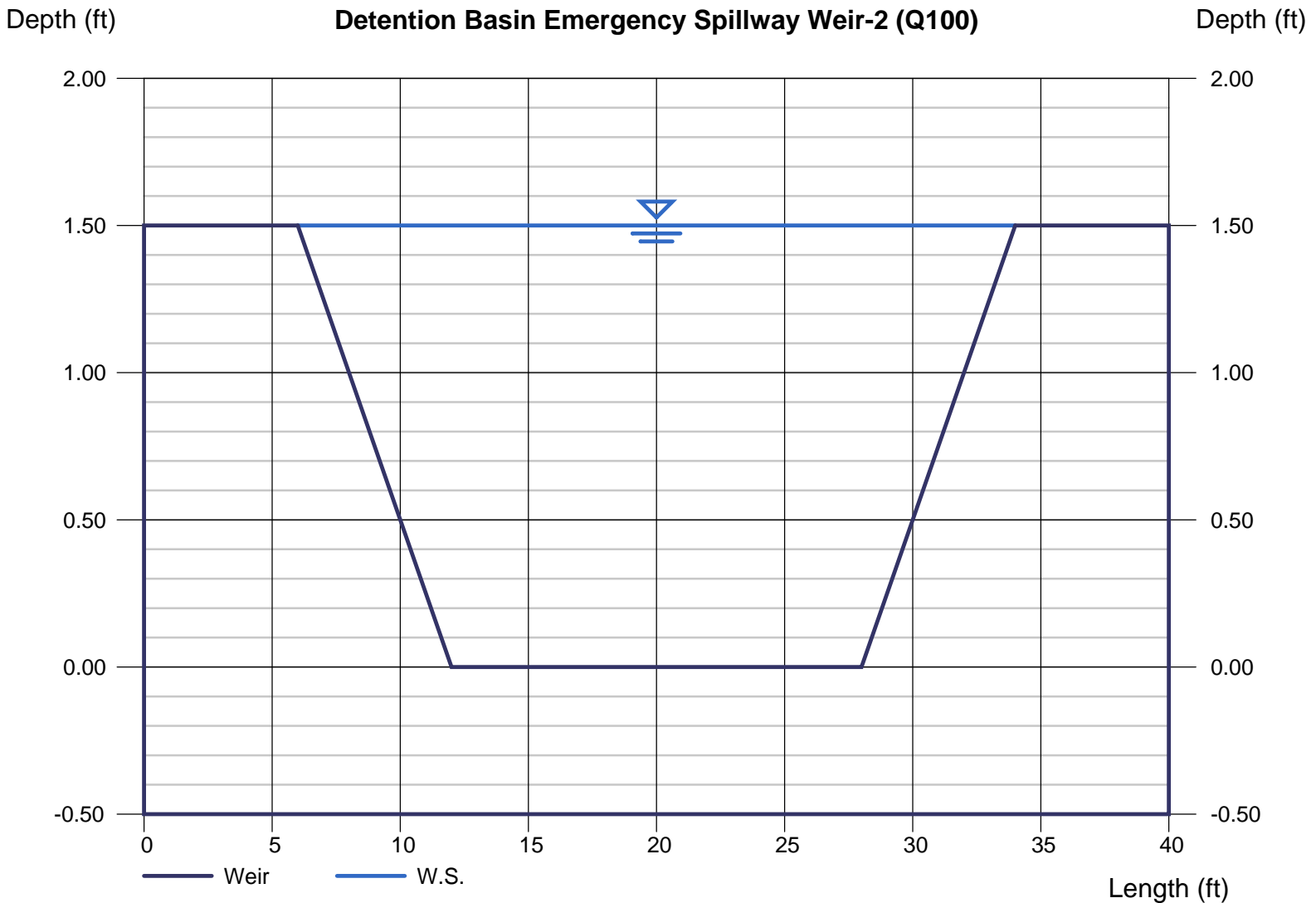
Crest = Sharp
Bottom Length (ft) = 16.00
Total Depth (ft) = 1.50
Side Slope (z:1) = 4.00

Highlighted

Depth (ft) = 1.50
Q (cfs) = 118.00
Area (sqft) = 33.00
Velocity (ft/s) = 3.58
Top Width (ft) = 28.00

Calculations

Weir Coeff. Cw = 3.10
Compute by: Known Q
Known Q (cfs) = 118.00



Channel Report

Emergency Spillway Outlet Channel-2 (Q100)

Rectangular

Bottom Width (ft) = 6.00
Total Depth (ft) = 0.75

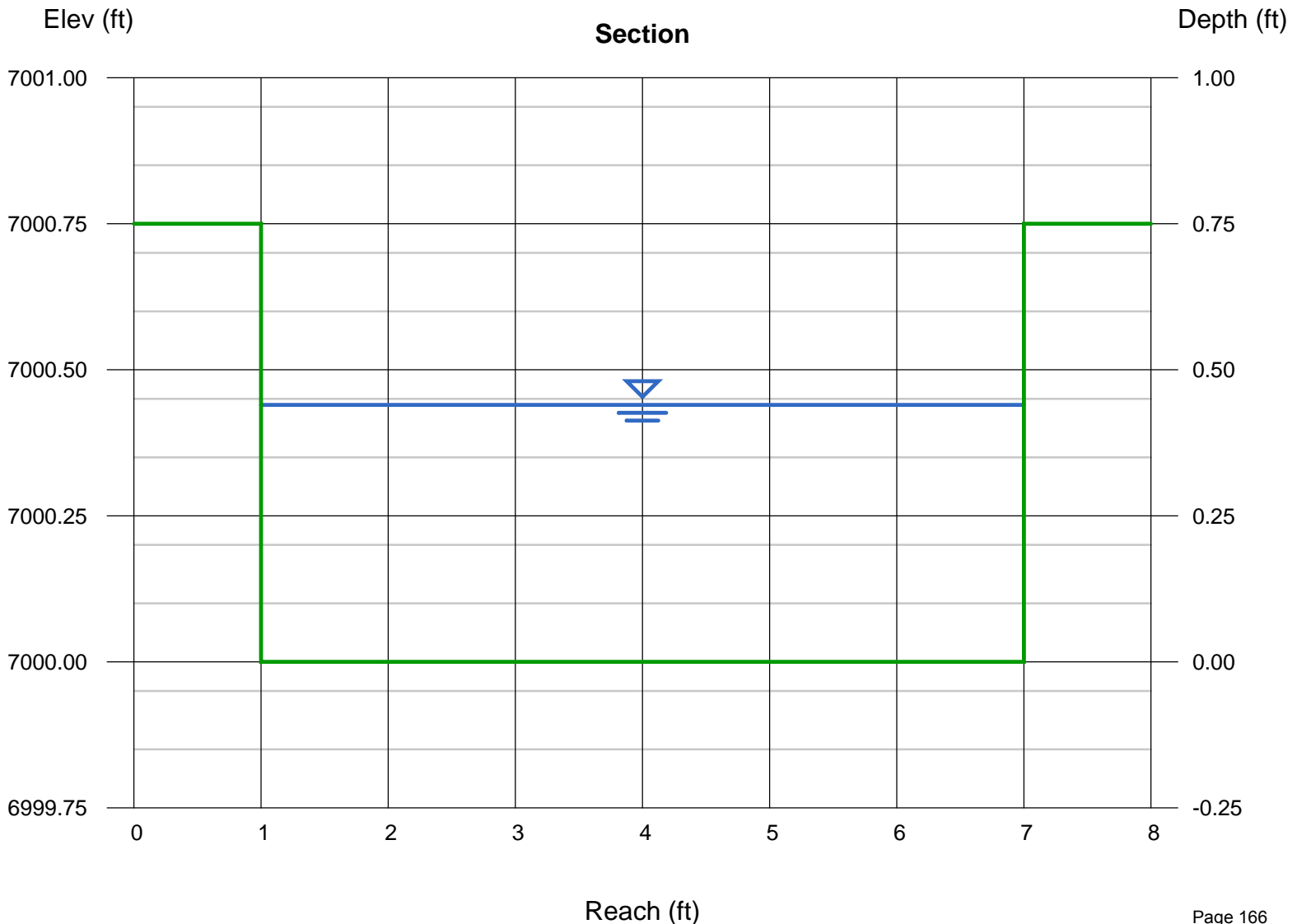
Invert Elev (ft) = 7000.00
Slope (%) = 50.00
N-Value = 0.012

Calculations

Compute by: Known Q
Known Q (cfs) = 118.00

Highlighted

Depth (ft) = 0.44
Q (cfs) = 118.00
Area (sqft) = 2.64
Velocity (ft/s) = 44.70
Wetted Perim (ft) = 6.88
Crit Depth, Yc (ft) = 0.75
Top Width (ft) = 6.00
EGL (ft) = 31.50



Channel Report

Emergency Spillway Outlet Channel-1 (Q100)

Rectangular

Bottom Width (ft) = 6.00
Total Depth (ft) = 0.75

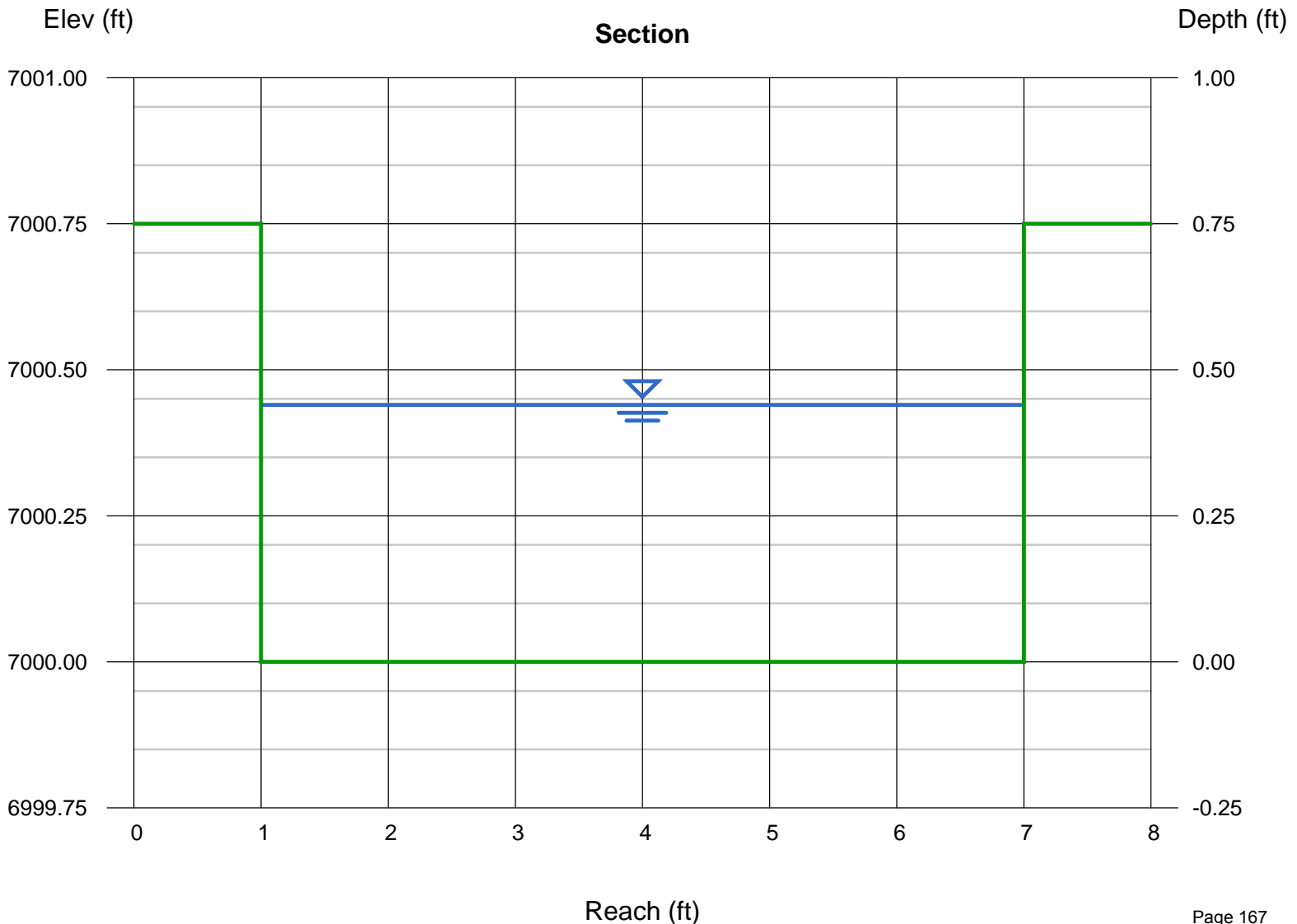
Invert Elev (ft) = 7000.00
Slope (%) = 50.00
N-Value = 0.012

Calculations

Compute by: Known Q
Known Q (cfs) = 118.00

Highlighted

Depth (ft) = 0.44
Q (cfs) = 118.00
Area (sqft) = 2.64
Velocity (ft/s) = 44.70
Wetted Perim (ft) = 6.88
Crit Depth, Yc (ft) = 0.75
Top Width (ft) = 6.00
EGL (ft) = 31.50



Weir Report

Weir LID-1 (Q100)

Trapezoidal Weir

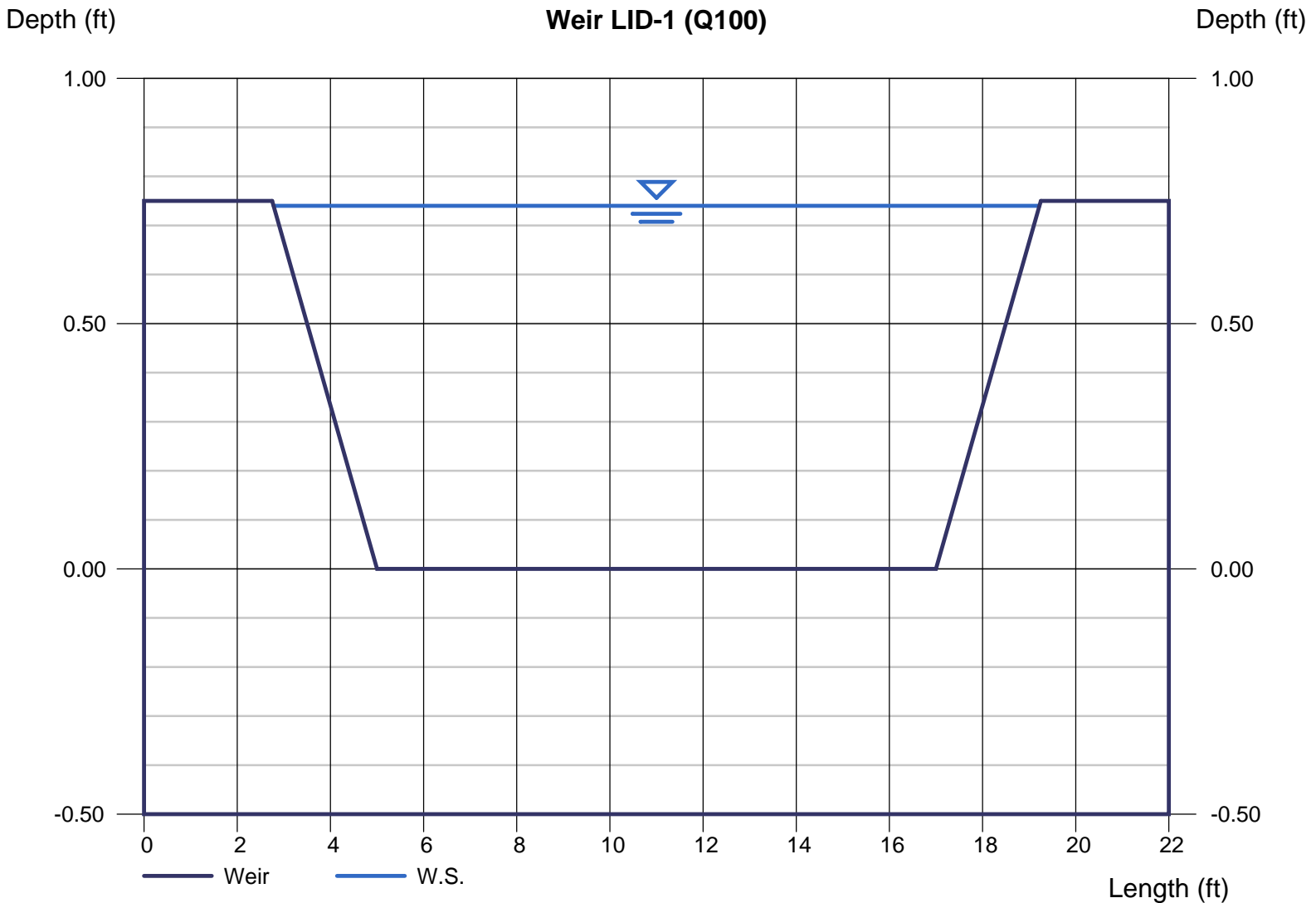
Crest = Sharp
Bottom Length (ft) = 12.00
Total Depth (ft) = 0.75
Side Slope (z:1) = 3.00

Highlighted

Depth (ft) = 0.74
Q (cfs) = 27.00
Area (sqft) = 10.52
Velocity (ft/s) = 2.57
Top Width (ft) = 16.44

Calculations

Weir Coeff. Cw = 3.10
Compute by: Known Q
Known Q (cfs) = 27.00



Weir Report

Weir LID-2 (Q100)

Trapezoidal Weir

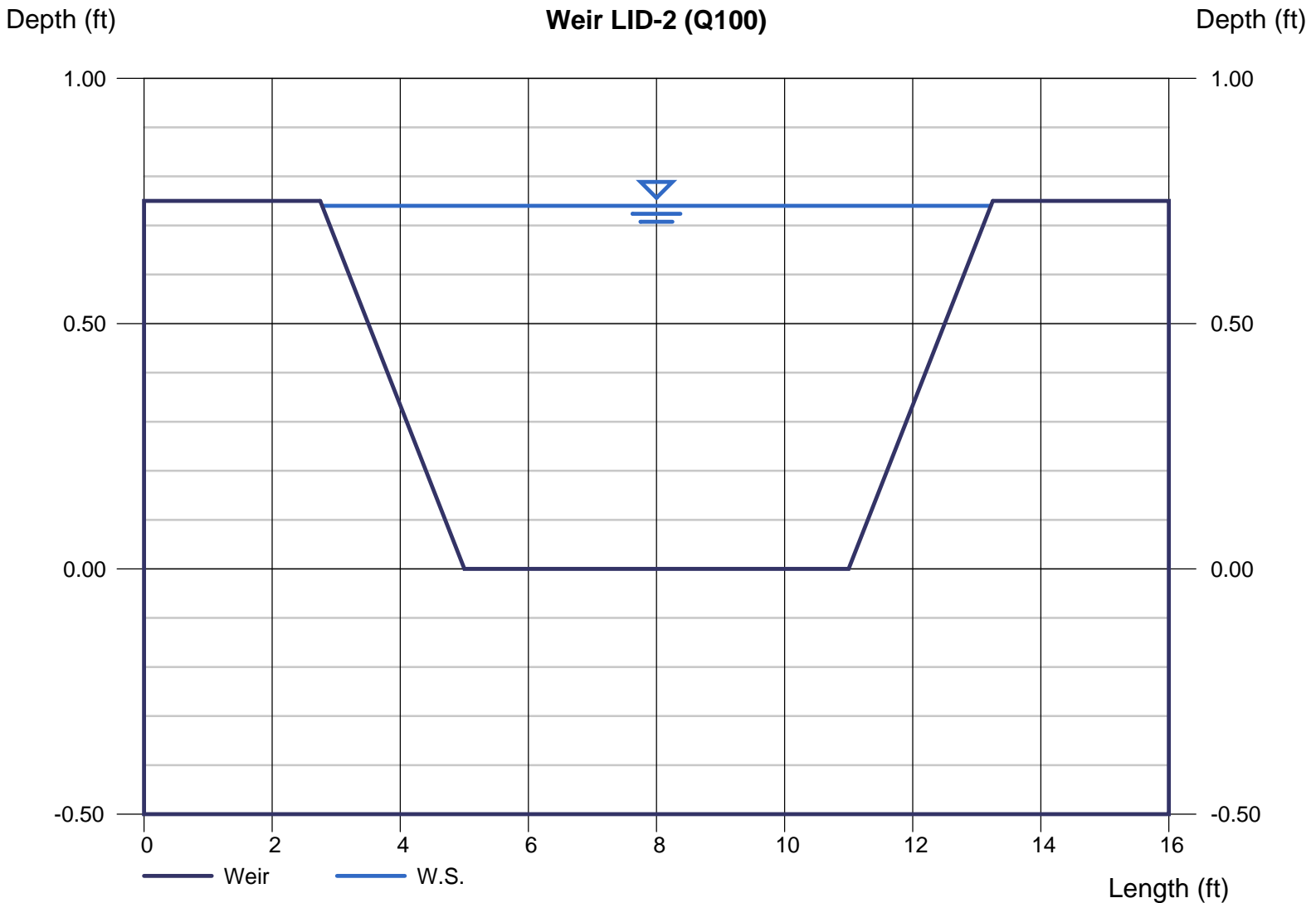
Crest = Sharp
Bottom Length (ft) = 6.00
Total Depth (ft) = 0.75
Side Slope (z:1) = 3.00

Highlighted

Depth (ft) = 0.74
Q (cfs) = 15.00
Area (sqft) = 6.08
Velocity (ft/s) = 2.47
Top Width (ft) = 10.44

Calculations

Weir Coeff. Cw = 3.10
Compute by: Known Q
Known Q (cfs) = 15.00



Weir Report

Weir LID-3 (Q100)

Trapezoidal Weir

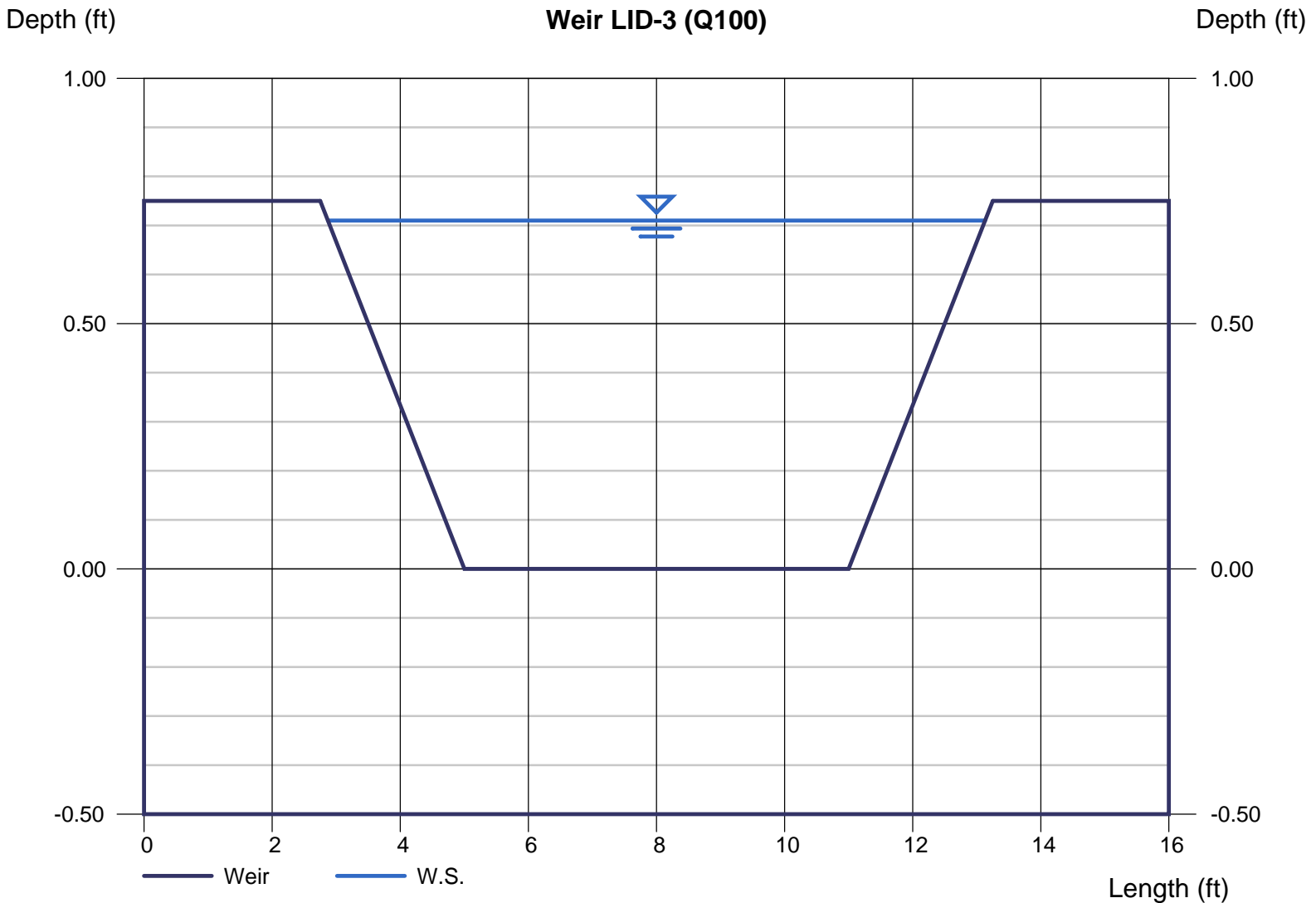
Crest = Sharp
Bottom Length (ft) = 6.00
Total Depth (ft) = 0.75
Side Slope (z:1) = 3.00

Highlighted

Depth (ft) = 0.71
Q (cfs) = 14.00
Area (sqft) = 5.77
Velocity (ft/s) = 2.43
Top Width (ft) = 10.26

Calculations

Weir Coeff. Cw = 3.10
Compute by: Known Q
Known Q (cfs) = 14.00



Channel Report

CHANNEL A (Q100)-Earthen

Trapezoidal

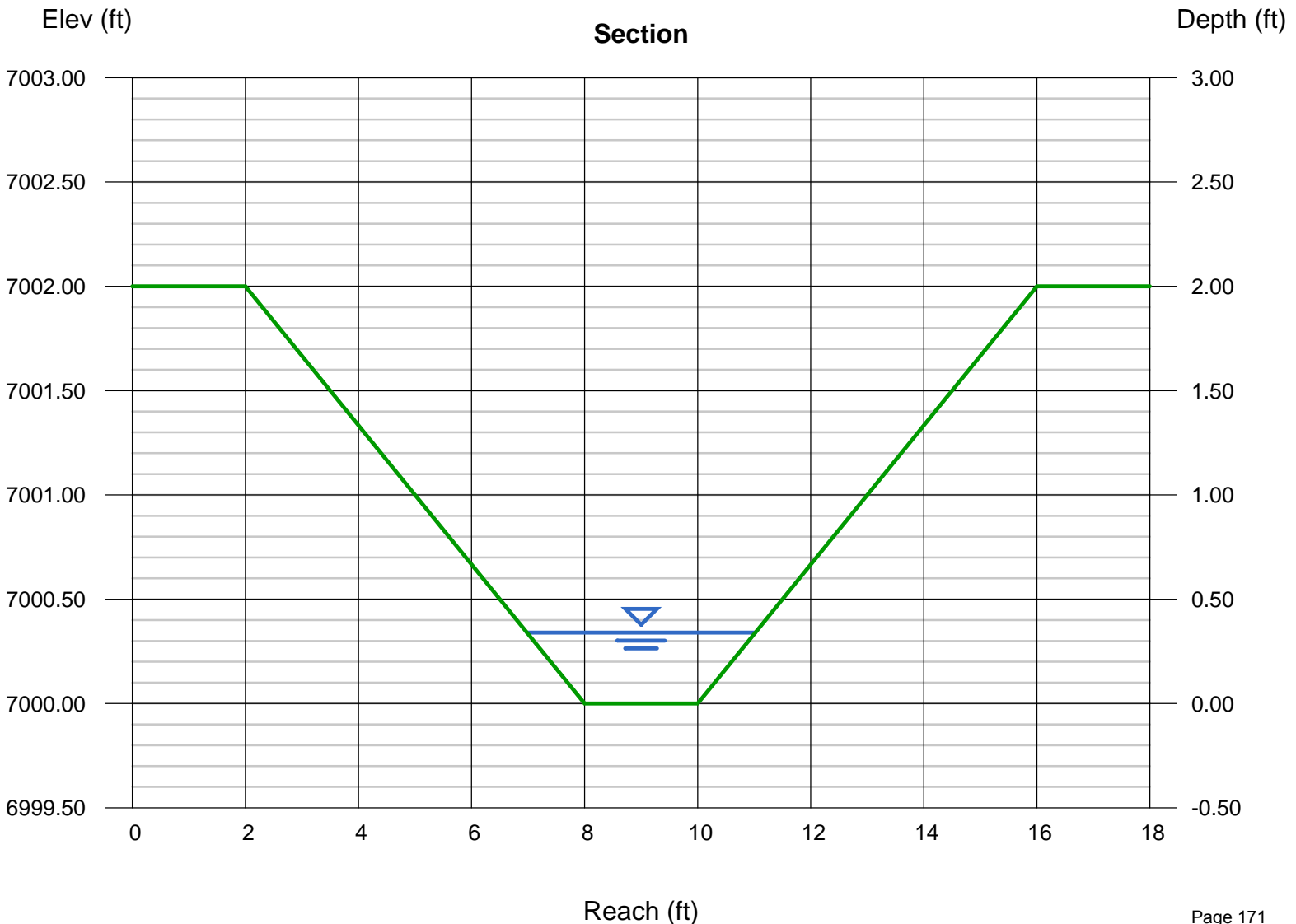
Bottom Width (ft) = 2.00
Side Slopes (z:1) = 3.00, 3.00
Total Depth (ft) = 2.00
Invert Elev (ft) = 7000.00
Slope (%) = 16.67
N-Value = 0.020

Highlighted

Depth (ft) = 0.34
Q (cfs) = 12.00
Area (sqft) = 1.03
Velocity (ft/s) = 11.69
Wetted Perim (ft) = 4.15
Crit Depth, Yc (ft) = 0.73
Top Width (ft) = 4.04
EGL (ft) = 2.46

Calculations

Compute by: Known Q
Known Q (cfs) = 12.00



Channel Report

CHANNEL A (Q100)-Rock Lined

Trapezoidal

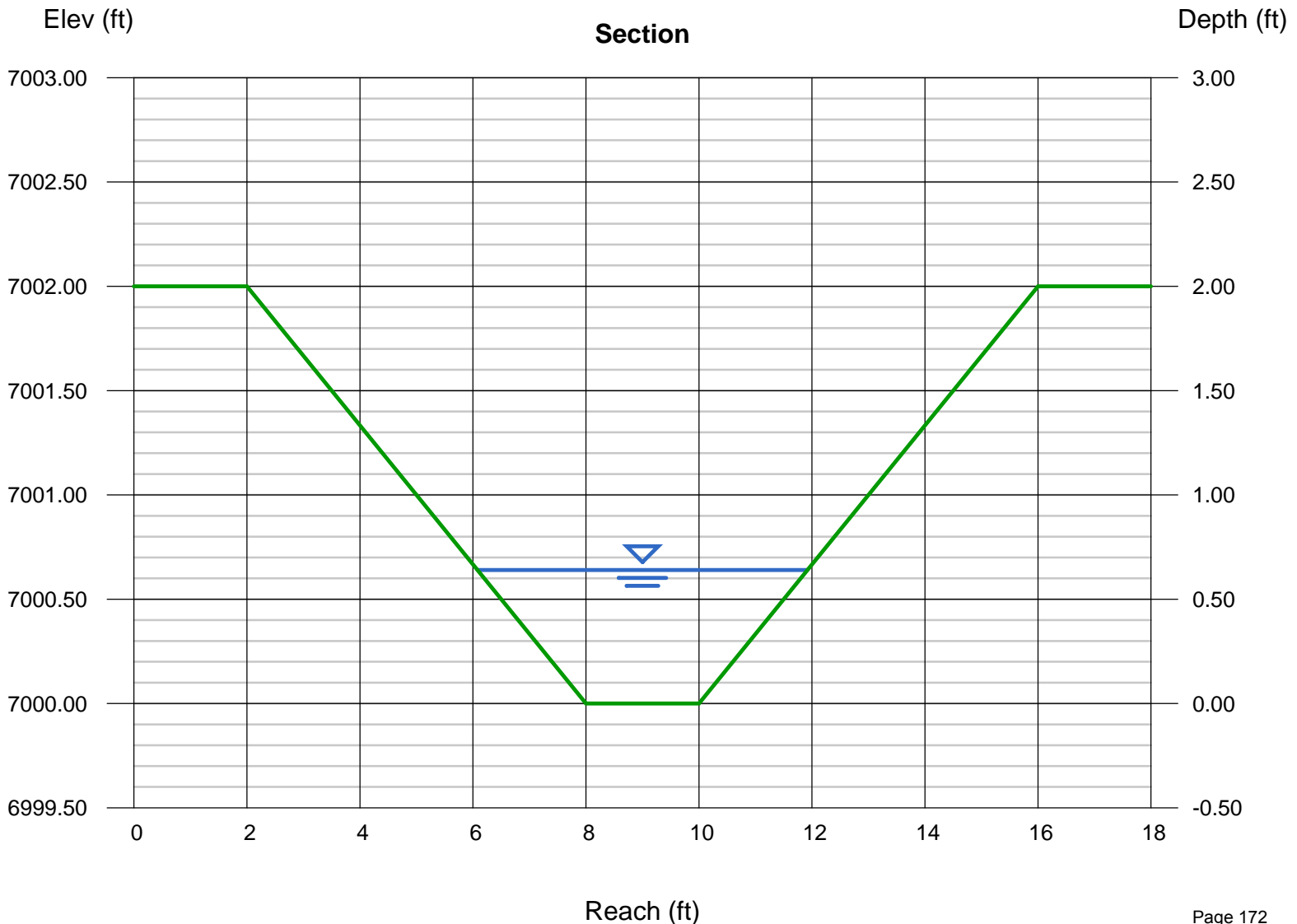
Bottom Width (ft) = 2.00
Side Slopes (z:1) = 3.00, 3.00
Total Depth (ft) = 2.00
Invert Elev (ft) = 7000.00
Slope (%) = 16.67
N-Value = 0.069

Highlighted

Depth (ft) = 0.64
Q (cfs) = 12.00
Area (sqft) = 2.51
Velocity (ft/s) = 4.78
Wetted Perim (ft) = 6.05
Crit Depth, Yc (ft) = 0.73
Top Width (ft) = 5.84
EGL (ft) = 1.00

Calculations

Compute by: Known Q
Known Q (cfs) = 12.00



Channel Report

CHANNEL B (Q100)-Earthen

Trapezoidal

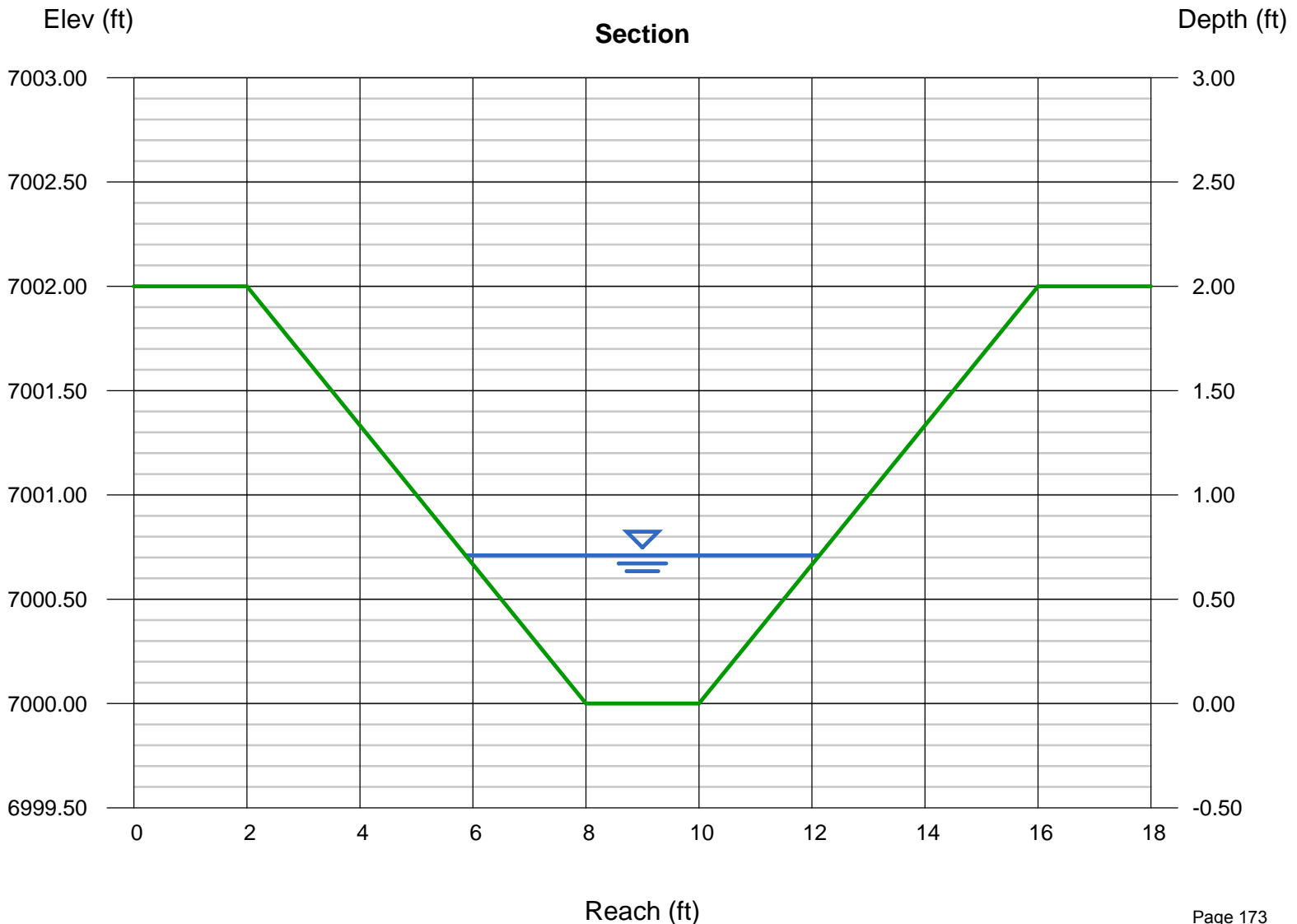
Bottom Width (ft) = 2.00
Side Slopes (z:1) = 3.00, 3.00
Total Depth (ft) = 2.00
Invert Elev (ft) = 7000.00
Slope (%) = 14.20
N-Value = 0.020

Highlighted

Depth (ft) = 0.71
Q (cfs) = 48.00
Area (sqft) = 2.93
Velocity (ft/s) = 16.37
Wetted Perim (ft) = 6.49
Crit Depth, Yc (ft) = 1.45
Top Width (ft) = 6.26
EGL (ft) = 4.88

Calculations

Compute by: Known Q
Known Q (cfs) = 48.00



Channel Report

CHANNEL B (Q100)-Rock Lined

Trapezoidal

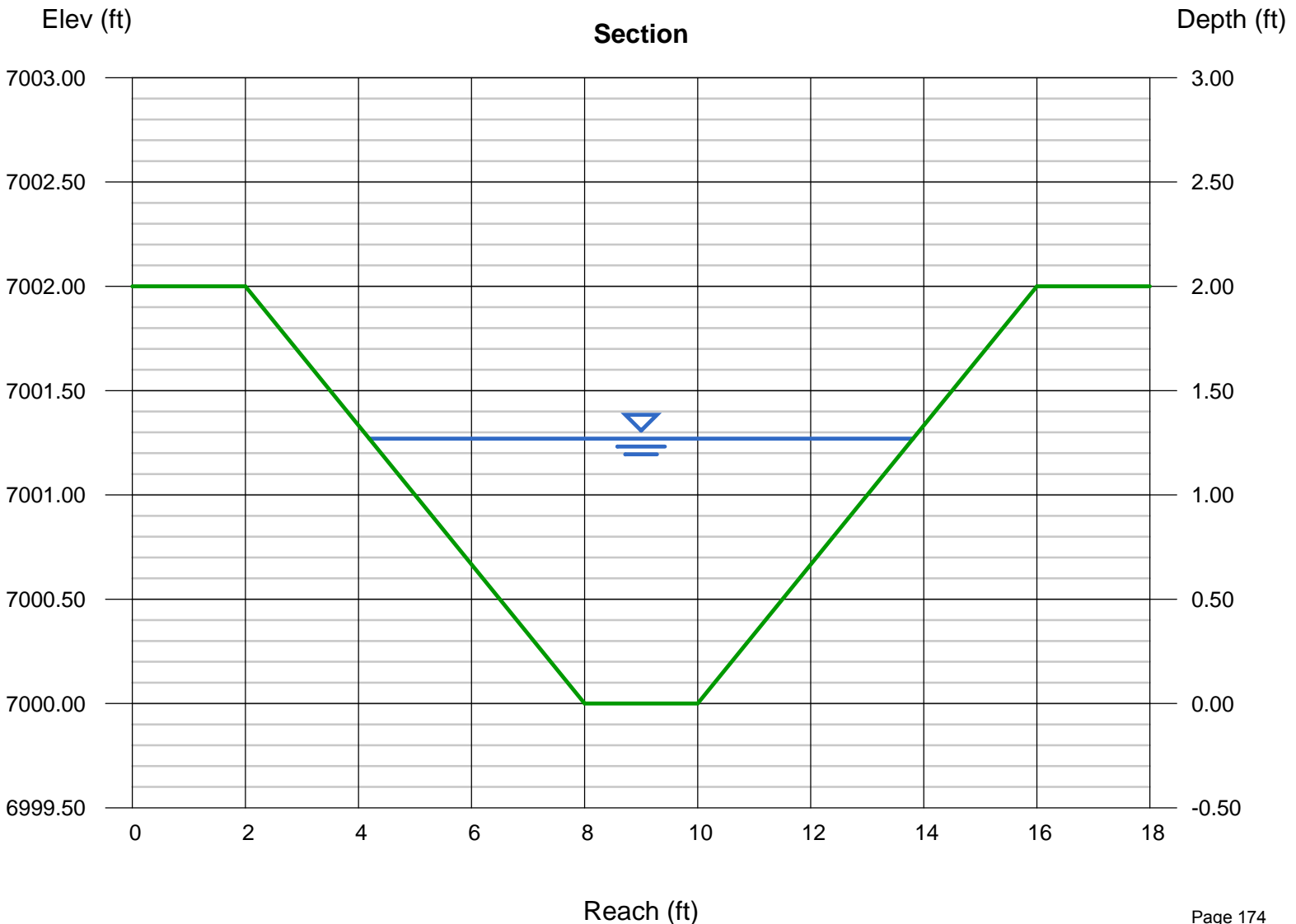
Bottom Width (ft) = 2.00
Side Slopes (z:1) = 3.00, 3.00
Total Depth (ft) = 2.00
Invert Elev (ft) = 7000.00
Slope (%) = 14.20
N-Value = 0.069

Highlighted

Depth (ft) = 1.27
Q (cfs) = 48.00
Area (sqft) = 7.38
Velocity (ft/s) = 6.51
Wetted Perim (ft) = 10.03
Crit Depth, Yc (ft) = 1.45
Top Width (ft) = 9.62
EGL (ft) = 1.93

Calculations

Compute by: Known Q
Known Q (cfs) = 48.00



Channel Report

CHANNEL C (Q100)-Earthen

Trapezoidal

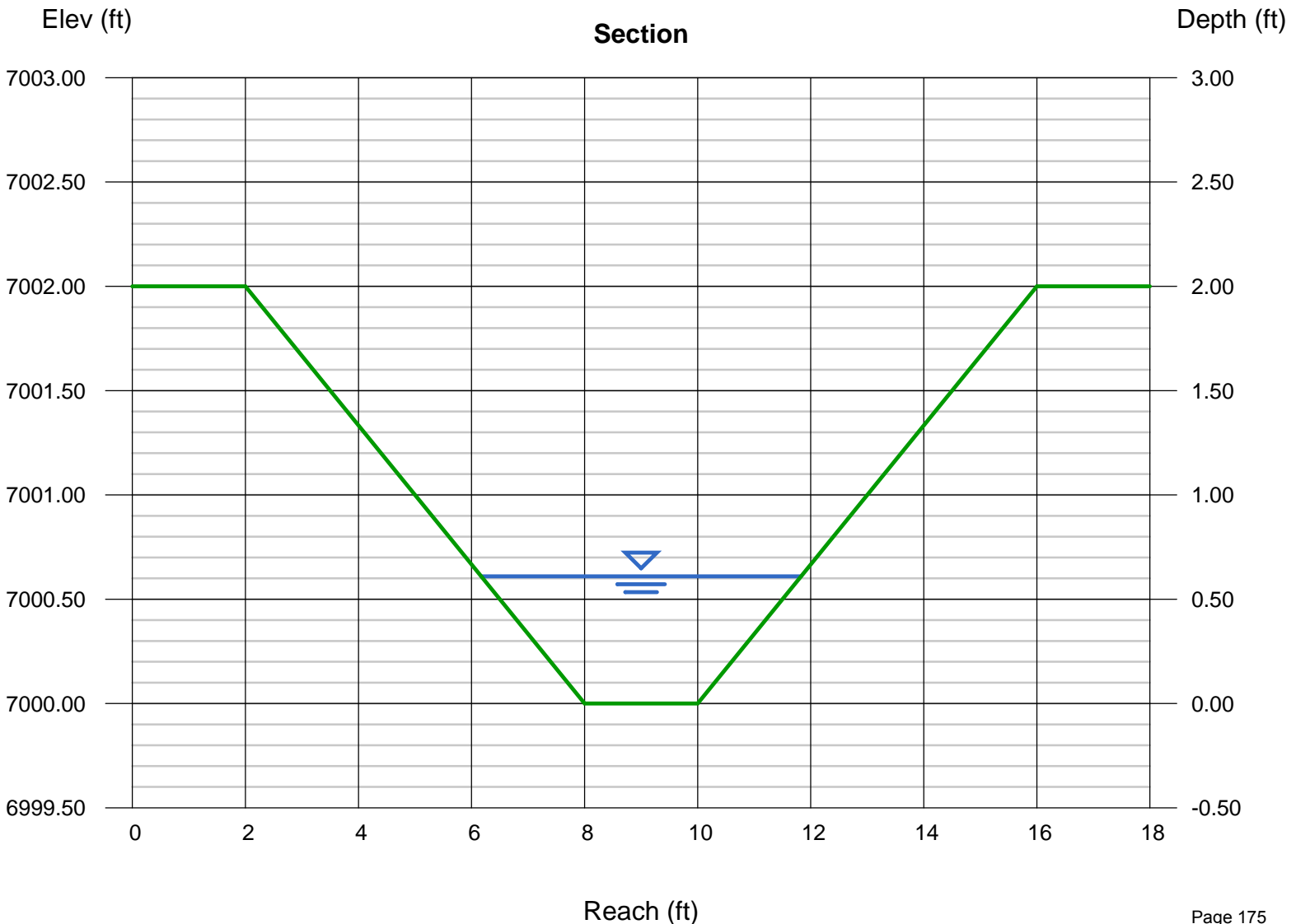
Bottom Width (ft) = 2.00
Side Slopes (z:1) = 3.00, 3.00
Total Depth (ft) = 2.00
Invert Elev (ft) = 7000.00
Slope (%) = 20.00
N-Value = 0.020

Highlighted

Depth (ft) = 0.61
Q (cfs) = 42.00
Area (sqft) = 2.34
Velocity (ft/s) = 17.98
Wetted Perim (ft) = 5.86
Crit Depth, Yc (ft) = 1.36
Top Width (ft) = 5.66
EGL (ft) = 5.63

Calculations

Compute by: Known Q
Known Q (cfs) = 42.00



Channel Report

CHANNEL C (Q100)-Rock Lined

Trapezoidal

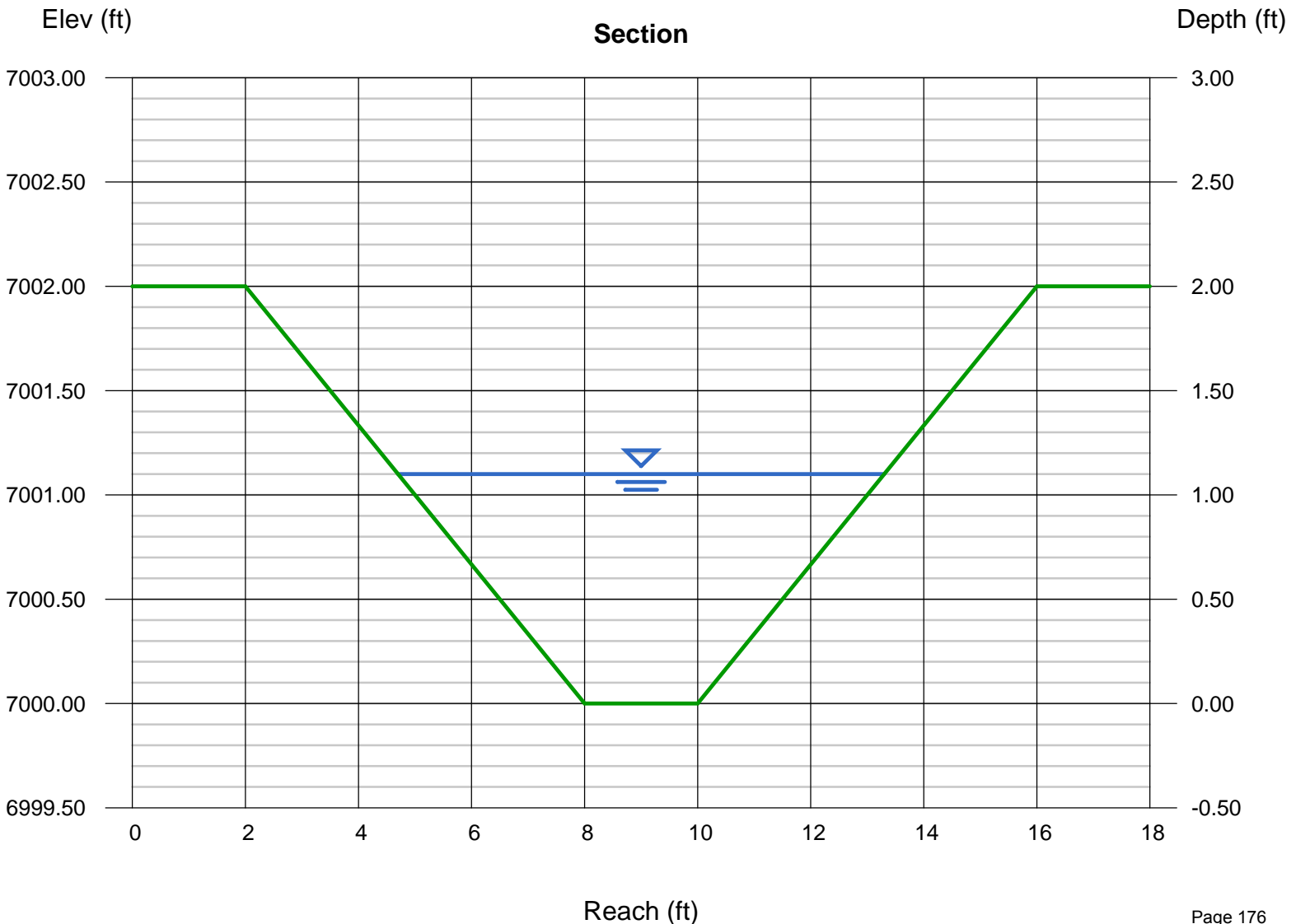
Bottom Width (ft) = 2.00
Side Slopes (z:1) = 3.00, 3.00
Total Depth (ft) = 2.00
Invert Elev (ft) = 7000.00
Slope (%) = 20.00
N-Value = 0.069

Highlighted

Depth (ft) = 1.10
Q (cfs) = 42.00
Area (sqft) = 5.83
Velocity (ft/s) = 7.20
Wetted Perim (ft) = 8.96
Crit Depth, Yc (ft) = 1.36
Top Width (ft) = 8.60
EGL (ft) = 1.91

Calculations

Compute by: Known Q
Known Q (cfs) = 42.00



Channel Report

CHANNEL D (Q100)-Earthen

Trapezoidal

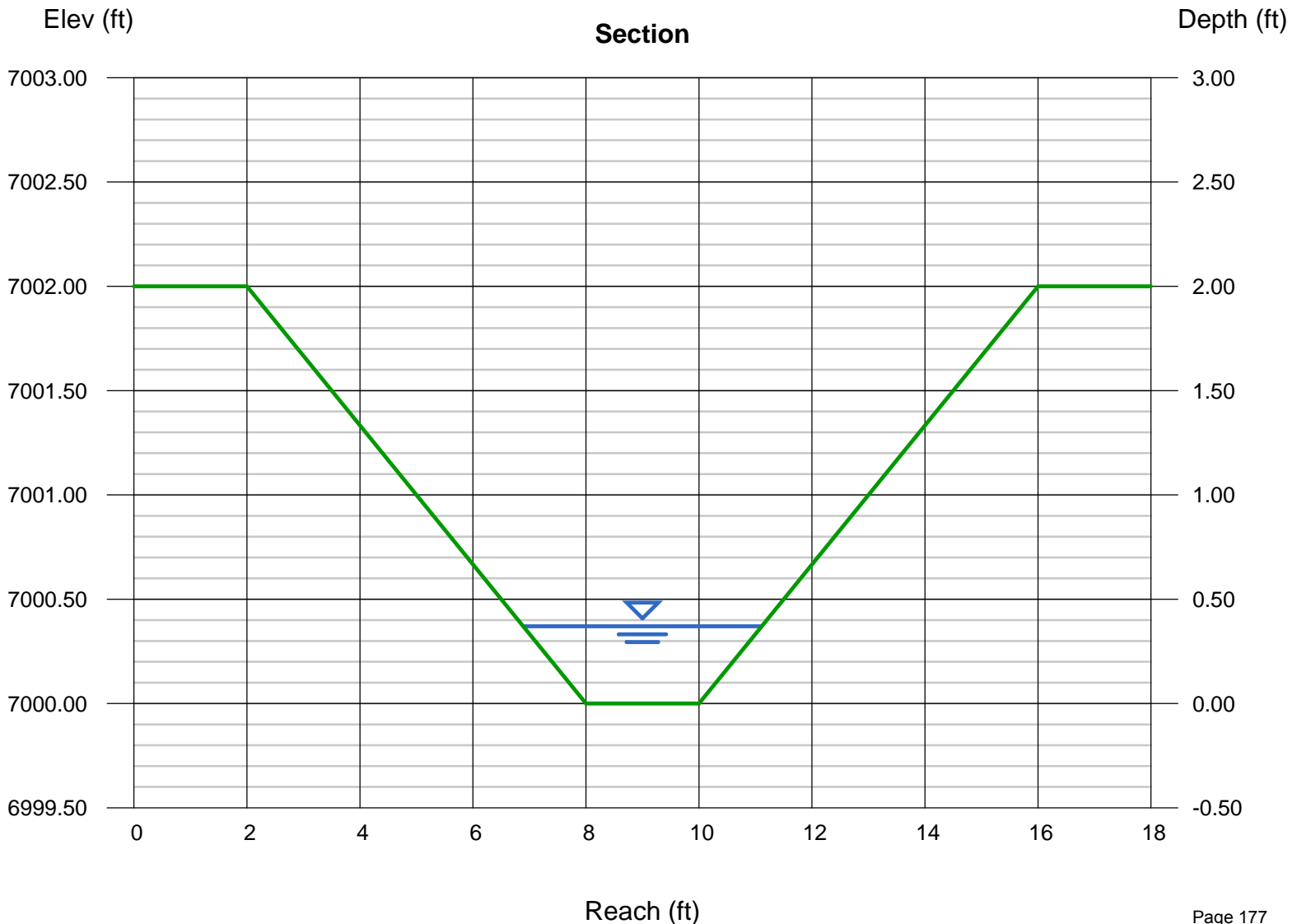
Bottom Width (ft) = 2.00
Side Slopes (z:1) = 3.00, 3.00
Total Depth (ft) = 2.00
Invert Elev (ft) = 7000.00
Slope (%) = 20.00
N-Value = 0.020

Highlighted

Depth (ft) = 0.37
Q (cfs) = 15.00
Area (sqft) = 1.15
Velocity (ft/s) = 13.04
Wetted Perim (ft) = 4.34
Crit Depth, Yc (ft) = 0.82
Top Width (ft) = 4.22
EGL (ft) = 3.01

Calculations

Compute by: Known Q
Known Q (cfs) = 15.00



Channel Report

CHANNEL D (Q100)-Rock Lined

Trapezoidal

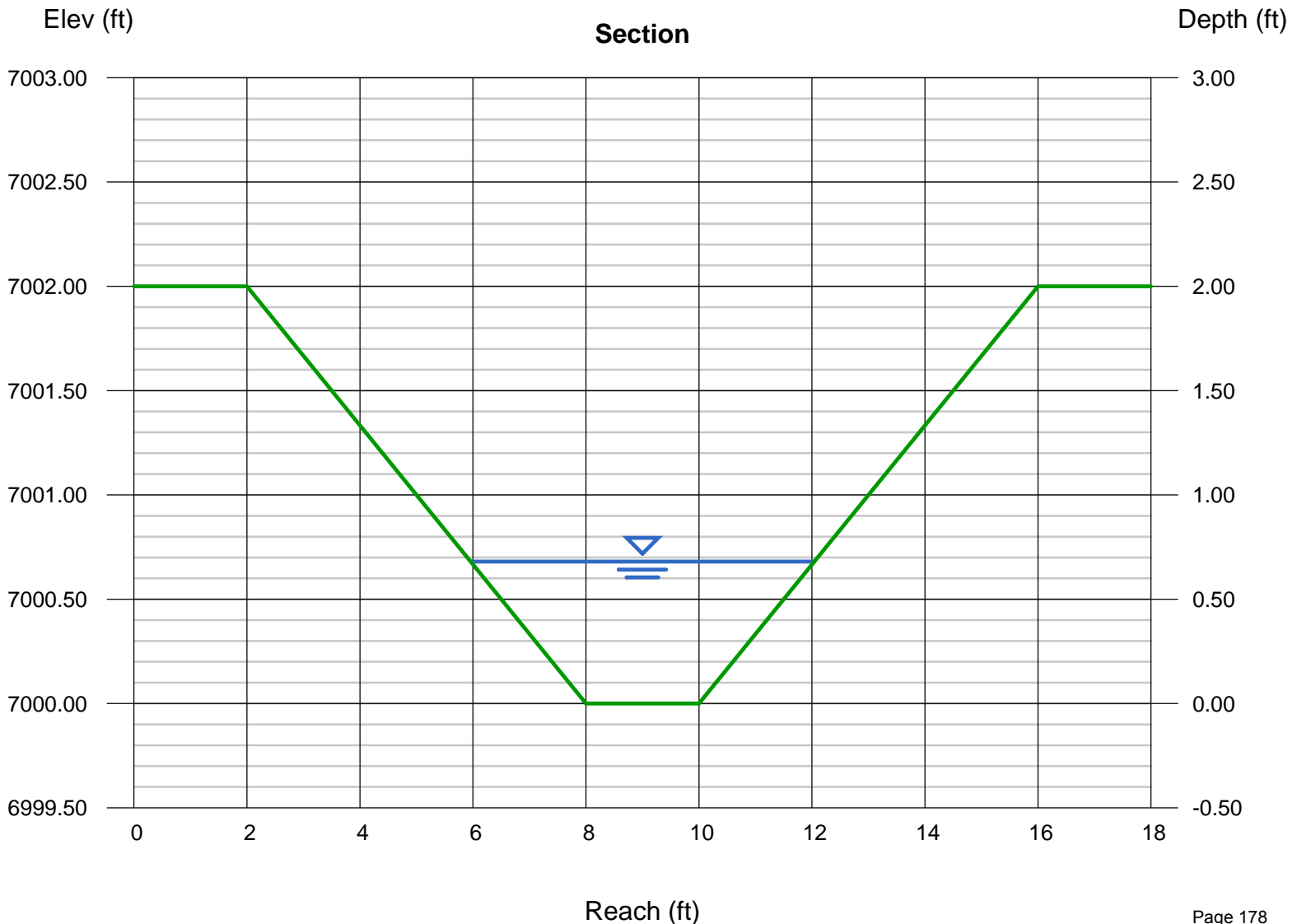
Bottom Width (ft) = 2.00
Side Slopes (z:1) = 3.00, 3.00
Total Depth (ft) = 2.00
Invert Elev (ft) = 7000.00
Slope (%) = 20.00
N-Value = 0.069

Highlighted

Depth (ft) = 0.68
Q (cfs) = 15.00
Area (sqft) = 2.75
Velocity (ft/s) = 5.46
Wetted Perim (ft) = 6.30
Crit Depth, Yc (ft) = 0.82
Top Width (ft) = 6.08
EGL (ft) = 1.14

Calculations

Compute by: Known Q
Known Q (cfs) = 15.00



Channel Report

CHANNEL E (Q100)-Earthen

Trapezoidal

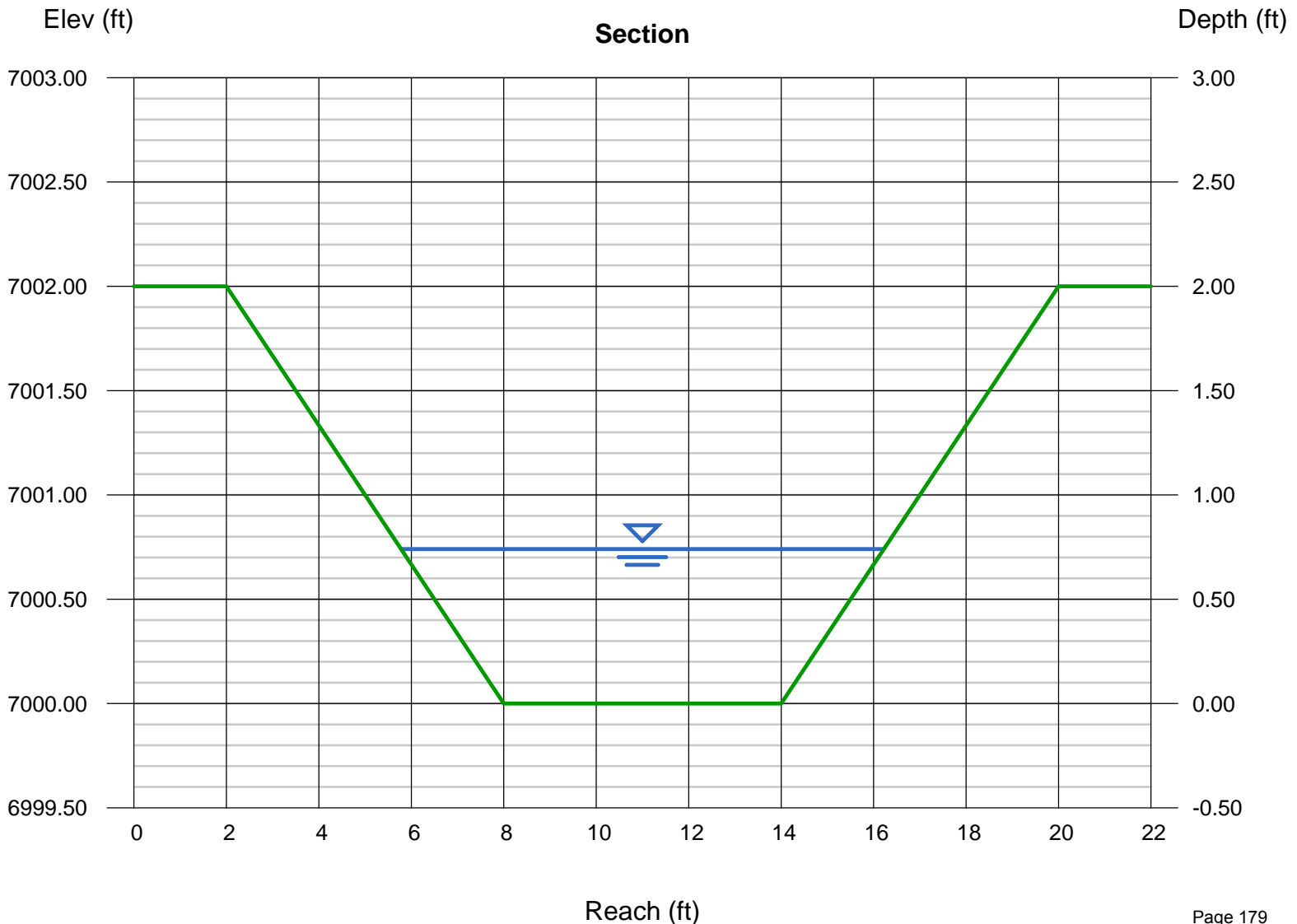
Bottom Width (ft) = 6.00
Side Slopes (z:1) = 3.00, 3.00
Total Depth (ft) = 2.00
Invert Elev (ft) = 7000.00
Slope (%) = 20.00
N-Value = 0.020

Highlighted

Depth (ft) = 0.74
Q (cfs) = 137.00
Area (sqft) = 6.08
Velocity (ft/s) = 22.52
Wetted Perim (ft) = 10.68
Crit Depth, Yc (ft) = 1.87
Top Width (ft) = 10.44
EGL (ft) = 8.63

Calculations

Compute by: Known Q
Known Q (cfs) = 137.00



Channel Report

CHANNEL E (Q100)-Rock Lined

Trapezoidal

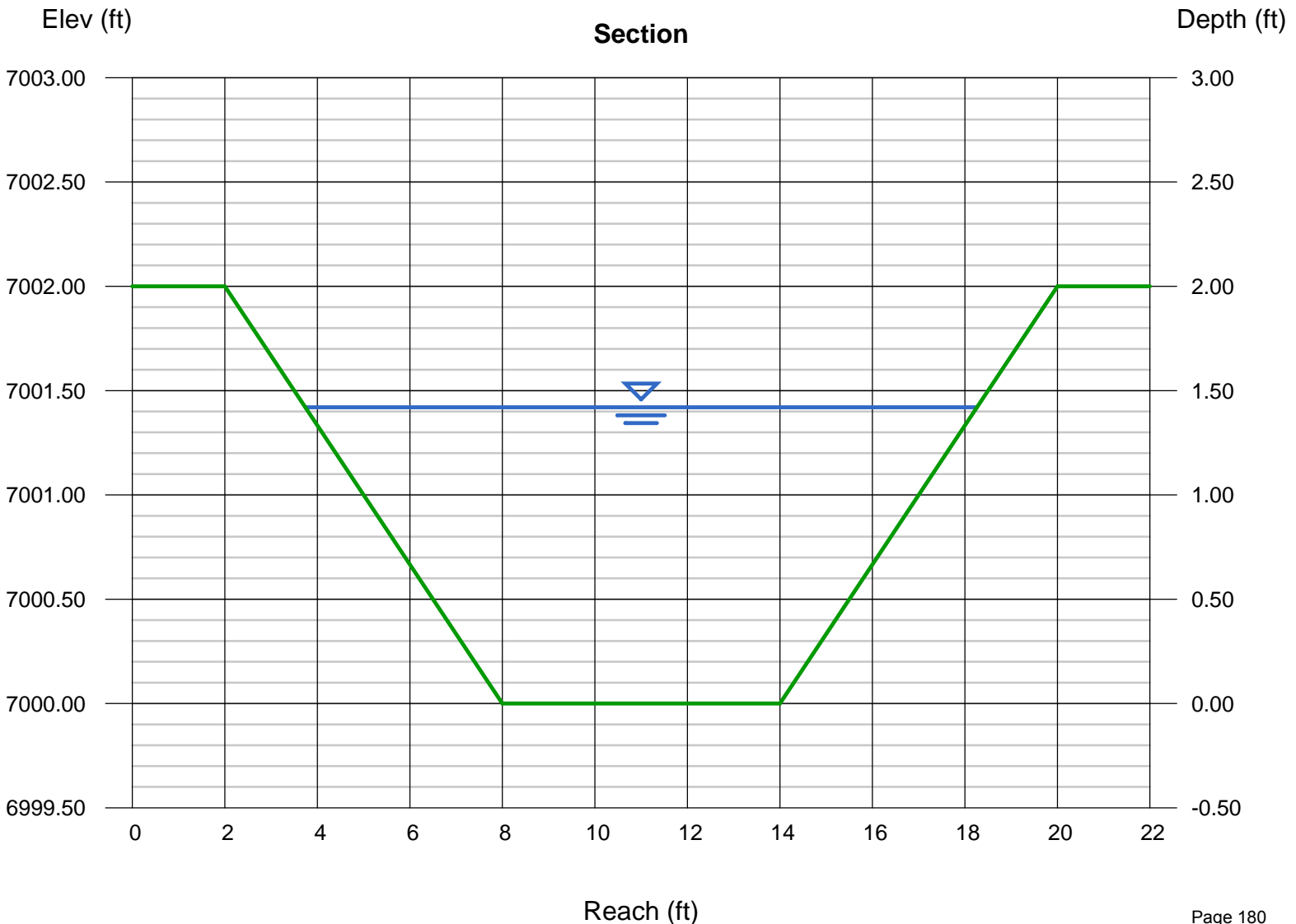
Bottom Width (ft) = 6.00
Side Slopes (z:1) = 3.00, 3.00
Total Depth (ft) = 2.00
Invert Elev (ft) = 7000.00
Slope (%) = 20.00
N-Value = 0.069

Highlighted

Depth (ft) = 1.42
Q (cfs) = 137.00
Area (sqft) = 14.57
Velocity (ft/s) = 9.40
Wetted Perim (ft) = 14.98
Crit Depth, Yc (ft) = 1.87
Top Width (ft) = 14.52
EGL (ft) = 2.79

Calculations

Compute by: Known Q
Known Q (cfs) = 137.00



Channel Report

CHANNEL F (Q100)-Earthen

Trapezoidal

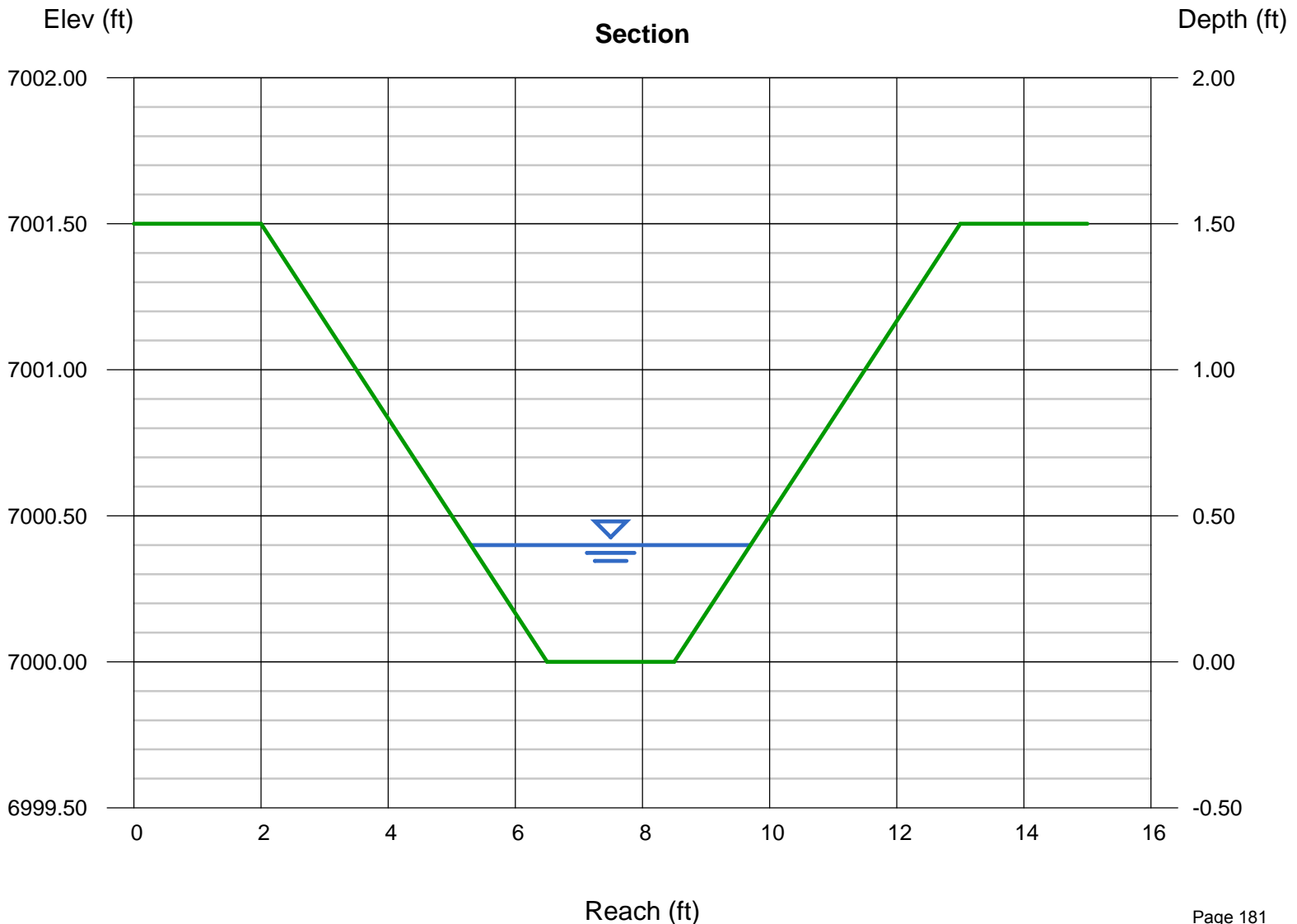
Bottom Width (ft) = 2.00
Side Slopes (z:1) = 3.00, 3.00
Total Depth (ft) = 1.50
Invert Elev (ft) = 7000.00
Slope (%) = 12.50
N-Value = 0.020

Highlighted

Depth (ft) = 0.40
Q (cfs) = 14.00
Area (sqft) = 1.28
Velocity (ft/s) = 10.94
Wetted Perim (ft) = 4.53
Crit Depth, Yc (ft) = 0.79
Top Width (ft) = 4.40
EGL (ft) = 2.26

Calculations

Compute by: Known Q
Known Q (cfs) = 14.00



Channel Report

CHANNEL F (Q100)-Rock Lined

Trapezoidal

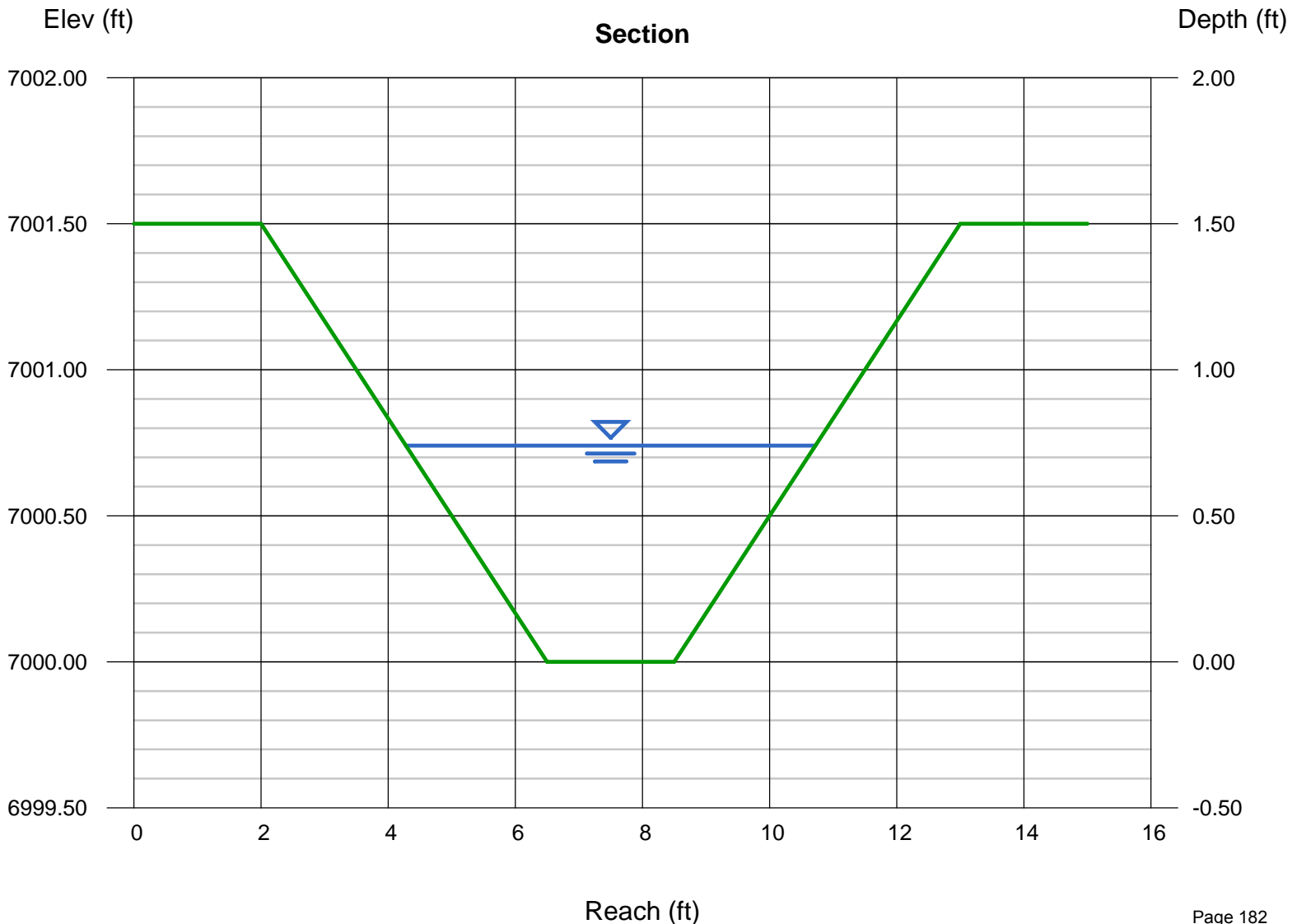
Bottom Width (ft) = 2.00
Side Slopes (z:1) = 3.00, 3.00
Total Depth (ft) = 1.50
Invert Elev (ft) = 7000.00
Slope (%) = 12.50
N-Value = 0.069

Highlighted

Depth (ft) = 0.74
Q (cfs) = 14.00
Area (sqft) = 3.12
Velocity (ft/s) = 4.48
Wetted Perim (ft) = 6.68
Crit Depth, Yc (ft) = 0.79
Top Width (ft) = 6.44
EGL (ft) = 1.05

Calculations

Compute by: Known Q
Known Q (cfs) = 14.00



APPENDIX D

Geotechnical Report by Western Technologies
Excerpts from Presidio in Pines Drainage Report



September 26, 2018

Woodson Engineering
124 North Elden Street, Suite 100
Flagstaff, Arizona 86001

Attn: Ms. Sirisha Kalluri, PE, CFM

Re: COF WWH Detention Basin
West Route 66 and Northwestern Street
Flagstaff, Arizona

Job No. 2528JW053

In accordance with our Proposal No. 2527PW137 dated August 9, 2017, we have completed some field exploration, laboratory testing, and field infiltration testing services for the above referenced project. Attached are the test pit location diagram, test pit logs and laboratory test results. Field infiltration testing was performed in each test pit. The following results were obtained:

Test Location	Test Depth (ft.)	Infiltration Rate (minutes/inch)
Test Pit 1	4.0	20
Test Pit 2	4.0	15

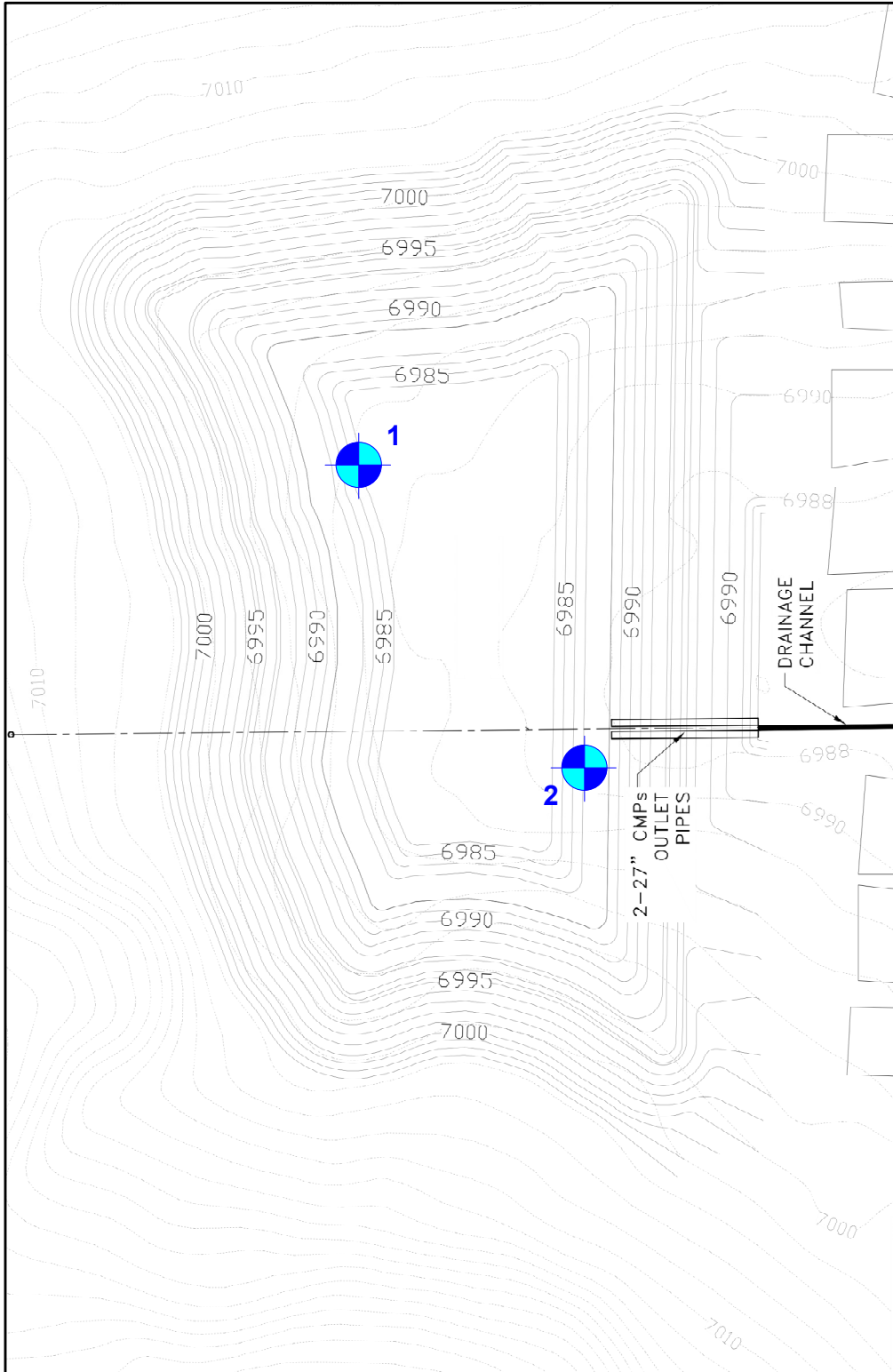
This completes our current services on this project. If you have any questions concerning this information, or require additional consultation, design, observation, or testing services, please contact us. We look forward to working with you on future projects.

Sincerely,
WESTERN TECHNOLOGIES INC.
Geotechnical Engineering Services



Craig P. Wiedeman, P.E.
Senior Geotechnical Engineer

Copies to: Addressee (emailed)



Not to Scale



Approximate Test Pit Location

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COF WWH DETENTION BASIN

Test Pit Location Diagram

Western Technologies Inc.

Job No.: 2528JW053

Plate: 1

COARSE-GRAINED SOILS
LESS THAN 50% FINES

GROUP SYMBOLS	DESCRIPTION	MAJOR DIVISIONS
GW	WELL-GRADED GRAVEL OR WELL-GRADED GRAVEL WITH SAND, LESS THAN 5% FINES	GRAVELS MORE THAN HALF OF COARSE FRACTION IS LARGER THAN NO. 4 SIEVE SIZE
GP	POORLY-GRADED GRAVEL OR POORLY-GRADED GRAVEL WITH SAND, LESS THAN 5% FINES	
GM	SILTY GRAVEL OR SILTY GRAVEL WITH SAND, MORE THAN 12% FINES	
GC	CLAYEY GRAVEL OR CLAYEY GRAVEL WITH SAND, MORE THAN 12% FINES	
SW	WELL-GRADED SAND OR WELL-GRADED SAND WITH GRAVEL, LESS THAN 5% FINES	SANDS MORE THAN HALF OF COARSE FRACTION IS SMALLER THAN NO. 4 SIEVE SIZE
SP	POORLY-GRADED SAND OR POORLY-GRADED SAND WITH GRAVEL, LESS THAN 5% FINES	
SM	SILTY SAND OR SILTY SAND WITH GRAVEL, MORE THAN 12% FINES	
SC	CLAYEY SAND OR CLAYEY SAND WITH GRAVEL, MORE THAN 12% FINES	

NOTE: Coarse-grained soils receive dual symbols if they contain 5% to 12% fines (e.g., SW-SM, GP-GC).

FINE-GRAINED SOILS
MORE THAN 50% FINES

GROUP SYMBOLS	DESCRIPTION	MAJOR DIVISIONS
ML	SILT, SILT WITH SAND OR GRAVEL, SANDY SILT, OR GRAVELLY SILT	SILTS AND CLAYS LIQUID LIMIT LESS THAN 50
CL	LEAN CLAY OF LOW TO MEDIUM PLASTICITY, SANDY CLAY, OR GRAVELLY CLAY	
OL	ORGANIC SILT OR ORGANIC CLAY OF LOW TO MEDIUM PLASTICITY	
MH	ELASTIC SILT, SANDY ELASTIC SILT, OR GRAVELLY ELASTIC SILT	SILTS AND CLAYS LIQUID LIMIT MORE THAN 50
CH	FAT CLAY OF HIGH PLASTICITY, SANDY FAT CLAY, OR GRAVELLY FAT CLAY	
OH	ORGANIC SILT OR ORGANIC CLAY OF HIGH PLASTICITY	
PT	PEAT AND OTHER HIGHLY ORGANIC SOILS	HIGHLY ORGANIC SOILS

NOTE: Fine-grained soils may receive dual classification based upon plasticity characteristics (e.g. CL-ML).

SOIL SIZES

COMPONENT	SIZE RANGE
BOULDERS	Above 12 in.
COBBLES	3 in. – 12 in.
GRAVEL	No. 4 – 3 in.
Coarse	¾ in. – 3 in.
Fine	No. 4 – ¾ in.
SAND	No. 200 – No. 4
Coarse	No. 10 – No. 4
Medium	No. 40 – No. 10
Fine	No. 200 – No. 40
Fines (Silt or Clay)	Below No. 200

NOTE: Only sizes smaller than three inches are used to classify soils

CONSISTENCY

CLAYS & SILTS	BLOWS PER FOOT
VERY SOFT	0 – 2
SOFT	3 – 4
FIRM	5 – 8
STIFF	9 – 15
VERY STIFF	16 – 30
HARD	OVER 30

RELATIVE DENSITY

SANDS & GRAVELS	BLOWS PER FOOT
VERY LOOSE	0 – 4
LOOSE	5 – 10
MEDIUM DENSE	11 – 30
DENSE	31 – 50
VERY DENSE	OVER 50

NOTE: Number of blows using 140-pound hammer falling 30 inches to drive a 2-inch-OD (1½-inch ID) split-barrel sampler (ASTM D1586).

PLASTICITY OF FINE GRAINED SOILS

PLASTICITY INDEX	TERM
0	NON-PLASTIC
1 – 7	LOW
8 – 20	MEDIUM
Over 20	HIGH

DEFINITION OF WATER CONTENT

DRY
SLIGHTLY DAMP
DAMP
MOIST
WET
SATURATED

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METHOD OF CLASSIFICATION

PLATE

A-1

The number shown in "TEST PIT" refers to the approximate location of the same number indicated on the "Test Pit Location Diagram" as positioned in the field by pacing or measurement from property lines and/or existing features.

"EQUIPMENT TYPE" refers to the equipment used in the excavation of the test pit, and may include the width of the bucket on the excavator and the use of "rock" teeth or attachments.

"SAMPLE TYPE" refers to the form of sample recovery, in which **R** = Ring sample and **G** = Grab Sample.

"DRY DENSITY (LBS/CU FT)" refers to the laboratory-determined dry density in pounds per cubic foot.

"WATER (MOISTURE) CONTENT" (% of Dry Wt.) refers to the laboratory-determined water content in percent using the standard test method ASTM D2216.

"USCS" refers to the "Unified Soil Classification System" Group Symbol for the soil type as defined by ASTM D2487 and D2488. The soils were classified visually in the field, and where appropriate, classifications were modified by visual examination of samples in the laboratory and/or by appropriate tests.

These notes and test pit logs are intended for use in conjunction with the purposes of our services defined in the text. Test pit log data should not be construed as part of the construction plans nor as defining construction conditions.

The test pit logs depict our interpretations of subsurface conditions at the locations and on the date(s) noted. Variations in subsurface conditions and characteristics may occur between test pits. Groundwater levels may fluctuate due to seasonal variations and other factors.

The stratification lines shown on the test pit logs represent our interpretation of the approximate boundary between soil or rock types based upon visual field classification at the test pit location. The transition between materials is approximate and may be more or less gradual than indicated.

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TEST PIT LOG NOTES



PLATE
A-2

DATE EXCAVATED: 8-29-18
 LOCATION: See Location Diagram
 ELEVATION: Not Determined

TEST PIT NO. 1

EQUIPMENT: DEERE 310K
 EXCAVATION TYPE: 24" bucket
 FIELD ENGINEER: G. Burr

THIS SUMMARY APPLIES ONLY AT THIS LOCATION AND AT THE TIME OF LOGGING. CONDITIONS MAY DIFFER AT OTHER LOCATIONS AND MAY CHANGE AT THIS LOCATION WITH TIME. DATA PRESENTED IS A SIMPLIFICATION.

MOISTURE CONTENT (% OF DRY WT.)	DRY DENSITY (LBS/CU FT)	SAMPLE TYPE	SAMPLE	BLOWS/FT.	DEPTH (FEET)	USCS	GRAPHIC	SOIL DESCRIPTION
34.1	84	G R		push	0 5 10 15	CH		Fat CLAY; with sand, trace gravel, brown/red, wet color change to light brown at 8 feet Backhoe Refusal at 10 Feet on Severly Weathered Limestone

N- STANDARD PENETRATION TEST
 R- RING SAMPLE
 C- CORE: %RECOVERY/RQD
 G- GRAB SAMPLE
 B- BUCKET SAMPLE

NOTES: Groundwater Not Encountered



WESTERN TECHNOLOGIES INC.
 2400 Huntington Drive
 Flagstaff, AZ 86004-8934

PROJECT: COF WWH DETENTION BASIN
 PROJECT NO.: 2528JW053

TEST PIT LOG

PLATE
A-3

DATE EXCAVATED: 8-29-18
 LOCATION: See Location Diagram
 ELEVATION: Not Determined

TEST PIT NO. 2

EQUIPMENT: DEERE 310K
 EXCAVATION TYPE: 24" bucket
 FIELD ENGINEER: G. Burr

THIS SUMMARY APPLIES ONLY AT THIS LOCATION AND AT THE TIME OF LOGGING. CONDITIONS MAY DIFFER AT OTHER LOCATIONS AND MAY CHANGE AT THIS LOCATION WITH TIME. DATA PRESENTED IS A SIMPLIFICATION.

MOISTURE CONTENT (% OF DRY WT.)	DRY DENSITY (LBS/CU FT)	SAMPLE TYPE	SAMPLE	BLOWS/FT.	DEPTH (FEET)	USCS	GRAPHIC	SOIL DESCRIPTION
21.2		G				GC		Clayey GRAVEL; with cobbles and boulders, some sand, brown, moist
		R	○	push	5			color change to light brown at 6 feet
					10			
					15			
Backhoe Stopped at 12 Feet								

- N- STANDARD PENETRATION TEST
- R- RING SAMPLE
- C- CORE: %RECOVERY/RQD
- G- GRAB SAMPLE
- B- BUCKET SAMPLE

NOTES: Groundwater Not Encountered



WESTERN TECHNOLOGIES INC.
 2400 Huntington Drive
 Flagstaff, AZ 86004-8934

PROJECT: COF WWH DETENTION BASIN
 PROJECT NO.: 2528JW053

TEST PIT LOG

PLATE
A-4


Test Pit No.	Depth (ft)	USCS Class.	Particle Size Distribution (% Passing by Weight)							Atterberg Limits		Laboratory Compaction Characteristics			Remarks
			3"	¾"	#4	#10	#40	#200	2μ	LL	PI	Dry Density (pcf)	Optimum Moisture (%)	Method	
1	0-5	CH	100	98	98	95	91	81.7		51	26				2
2	0-5	GC	82	61	56	55	50	44.9		52	35				2

NOTE: NP = Non-plastic
μ = microns (2μ = 0.002mm)

REMARKS

Classification / Particle Size / Moisture-Density Relationship

1. Visual
2. Laboratory Tested
3. Minus #200 Only
4. Test Method ASTM D698/AASHTO T99
5. Test Method ASTM D1557/AASHTO T180
6. From the ADOT Family of Curves

 <p>Geotechnical Environmental Inspections Materials</p> <p>Western Technologies Inc. The Quality People Since 1955</p> <p>wt-us.com</p>	PROJECT: COF WWH DETENTION BASIN JOB NO.: 2528JW053	PLATE B-1
	SOIL PROPERTIES	

REV	DESCRIPTION	BY	DATE	APPN	DATE

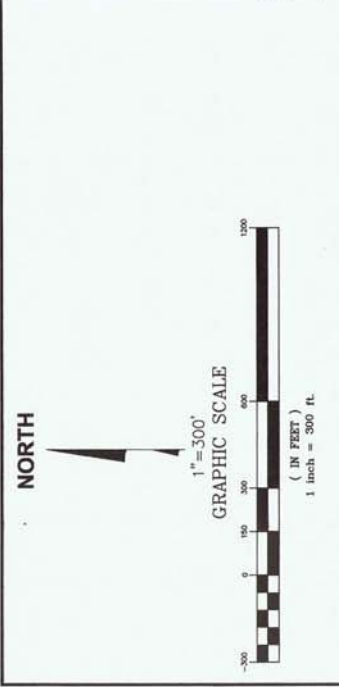
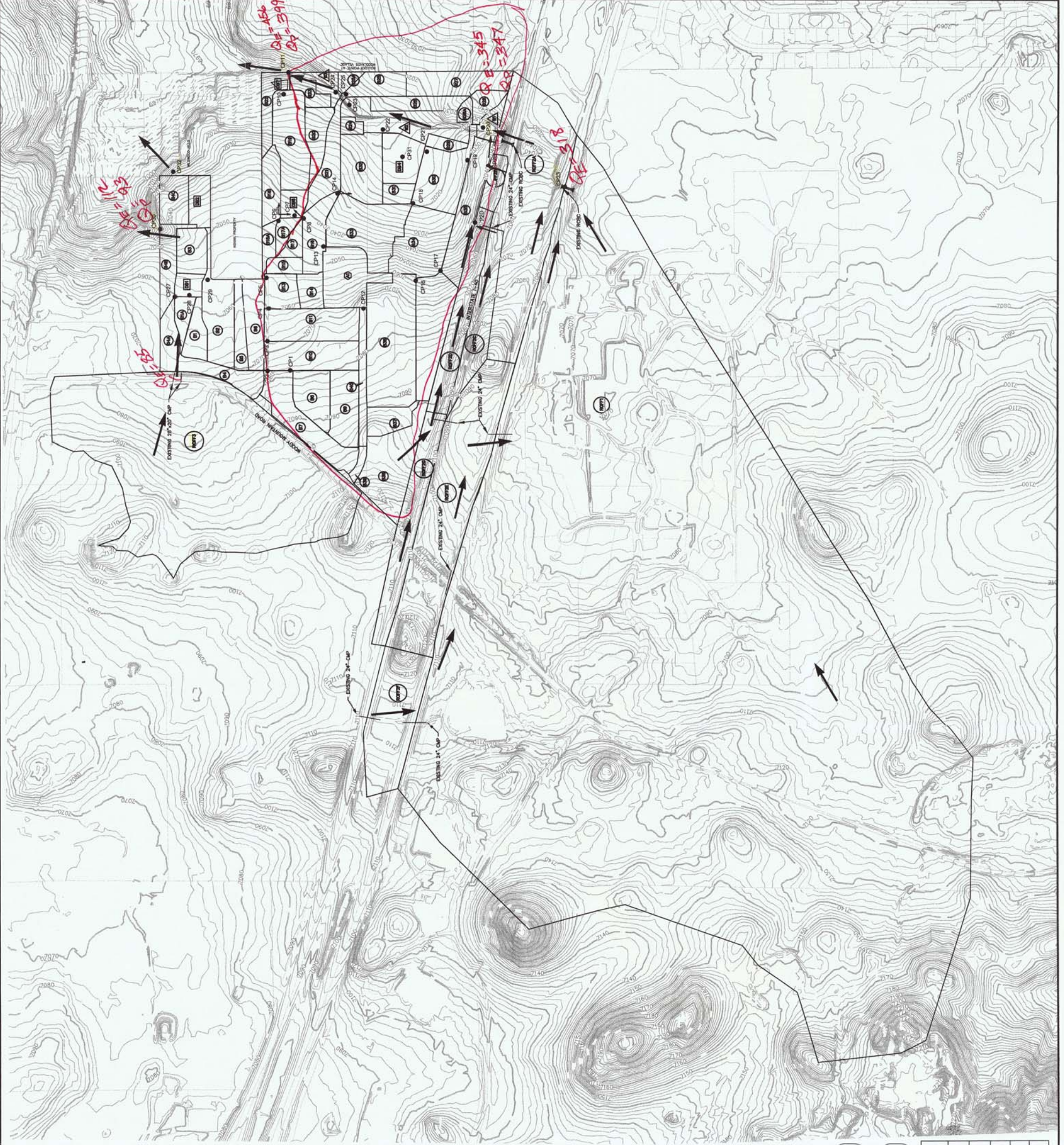
PROJ. NO.:
 DESIGN: RCW
 DATE: 12/27/04
 SCALE: AS SHOWN
 CADFILE: BASINS.dwg

Stamp Date: _____
 Exp. Date: _____

TRC
 Customer-Focused Solutions
 BV Engineering Nevada
 Web: trcsolutions.com
 Fax: 702-307-4222
 8395 W. SUNSET ROAD
 SUITE 190
 LAS VEGAS, NV 89113

PREMIERE ACQUISITIONS LLC
 PRESIDIO IN THE PINES
 DEVELOPED CONDITION BASIN MAP (OVERALL)

SHEET
FIG 12
 1 OF 1 SHEETS
 PROJECT ID
601.006N



DEVELOPED CONDITION BASINS

HEC-1 STORM FLOW SUMMARY		HEC-1 STORM FLOW SUMMARY	
BASIN	ACRES	0100 (CFS)	0100 (CFS)
B1	0.87	4	16
B1A	0.65	4	28
B2	2.63	12	37
B3	1.31	6	36
B4	1.48	4	39
B4A	1.08	4	53
B4B	1.41	5	68
B4C	1.38	4	68
B5	0.95	3	69
B6	1.67	9	7
B7	2.91	12	NOT USED
B8	1.75	8	82
B9	1.75	8	89
B10	2.63	11	11
B11	2.94	15	19
B12	1.14	6	28
B13	1.14	6	NOT USED
B14	0.63	3	39
B15	0.56	3	47
B16	1.62	9	60
B17	0.50	4	56
B17A	0.49	4	347
B18	1.29	7	125
B18A	0.52	3	17
B19	2.53	12	366
B20	1.27	6	370
B21	1.61	9	15
B22	1.72	8	NOT USED
B23	0.95	4	NOT USED
B24	1.26	5	11
B25	1.26	5	18
B26	1.26	5	93
B27	2.29	10	127
B28	0.69	3	4
B28A	0.31	4	318
B29	0.43	4	
B30	2.82	14	
B31	0.59	4	
B32	2.66	13	
B33	3.87	21	
B34	3.28	16	
B35	2.87	9	
B36	2.59	13	
B37	3.10	8	
B38	0.27	4	
B40	1.02	7	
B41	3.34	9	
W1	0.65	2	
W2	3.02	8	
W3	0.71	2	
W4	2.75	7	
A1	2.70	300	
ROFF1	270.88	32	
ROFF2A	13.90	31	
ROFF2B	0.94	9	
ROFF2C	3.04	13	
ROFF2D	3.78	28	
ROFF2E	13.30	22	
ROFF2F	6.12	12	
ROFF2G	4.36	12	
ROFF3	37.43	85	

NOTE: SHOWN DO NOT REFLECT STORM DRAIN DEDUCTIONS

NOTE: SEE FIGURE 11 FOR DETAILED ON-SITE FLOW PATTERNS

NOTE: THIS INDEX IS PROVIDED ONLY TO SHOW FLOW PATTERNS AND FLOW VALUES

LEGEND

XX	BASIN
XX	DETENTION BASIN 1
XX	WASH 1
XX	AMPHITHEATER 1
XX	WATERS OF THE US

